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F-4 RAIN TIRE PERFORMANCE FLIGHT TESTS

Larry K. McCallon, Major USAF, Project Engineer

MARCH 1974 FINAL REPORT



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AIR FORCE FLIGHT TEST CENTER
EDWARDS AIR FORCE BASE, CALIFORNIA
AIR FORCE SYSTEMS COMMAND
UNITED STATES AIR FORCE

This technical report was submitted under Job Order Number 5549AO by the Performance and Flying Qualities Branch, Flight Test Engineering Division, Directorate of Test Engineering and Services, of the Air Force Flight Test Center, Edwards AFB, California 93523.

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Prepared by:

13 February 1974.

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This report presents the re	sults of the B	F-4 Rain Tire flight
test program. A total of 155	test landings	s were made by an un-
slatted F-4E on both a dry an	d wet concrete	runway. These tests
were done primarily to (a) co	mpare the peri	formance of the Hytrol
Mark III antiskid system to t	he production	F-4 antiskid system,
the Hytrol Mark II, (b) evalu		
mance of four new main landin	g gear tire to	read designs, (c) eval-

uate the directional control performance of three new nosewheel

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tire tread designs compared with that of the Standard nosewheel tire, and (d) evaluate a pilot-selectable, two-mode authority steering system. Secondary objectives were to determine the effects of tire tread wear, various touchdown sink rates, and no flap/half flap landing configurations on the wet runway stopping performance of the F-4. The Mark III antiskid system provided an improvement in the wet runway stopping performance with all five tire tread designs that were tested when compared with that of the Mark II antiskid system with the same tire tread designs. In fact, with the Mark III antiskid system all five tire tread designs outperformed the Mark II/Standard tire combination. Wheel spindowns which could lead to serious locked wheel problems occurred at high brake application groundspeeds with the Mark II antiskid system on As a result, a number of Flight Manual changes are wet runways. The Sommers tire tread design provided the best recommended. stopping performance of all the tires tested. The improvement in stopping performance resulting from use of the Sommers tire was so dramatic that both the Mark II/Sommers tire and Mark III/ Sommers tire combinations outperformed all other antiskid/tire combinations tested. The stopping performance was degraded when worn tires were used with either antiskid system. This degradation was substantial with the Sommers tire, which resulted in no difference between the stopping performance of the Sommers tire and Standard Tire when both tires were worn. Varying the touchdown sink rate affected the wheel spinup times on a wet runway. Brake application before full wheel spinup with the Mark III antiskid system had no significant effect on the wet runway stopping performance. The results of no flap and half flap landing configuration stopping performance tests were inconclusive. Pilot evaluation of the pilot-selectable, twomode authority, nosewheel steering system showed that aircraft control, when the +15 degrees mode was used during takeoffs and landings, was unchanged compared with the production (+70 degrees only) steering system. The pilot also noted no change in the control effort required. Having two steering modes was considered an advantage; however, separate pilot selectability of the steering mode was believed to be unacceptable from a safety standpoint. Recommendations for wiring the system for proper steering mode selection are made. The pilot observed no noticeable difference in the performance characteristics of the three new nosewheel tire tread designs when compared to the Standard nosewheel tire. A number of recommendations concerning braking test instrumentation are made.

PREFACE

This report presents the results of the F-4 Rain Tire flight test program which was conducted at the Air Force Flight Test Center, Edwards AFB, California, between 17 February and 21 September 1973. A total of 70 flights, resulting in 155 test landings, was made for a total of 87.4 flying hours.

The Project Officers during the flight test part of this program, who also served as the project pilots, were:

Lieutenant Colonel George H. Meyers, III Captain Leslie B. Anderson, III January - June 73 June - September 73

The author wishes to express special appreciation to Mr. Charles H. Shields, systems engineer, for his guidance and technical assistance during this program. In addition to participating as a crewmember on some of the flights, he was in charge of ground operations for over 80 percent of the test flights.

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INTRODUCTION

BACKGROUND

The initial requirement to improve the operational capability of the F-4 aircraft on wet runway surfaces was established by United States Air Force, Europe (USAFE) Required Operational Capability (ROC) No. USAFE-11-69, dated 1 July 1969. Further guidance was provided by USAF Requirements Action Directive (RAD) No. 1-60-(1), dated 23 November 1970. During the period July 1968 to July 1969, USAFE had experienced 17 barrier engagements that were traced directly to the phenomenon of tire hydroplaning. USAFE also experienced numerous drag chute failures during 1968. Because of these failures as well as the number of short runways, the number of arresting system engagements was inordinately high. Since most USAFE bases were equipped with BAK-9 and/or BAK-12 arresting systems which had a minimum recycle time of 15 minutes, fighter recoveries and launches were significantly delayed each time an aircraft engaged the barrier. Reliance on arresting systems to stop aircraft on wet runways increased the possibility of aircraft accidents off the end of the runway. These factors reduced the operational capability of USAFE during wet weather and constituted a severe operational hazard. Therefore, it was decided to investigate whether a landing gear tire redesign and/or antiskid modification could improve the F-4 wet runway performance.

In response, AFSC Development Directive No. 263, dated 1 March 1971, was issued, thereby establishing the Rain Tire program identity (Project 5549) and overall program guidance. The purpose of the project was to develop and test hardware which would improve aircraft control and braking during the landing roll on wet runways. The specific objectives were to provide a 25 percent increase in tire friction on wet surfaces, with less than 25 percent decrease in tire tread life; an increase in wet surface antiskid efficiency with no decrease in tire reliability; and an increase in effective steering on wet surfaces. A number of constraints were imposed on the project. The antiskid system had to be off-the-shelf, and testing was proposed in conjunction with the tire tests. Any substitute antiskid control box had to have the same installation, fit, connections, and functions as the existing F-4 antiskid. Major wiring modifications, hydraulic system modifications, or aircraft modifications other than replacement of existing equipment required for antiskid and steering control improvements were not authorized. The safety of F-4 operations on dry runways could not be compromised to provide any tire, antiskid, or steering control improvements.

The overall Rain Tire project testing effort was to include flight tests, carriage tests, and field service tests. For the flight test part of the Rain Tire project, the Aeronautical Systems Division (ASD) requested that the AFFTC evaluate the wet runway performance improvements resulting from four new tire tread designs, an antiskid modification, and a steering modification. In conjunction with the flight tests, carriage track tests of each tire configuration were to be performed at NASA Langley Research Center. Also, the braking and cornering characteristics of each tire were to be independently determined and compared with the flight test data to observe the ability of the F-4 aircraft to use the stopping potential of each design under consideration. The results of Project 5549 were to be correlated by ASD with Project Combat Traction results, Air Force Weapons Laboratory (AFWL) runway surface studies, and other allied efforts to provide a coordinated recommendation.

FLIGHT TEST OBJECTIVES

The specific primary objectives of the Rain Tire flight test program were:

- To quantitatively compare the performance of the Hytrol Mark III antiskid system to the production F-4 antiskid system, the Hytrol Mark II.
- To quantitatively evaluate the wet runway performance of four new main landing gear tire tread designs and compare with the standard production tire performance.
- To qualitatively determine whether three new nosewheel tire tread designs had any effect on the wet runway directional control of the aircraft.
- To qualitatively evaluate a two-mode, limited authority, electricallycontrolled, pilot-selective steering system.

Secondary objectives were to determine the effect of tire tread wear, various touchdown sink rates, and no-flap/half-flap landing configurations on the wet runway stopping performance of the F-4. The secondary objectives resulted from requests to ASD by the Air Force Inspection and Safety Center (AFISC) and the Tactical Air Command (TAC) after review of the F-4 accident history.

TEST AND EVALUATION

GENERAL

TIRES AND SYSTEMS DESCRIPTION

NOSEWHEEL STEERING SYSTEM

Nosewheel steering was provided on the production F-4E by an electrically-controlled, hydraulically-actuated system which is shown schematically in figure 1. When the system was energized by holding down the nosewheel steering button on the forward or aft control stick grip, steering was controlled by rudder pedal movements, which were relayed electrically to the hydraulic actuating system. When de-energized, the nosewheels were free to caster, and the steering system performed a secondary function of shimmy damping.

The system contained a command potentiometer attached to the rudder control linkage, a follow-up potentiometer geared to the steering collar, an electrohydraulic servo valve attached to the rotary hydraulic actuator, and an electronic controller (figure 2). The movement of the rudder pedals increased or decreased the command potentiometer wiper voltage level and the strut rotation increased or decreased the follow-up potentiometer wiper voltage. The controller compared the voltages from the potentiometer wiper circuits and sent an appropriate signal to the electrohydraulic servo valve to steer the wheels via the hydraulic actuator to reduce the differential voltage or error signal. The wheels stopped turning when, at the commanded position, the error signal was zero. The standard +70 degrees of steering angle permitted the aircraft to virtually pivot about either main landing gear for close maneuvering.

The nosewheel steering system which was flight tested provided a pilot-selectable, two-mode authority: +15 degrees for landing and takeoff, and the standard +70 degrees for taxiing and close maneuvering. The additional mode for the steering system was accomplished by changes in the steering control box. Also, additional aircraft wiring was required to provide a steering mode select panel in the front cockpit. This panel (figure 3) contained a two-position switch and two green pressto-test indicator lights which showed which steering mode had been selected whenever the gear handle was in the down position. However, no attempt was made to optimize the cockpit controls or modify the production steering engage and/or wheel turning rate characteristics. A comparison of the standard and modified steering responses is shown in figure 4. As can be seen, the response for the two modes was the same over the first 35 percent of the rudder pedal deflection, which would provide the same "feel" to the pilot for the majority of takeoff and landing rolls. Limiting the steering authority for takeoff and landing would prevent over-command of the nosewheel during situations requiring large rudder pedal deflections. The steering angle was limited to +15 degrees to provide the optimum tire cornering capability during adverse weather operations such as in wet runway, strong crosswind landing operations. Previous tests (reference 1) have shown that increasing the wheel steering angle beyond this 15-degree value actually decreases the tire cornering capability.

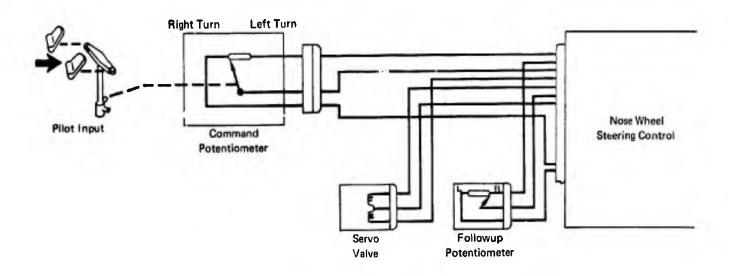


Figure 1 Nosewheel Steering Schematic

Proposal for Nosewheel Steering and Skid Control Design, Instrumentation and Technical Support, MDC Al406, McDonnell Aircraft Company, St. Louis, Missouri, 12 November 1971. UNCLASSIFIED

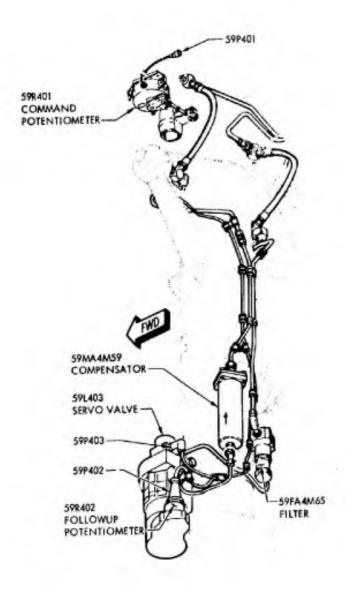


Figure 2 Hosewheel Steering Layout

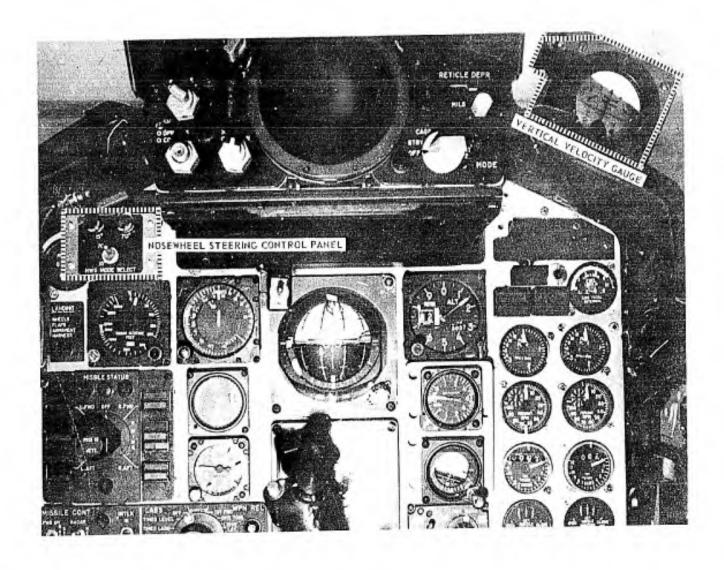


Figure 3 Front Cockpit Instrument Panel

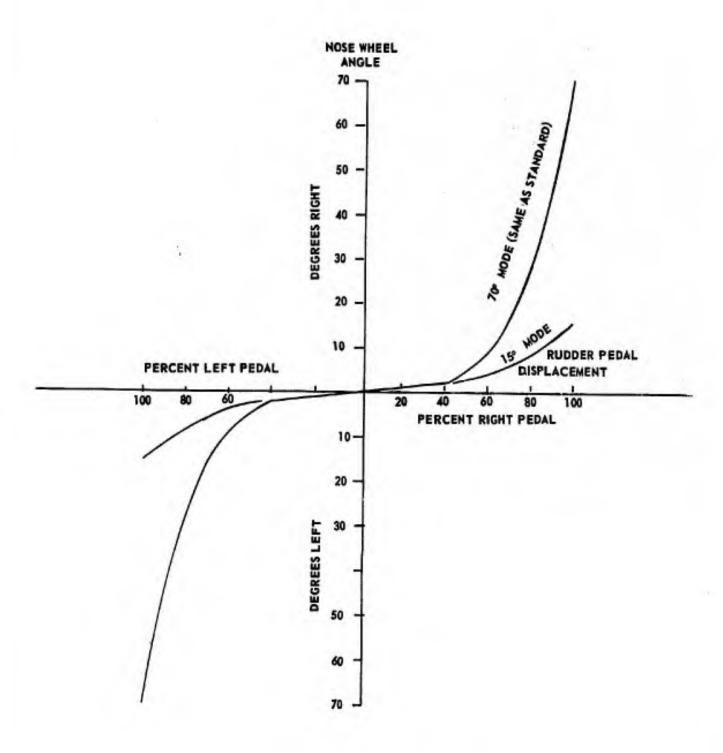


Figure 4 Two-Mode Steering Response

TEST TIRES

The five types of tire treads which were flight tested during this program were designated as Standard (production tire), BFG, USAF, Sommers, and Dunlop. All of the main landing gear tires were size 30 x 11.5 - 14.5 Type VIII tires having a 24-ply rating. The Standard, USAF, and BFG nose gear tires were size 18 x 5.5, Type VII tires with a 14-ply rating. The Dunlop nose gear tire was a size 18 x 5.7, Type VII tire with a 12-ply rating. A comparison of all the tire tread types is shown in figure 5. The tire pressure used during the test program was 265 psi for all the main tires, and was 165 psi for all the nose tires.

The Standard tires (figure 6) were made by the Goodyear Tire and Rubber Company. Both the main and nose gear tires had three circumferential grooves, which were 8/32 inch deep on the main tire and 4/32 inch deep on the nose tire.

The BFG tires shown in figure 7 were produced by the B.F. Goodrich Company. The main gear tires had 6 circumferential grooves with 69 lateral shoulder grooves which crossed the outer circumferential groove on each side. The nose tires had 3 circumferential grooves, 55 shoulder grooves, and, in addition, 55 lateral grooves all the way across the tire. The main tire circumferential grooves were 7/32 inch deep with 8/32 inch deep shoulder grooves. The nose tire grooves were 11/64 inch deep.

The USAF tires were also made by the B.F. Goodrich Company and are shown in figure 8. The main tire had 4 circumferential grooves with 69 lateral shoulder grooves. The nose tire had 3 circumferential grooves with 55 lateral shoulder grooves. Neither the main tire nor the nose tire shoulder grooves crossed any of the circumferential grooves. The main tires had 7/32 inch deep circumferential grooves and 15/64 inch deep shoulder grooves. The nose tire circumferential grooves were 5/32 inch deep with 11/64 inch deep shoulder grooves.

The Dunlop tires shown in figure 9 were produced by Dunlop, Ltd. The main tire had three, 13/64 inch deep, circumferential grooves and the nose tire had six, 5/64 inch deep, circumferential grooves. Both the nose and main tires had a multitude of small, randomly drilled holes in the tread.

The Sommers tire, shown in figure 10, was a Standard tire which had been modified by a patented tread cutting process. The modification resulted in 56 to 58 lateral saw cuts across the tire. The depth of the saw cuts alternated between 1/4 and 3/16 inch.

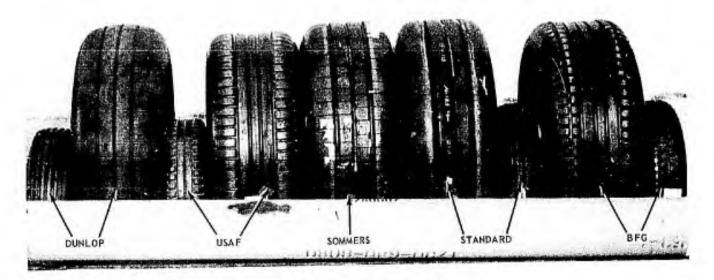


Figure 5 Tire Comparison

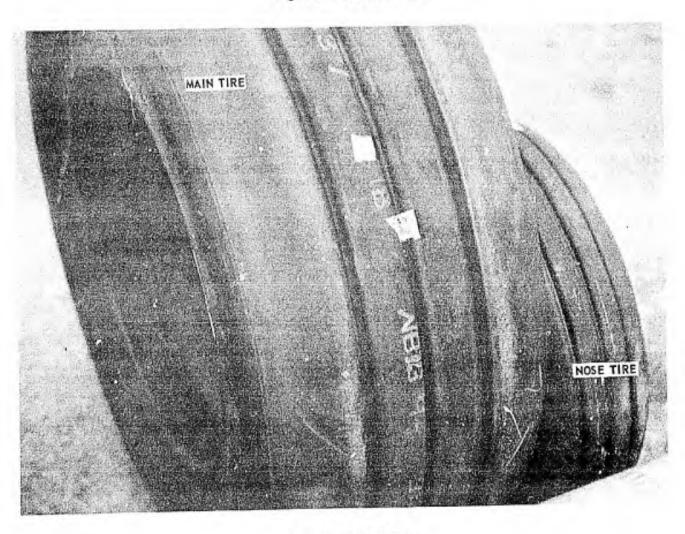


Figure G Standard Tires



Figure 7 BFG Tires



Figure 8 USAF Tires

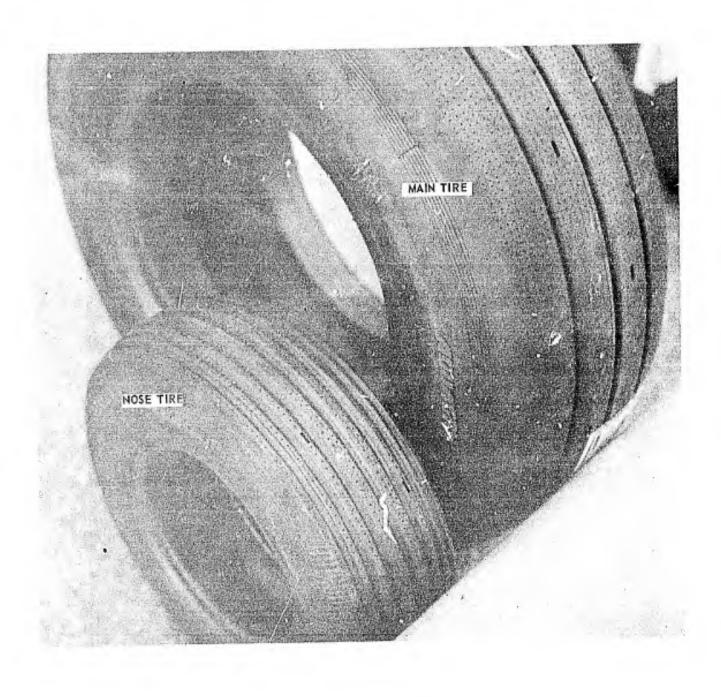


Figure 9 Dunlop Tires

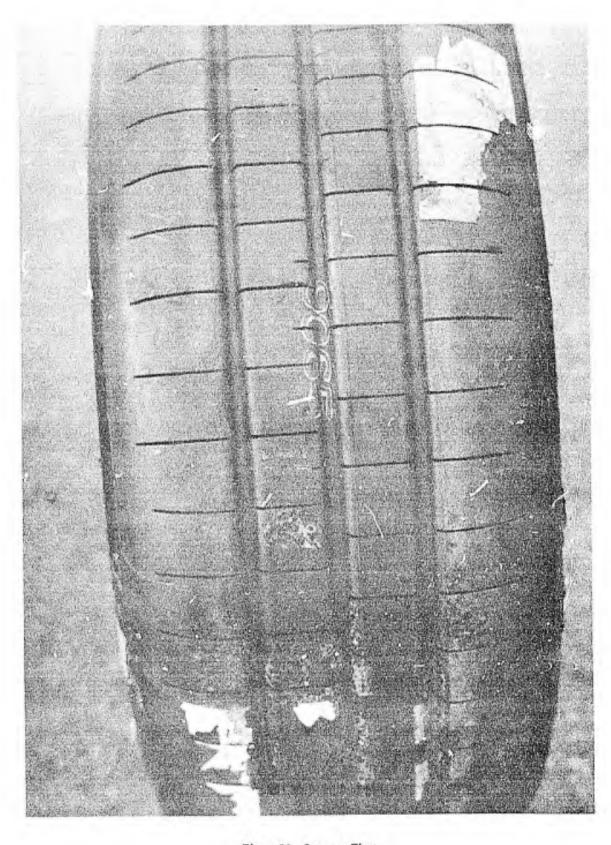


Figure 10 Sommers Tires

WHEEL BRAKE AND ANTISKID SYSTEM

Each wheel brake contained eight rotating and seven stationary discs, six piston assemblies, a self-adjusting mechanism for each piston assembly, a pressure plate, and a shuttle valve. The brake assembly is shown in figure 11. The brake control valves had two operating modes, one for normal braking and one for emergency braking. An accumulator stored hydraulic fluid under pressure for emergency braking. Should utility hydraulic pressure fail, a manually-operated emergency brake valve, which could be actuated by a T-handle in either cockpit, directed fluid from the accumulator to the emergency portion of the dual brake control valve and emergency braking was accomplished by depressing the rudder - brake pedals. There was no antiskid function during emergency braking.

During normal braking operations, the effort applied to the brake pedal caused the dual brake control valve to regulate the amount of hydraulic pressure which flowed through the antiskid control valve to the individual brakes. With the antiskid system turned off, this metered hydraulic pressure passed through the de-energized antiskid control valve to the wheel brake and was applied to the six brake pistons. The force acting upon each piston was transmitted to the pressure plate, which was forced against the rotors and stators to slow down or stop the wheel rotation. When hydraulic pressure was released, springs returned the pistons to their original position, releasing the braking force.

Both the Mark II and Mark III antiskid systems were pressure-modulating types with paired wheel control and consisted of an exciter ring and sensor for each of the main gear wheels, a control box, a control valve, an on-off switch, quick disengage switches on the forward and aft control stick, and a warning light in the forward cockpit. Essentially, the only difference between the two systems was in the logic circuits in the control box which controlled the modulation of the brake pressure. The part numbers and serial numbers of hardware items used during the test program are given in table 1.

When the antiskid system was turned on, and the aircraft ground speed was above 10 knots, wheel speed information for the antiskid control box logic of both systems was provided by a wheel speed sensor, comprised of a permanent magnet with an inductive pickup coil, mounted in each wheel brake housing. The gear tooth design of the ferrous exciter ring mounted in each wheel assembly caused a fluctuating distortion of the sensor's magnetic field, which induced an ac signal in the sensor's pickup coil at a frequency of 90 cycles per wheel revolution. This ac signal, having a frequency and amplitude proportional to the wheel speed, was sent as an input signal to the antiskid control box which converted the signal to a dc wheel speed signal that was proportional to the ac frequency, but was independent of the ac amplitude. The dc signal was used by the skid detection, wheel speed control logic of both the Mark II and Mark III antiskid control boxes. This dc signal was also picked off by the aircraft test instrumentation to provide the recorded wheel speed data and the cockpit wheel speed readout.

Table 1
WHEEL, BRAKE, AND ANTISKID COMPONENTS

	Component	Type Antiskid	Part No.	l'Earl		
	Wheel	Mark II	9550498		II NO.	
		Mark III				
	Brake	Mark II	9550499			
	Assembly	Mark III	9550499			
	Wheel Speed	Mark II	40-595	22067	& 21750	
	Sensors	Mark III	40-619-1	635 &		
	Antiskid Control Box	Mark II	42-065-1	1305		
	CONTIOL BOX	Mark III	42-311 (Mod 1)1	101		
Antiskid Control Valve	Servo Valve	Mark II	1056350-3	2140	39652	
		Mark III		2240	3963	
	Valve Control	Mark II	39-113	1920	3423 ²	
		Mark III			3423	

Mod 1 beginning with Test 11A.

 $^{^2}$ This unit used beginning with Test 4A.

The logic in the Hytrol Mark II antiskid control box operated on a rate detection principle which compared the instantaneous wheel deceleration with a fixed reference of 16 radians/second2. Any wheel deceleration greater than this reference was interpreted as a skid. This skid threshold represented a deceleration higher than the aircraft was capable of achieving under ideal braking conditions. The skid rate and locked wheel detector, shown in the schematic (figure 12), provided an error signal from the above comparison which was proportional to the rate and depth of skids between 16 and 120 radians per second2 (approximately 20 and 140 feet per second2). If the wheel deceleration was greater than 120 radians per second2, the locked wheel circuitry was actuated, commanding full brake pressure release. The capacitor recovery time in this locked wheel circuit was designed to be considerably longer than the natural recovery time of the wheel under most conditions. The error signal was amplified by the valve driver circuit and transmitted as an electrical command to the antiskid control valve. The pressure bias modulation (PBM) circuitry applied a modulating signal to the valve driver after the initial skid signal. This modulating signal caused the brake pressure to be reapplied at a level below the pressure which caused the last skid, and then to be increased linearly with time until the next impending skid caused the whole cycle to repeat.

The logic in the Hytrol Mark III antiskid control box (figure 13) used the same dc wheel speed signal as the Mark II. However, the Mark III operated on a slip velocity principle which compared the instantaneous translational wheel speed information with a predicted aircraft speed and modulated the brake pressure to try to maintain an optimum difference or slip velocity. Personnel of the Hydro-aire Division of Crane Company, Burbank, California, had determined from tire traction research done by NASA that the maximum tire-to-pavement braking coefficient was achieved by maintaining a slip velocity of approximately 10 feet per second. accomplish this, a velocity reference was continually computed. The average deceleration of the aircraft was derived from the wheel speed signal by the reference deceleration circuit and was used to establish the velocity reference at a deceleration level slightly greater than the average aircraft deceleration just computed. The wheel speed was then compared with this "psuedo" aircraft speed to determine the slip velocity expressed as an error signal. The comparator provided this error signal to the PBM circuit, the transient control circuit, and the compensating The output signals from these three circuits were then summed to provide a composite signal to the valve driver.

The PBM circuit integrated the velocity error voltage to provide a control voltage for the normal smooth modulation of the brake pressure. It modulated the brake pressure in an attempt to hold the velocity error voltage (slip velocity) at a preset PBM threshold value (10 feet per second). However, the velocity reference decreased more rapidly than the wheel velocity, which caused the velocity error voltage to decrease, thereby increasing brake pressure until a skid occurred. The output of the PBM circuit resulted in a decrease in brake pressure for slip velocities above the threshold and an increase in brake pressure for slip velocities below the threshold. The rate of increase or decrease was dependent on the value of the error voltage.

The transient control circuit provided rapid recovery from skids. It generated a large-magnitude, rapid-response signal when its preset error threshold was exceeded by a velocity error voltage generated by a greater than normal wheel speed departure. This commanded a rapid re-

duction of brake pressure to allow for wheel spin-up. During the wheel speed recovery, the transient control was designed to command a rapid buildup in brake pressure to avoid excessively long periods of reduced brake pressure.

The compensating network provided phase compensation to overcome the lag in the brake hydraulic system by providing an electrical spike at the start of brake release or reapplication in each skid cycle. The overall effect of the compensating control was to improve the response to incipient skid conditions.

Antiskid Control Valve

The antiskid control valve was a pressure-modulating, two-stage pressure control servo valve. Basically, it; consisted of a torque motor, jet pipe, receiver tubes, and two pressure-modulating slave pistons. It converted the electrical signals from the valve driver part of the control box into hydraulic pressure commands to the brakes. The antiskid control valve operated in series with and was located downstream from the brake control valves. All three valves were located in the nose wheel well and were hydraulically connected to the brakes through 0.25-inch diameter tubing. Operation of the valve is shown in figure 14. Pilot-metered pressure acted on one end of each of the second stage pistons. action was opposed and balanced by brake pressure acting on the opposite The pilot-metered pressure was also transmitted to the jet pipe which directed the pressure, now a control pressure, to the receiver tubes to apply equal pressure to both sides of the second stage pistons. Since the pressures balanced each other, the springs acted to move the pistons to an open position, which connected pilot-metered pressure to the brakes.

when a skid signal was received at the torque motor, the jet pipe was deflected to increase the pressure in one receiver pipe and decrease it in the other. This unbalance in pressure caused the piston to shift which restricted the passage from the pilot-metered pressure. This reduction in pressure to the brakes continued until the torque motor received a signal to reposition the jet pipe over the receiver tube to equalize the pressure at both ends of the pistons, allowing the springs to again shift the pistons to the open position.

Automatic Checking Circuit

Both the Mark II and Mark III antiskids had an electrical checkout and fail safe system which automatically checked the system at the time power was first applied. This circuit also provided a warning of an electrical antiskid component failure to the pilot any time during flight when the antiskid switch was on and the landing gear control handle was The automatic checking circuit was designed to check for faulty wheel speed sensor coils or a shorted or open wire in the antiskid control box, control valve torque motor, and other associated wiring. Every time the antiskid system was turned on, or the landing gear control handle was placed in the down position with the antiskid system already on, a simulated skid signal was applied to the antiskid system circuits. If a faulty component existed, the ANTISKID INOPERATIVE light illuminated (figure 15) and, for the Mark II system, braking would be returned to full manual control. In the Mark III system, for certain types of failures, the system retained whatever skid control was available at the time of the failure.

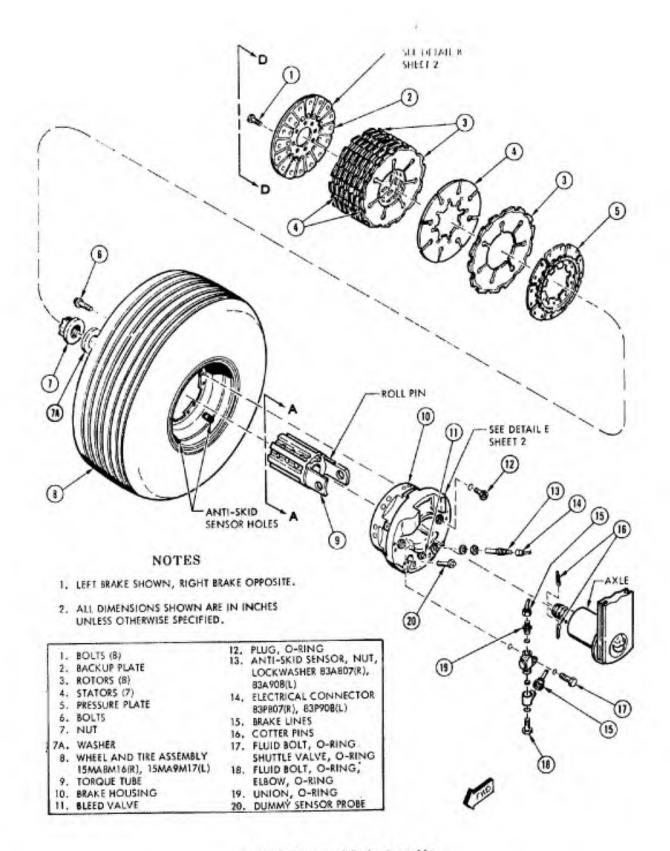


Figure 11 Wheel Brake Assembly

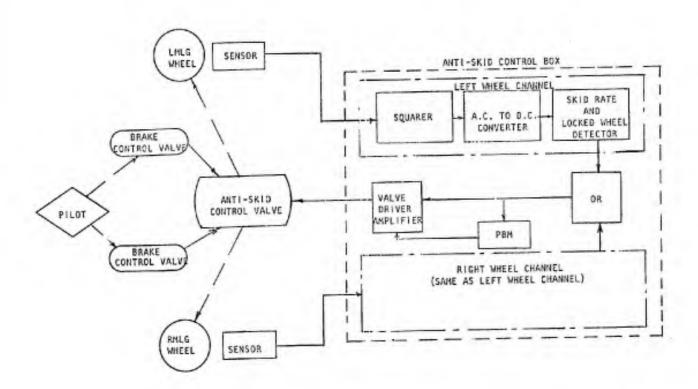


Figure 12 Mark II Antiskid System Schematic

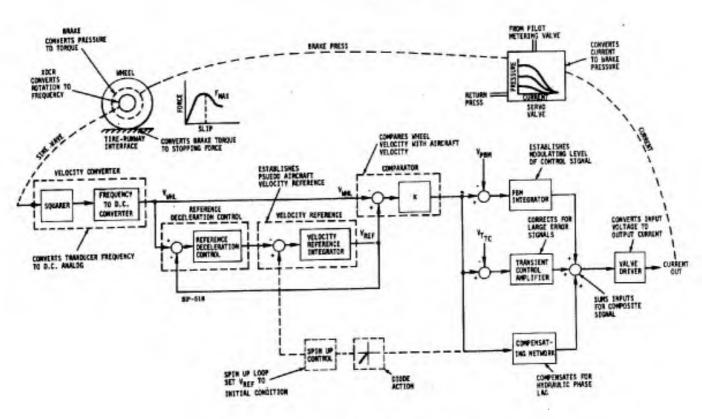


Figure 13 Mark III Amiskid System Schematic

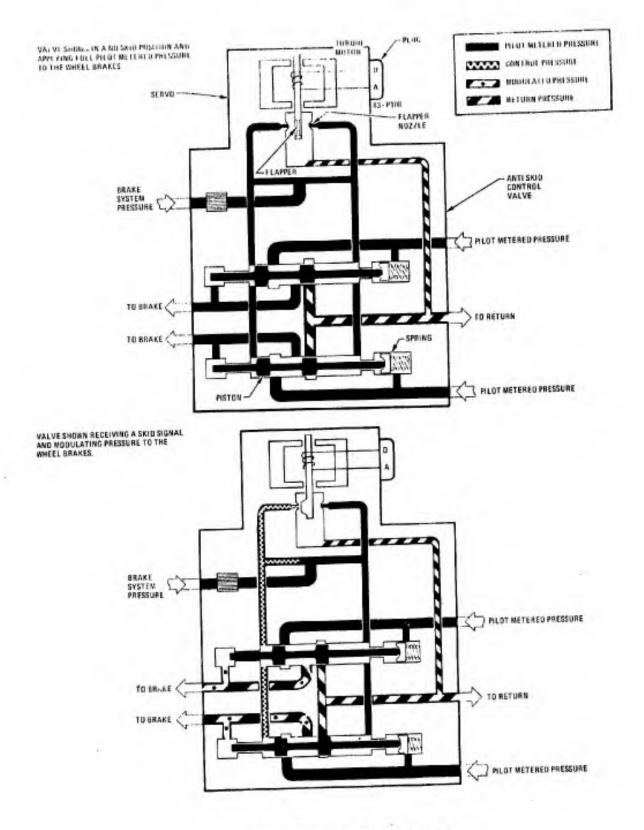


Figure 14 Antiskid Control Valve Operation

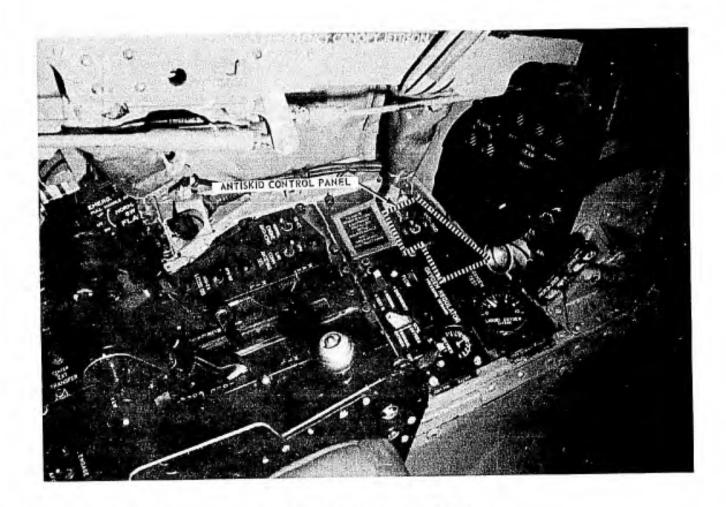


Figure 15 Left Console-Front Cockpit

TEST PROCEDURES

TEST SECTION AND RUNWAY DESCRIPTION

All tests were conducted on runway 04 at Edwards Air Force Base. The runway was 15,000 feet long and 300 feet wide and was constructed of 25-foot square, belt-finished concrete sections. There was an 1,850-foot overrun on the east end with a runout of several miles on Rogers Dry Lake bed available in the event of emergencies. The average southwest to northeast slope of runway 04 was 0.14 percent. The runway was crowned, having a transverse slope of 0.5 percent.

The wet test section was 8,000 feet long and 50 feet wide. It was laid on the centerline or crown of the runway and began 2,500 feet from the approach end of runway 04 (figure 16). This left 4,500 feet of dry runway at the end of the wet test section to provide a stopping assurance section.

The reason that the wet test section was on the southwest end of the runway was twofold. First, landing on runway 04 would provide the lakebed in case of emergency. Second, the prevailing winds at Edwards AFB were from the southwest, therefore the northeast end of the runway had more accumulated rubber than did the southwest end. Since this rubber buildup could affect the test results, an attempt was made to keep this variable to a minimum by putting the test section as far toward the southwest end of the runway as possible and still provide a dry section for aircraft touchdown.

RUNWAY WETTING PROCEDURES

For the wet runway tests, the test section was wetted by using two 5,000-gallon water tankers as shown in figures 17 and 18. The water tankers entered the runway from either the center taxiway or the fire road between the center and northeast taxiway and began the wetting pass at the northeast end of the test section. The trucks lined up one behind the other on the centerline, and each truck laid down a 50-foot wide spray pattern. The trucks proceeded toward the southwest end of the runway at a speed (approximately 11 miles per hour) which would allow the entire 5,000 gallons per truck to be dispensed in the 8,000 feet of test section. Having wetted the test section, the water trucks moved to the northwest edge of the runway and exited the runway at the west taxiway as fast as possible.

Other wet runway test programs conducted at AFFTC had indicated that water runoff and evaporation would be a problem. Experience had also shown that this problem would best be solved by using a mixture of water and organic fire fighting foam. Therefore, a one-percent foam/water mixture was used to wet the test section. To keep the foam build-up to a minimum, every other wetting pass for a day's testing was made with water only. To see if the foam had any effect on the aircraft stopping performance, a series of tests were conducted using only water to wet the test section.

TESTING PROCEDURES

Approximately 35 minutes before each series of landings which required a wet runway, the water trucks made one wetting pass with the one-percent foam/water mixture to pre-wet the test section. After refilling the trucks and immediately prior to the initial aircraft takeoff, a second wetting pass was made using only water. As the second wetting pass began, the test aircraft proceeded down the dry part of the runway on the southeast side of the test section to the 9,000-foot remaining marker on runway 04 for engine runup. After the water trucks had passed, the test aircraft took off and went into a closed pattern for landing. As soon as possible after the water trucks had finished the wetting pass and cleared the runway, the aircraft landed, touching down in the first 1,500 feet of dry runway to allow the wheels to spin up and the engines to spin down to idle before entering the test section. After the test section was entered, maximum braking was commanded by the pilot and held until the aircraft speed reached approximately 20 knots, and then released to preclude possible brake seizure. If the aircraft exited the wet test section before slowing to 20 knots, brake pressure was released prior to exiting to allow for full wheel spinup and then reapplied to stop the

aircraft in the remaining 4,500 feet of dry runway. The Flight Manual (reference 2)² recommended using full aft stick during braking on a wet runway; therefore, this procedure was used on all test landings, both wet and dry. Nosewheel steering was engaged prior to or at brake application and held on for all test landings. Although carried on all flights, the drag chute was not used during any of the test landings.

As soon as possible after the aircraft came to a stop, the crew chief, who was in a vehicle with the test conductor at the center taxiway, was driven to the aircraft location where he visually inspected the brakes for any malfunction and the tires for flat-spotting or chunking. The brake temperature was also monitored in the rear cockpit, while the aircraft was on the ground, to see if the temperature exceeded 900 degrees C. This was the temperature, calculated by ASD (ENFL), below which a maximum test gross weight aborted takeoff could be made safely. This temperature was not exceeded on any of the test landings.

If the tires were not flat-spotted, and if there were no obvious malfunctions, the aircraft took off and went into a holding pattern at approximately 10,000 feet altitude, flying with the landing gear down to air cool the tires, wheels, and brakes. To minimize taxi time and heat buildup in the tires and brakes, the aircraft took off on the dry part of runway 04 from where it had stopped if there was 4,000 feet of runway remaining. If there was not enough runway remaining, then the aircraft was taxied to the approach end of runway 22 for takeoff.

The rate and amount of heat transfer to the wheels and tires was uncertain, but the maximum temperature while on the ground had been estimated to occur approximately 20 to 30 minutes after landing. Therefore, a time limit was imposed such that the time between the aircraft coming to a stop and taking off again would not exceed 10 minutes. This limit proved to be no problem during the test program since the time between coming to a stop and taking off never exceeded five minutes and was normally on the order of two minutes.

If the aircraft could not take off again for any of the reasons given above, or if the previous landing had been the last maximum braking landing for that test series, the aircraft was taxied directly to the hot gun line located on the northeast taxiway. The aircraft was parked, with a fire truck standing by, while the wheels and tires were cooled by using cooling fans.

Once in the air, the brake temperatures were monitored to determine when the next wetting pass could be made and the whole procedure was repeated at another gross weight. For safety reasons and to minimize any effects on the stopping performance due to brake temperature, it had been

T.O. 1F-4C-1, Flight Manual, USAF Series F-4C, F-4D, and F-4E Air craft, 15 August 1973. UNCLASSIFIED

arbitrarily determined that the brake temperature had to be below 100 degrees C before another maximum braking stop could be made. It took approximately 30 minutes of flying with the gear down to air-cool the brakes to this limit. However, this coincided well with the 30- to 45-minute time required to refill the water tankers and rewet the test section. During this 30 minutes or so of flying, the aircraft consumed approximately 4,000 pounds of fuel. Therefore, this procedure of landing and then taking off to air-cool the wheels and brakes in flight resulted in a maximum of three test landings per flight with a full internal fuel load on the aircraft at takeoff.

For the test landings done to investigate the effects of sink rate and flap setting, the same general test procedures were used. However, on landing, the aircraft touched down in the wet test section using airspeeds and procedures as described in the Flight Manual for the configuration or sink rate being tested. For a few of these test landings, maximum braking was commanded by the pilot as soon as it was comfortably possible after touchdown, which meant in some cases that brakes were applied before full wheel spinup. For the majority of these landings, however, maximum braking was not commanded until the wheels had fully spun up.

不得更加,我们就是我们的,我们就是我们的,我们就是我们的,我们的,我们的,我们的,我们的,我们的,我们就是我们的,我们就是我们的,我们是这种人的,我们也是我们的

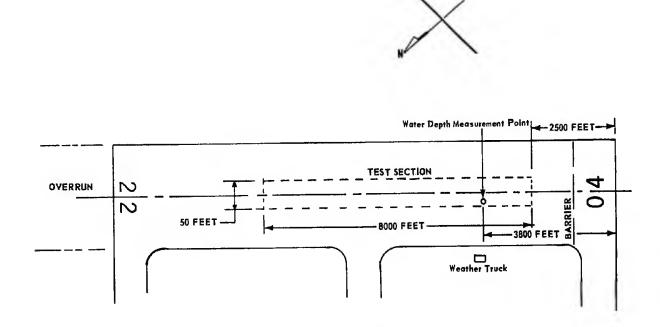


Figure 16 Test Section Layout

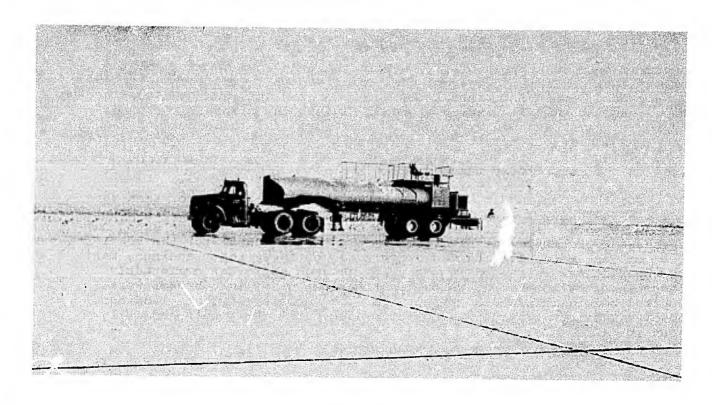


Figure 17 Water Tanker

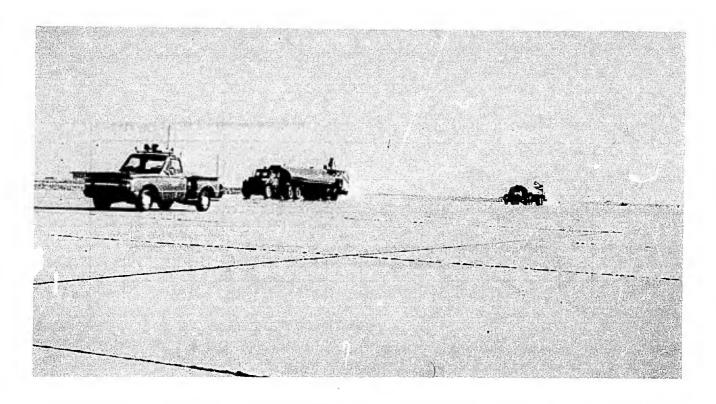


Figure 18 Wetting Procedure

WATER DEPTH MEASUREMENTS

Water depth measurements were made at one point in the wet test section. Due to a lack of manpower, the AFFTC could not make as many water depth measurements as ASD had requested. Therefore, before the test program began, ASD personnel picked one spot in the test section of the runway as a "representative puddle". This spot was marked with paint and the depth gauge was always oriented the same way with respect to the runway when depth measurements were taken (figure 31). For each test the portable weather station was positioned off the runway opposite this point, and the same person who recorded the atmospheric data also made the water depth measurements. Two depth measurements were made per landing. measurement was made as soon as possible after the water tankers passed the measurement point on the wetting pass prior to the aircraft landing. Another was made immediately after the aircraft had landed. Because the foam floated on top of the water in the foam/water mixture, it was very difficult if not impossible to get an accurate reading of the depth. Therefore, the measured depth of thi: "representative puddle" was not a valid indication of the water depth hroughout the test section.

TESTING LIMITATIONS

Two limitations were imposed on when testing could take place. First, because of the hazardous aspects of the test and the potential for tying up the runway for long periods of time, all testing was done during other than normal duty hours at Edwards AFB. This restriction, plus the wind limit of eight knots or less from any direction, resulted in the tests being done during early morning hours on weekdays, weekends, and holidays. The reasons for imposing the eight-knot wind limit were essentially "goodness" of data, and aircraft controllability. It is evident from the wind corrected ground roll formula in appendix A that, to minimize the correction factor for wind and improve data "goodness", the wind velocity should be as low as possible. In addition, a direct crosswind of five to eight knots would appreciably displace water from one side of the test section to the other, as well as make it impossible for the water trucks to spray a uniform water pattern. To be able to compare the tire and antiskid performance, the wetness of the test section needed to be as consistent as possible from one test landing to another.

Normally, when landing in a crosswind on a wet runway, the pilot can use asymmetric power and braking in addition to nosewheel steering, rudder control, etc., to maintain directional control. However, in these tests, the pilot had to use full braking throughout the ground rolls with the engines at idle. Thus, the aircraft controllability and safety aspects also helped establish the eight-knot wind limit.

TIRE WEAR AND BRAKE INSPECTION

Tire wear measurements were made before and after each flight using a tire tread depth gauge. It was originally believed that making tire tread depth measurements after each landing would have been unsafe. However, experience during the test program showed that the crew chief would have had adequate time to safely make such measurements while inspecting the brakes and tires between each landing. The tires were not used again once 50 percent tread wear had been achieved except for the 60-percent tire wear tests.

All tests were done using the new wheel design (P/N 9550498), which meant that the entire brake stack had to be removed each time the tires were changed. Therefore, the brakes were inspected for wear and evidence of brake component failure using T.O. 1F-4E-2-5 (reference 3) procedures each time the tires were changed.

ANTISKID SYSTEM CHECKOUT

Everytime the antiskid system was changed from the Mark II to the Mark III, or vice versa, an operational checkout of the system was done using a modified AN/AJM-18 antiskid system test set (figure 19). The modification to the test set was merely to permit on-scale readings with both Mark II and Mark III systems. The checkout procedure used was the same as the one in T.O. 1F-4E-2-5 modified for the different scale readings.

Two problems were noted during the test program in using the T.O. checkout procedure. First, on a number of occasions, when there was an abnormal indication during the checkout procedure, the remedy was to replace the antiskid control box. Further checking revealed that the problem was not the control box, but bent pins in the electrical connector plugged into the control box or faulty connections at the sensors. The second problem occurred only once. Normal procedure calls for use of the emergency brake system to stop the aircraft during towing operations. In order to restore normal braking, the emergency brake control valve in the nosewheel well must be manually reset. On one occasion this was not done before the operational checkout of the antiskid system. As a result, since the emergency brake system bypasses the antiskid control valve, an abnormal indication was encountered during the antiskid control valve check. The remedy according to the T.O. was to replace the antiskid control valve. In these instances the T.O. procedure proved to be inadequate. To improve the T.O. procedure paragraph 4-31, Antiskid System Operational Checkout, in T.O. 1F-4E-2-5 should be changed as follows. First, add the following NOTE under ANTISKID CONTROL VALVE CHECK prior to procedure 3a: (R 13)

NOTE

Before proceeding, check the EMERGENCY BRAKE CONTROL VALVE and reset, if necessary.

³T.O. 1F-4E-2-5, Landing Gear and Related Systems, USAF Series F-4E Aircraft, 1 March 1972, changed 1 October 1973. UNCLASSIFIED

Second, add this NOTE under ANTISKID CONTROL BOX CHECK prior to procedure 4a: (R 14)

NOTE

When the remedy for abnormal indication requires replacement of the control box, check all electrical connections in the antiskid system for bent pins and faulty connection before effecting the replacement.

In addition to the full operational checkout whenever the antiskid system was changed, a "last chance" check was made before each flight prior to taxi, after engine start, using a battery-operated tester provided by Hydro-aire specifically for this test program and shown in figure 20. The test box connector was attached to the J2 test connector on the antiskid control box. The pilot then turned the antikid system on and applied full pilot-metered brake pressure. When the button on the tester was pushed and released, a wheel speed and skid signal was provided to the antiskid control box which, in turn, sent a signal to the control valve to release the brake pressure. To insure that the brake pressure had been released by the control valve, the brake discs were visually checked by the crew chief and probed with a screw driver to make sure that they had been released. This procedure was followed for each main landing gear (MLG) brake using both a right and left wheel skid (tester toggle switch).

Throughout the test program measures were used in addition to the published T.O. procedures to check out the operation and correct assemtly of both the brake and antiskid system prior to the test flights. Even though this was done, a number of problems, as discussed in this report, were still encountered. The published T.O. procedures for brake assembly and operational checkout of the antiskid and brake system, as well as the trouble shooting procedures proved to be inadequate. Although a number of specific recommendations for improvement are made in this report, better overall procedures and/or equipment should be developed for the brake and antiskid system assembly and operational checkout. The procedures and/or equipment developed should address both the preflight checkout and assembly and checkout after any brake/antiskid system components are disturbed for replacement or other maintenance actions. (R 15)

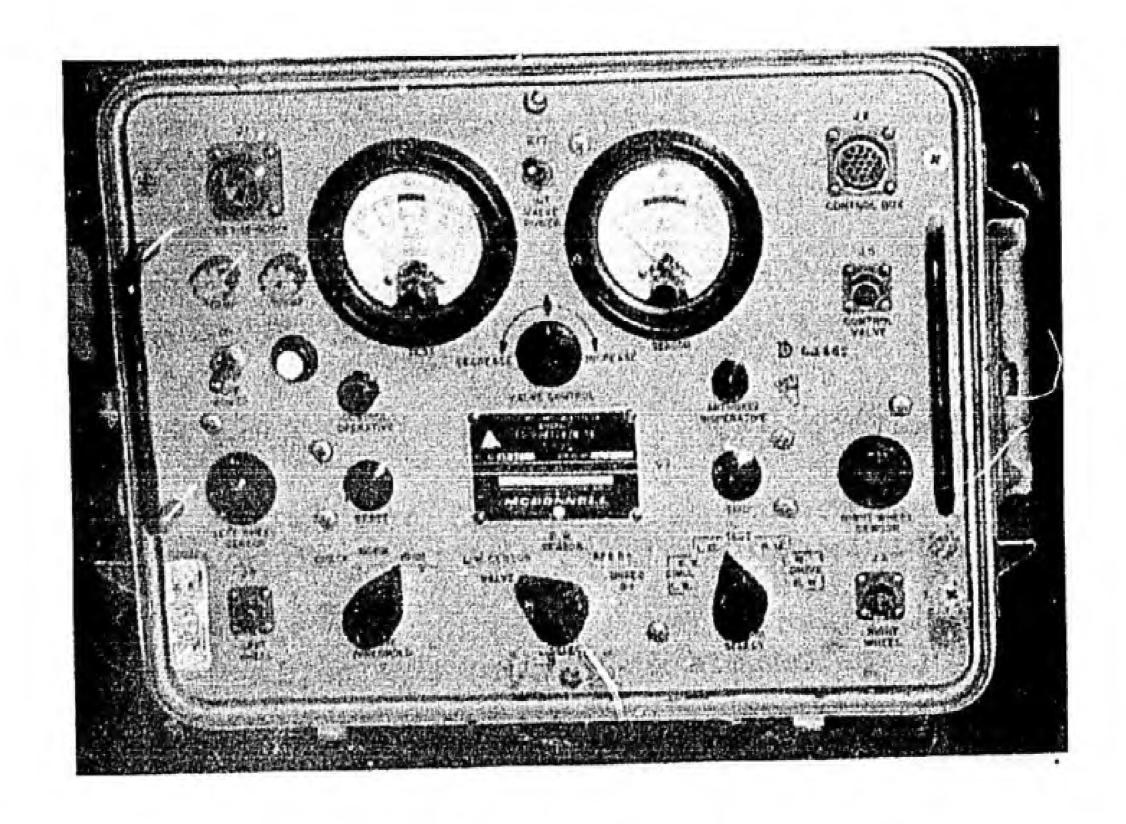


Figure 19 AN/AJM-18 Antiskid Test Set

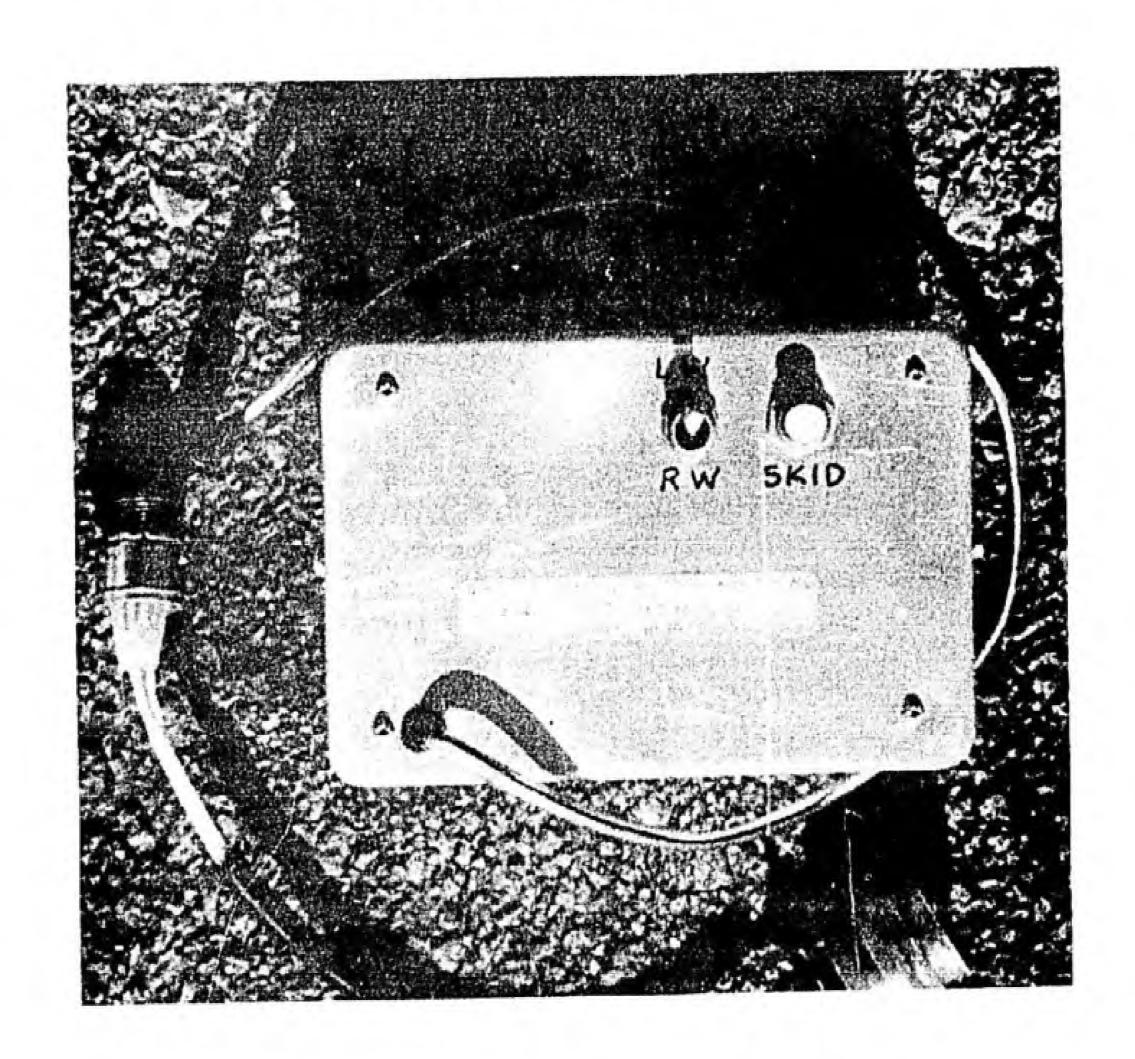


Figure 20 "Last Chance" Tester

RUNWAY CONDITION MEASUREMENTS

In order to correlate the Rain Tire test results with the results of Project Combat Traction, ASD had requested that the AFWL provide a characterization of the skid-resistant properties of the runway and the pavement traction experienced during the Rain Tire test landings. To accomplish these tasks, AFWL used their diagonally braked vehicle (DBV) and Mu-Meter during landing test operations on 17 March 1973 (Test No. 10A) and 24 March 1973 (Tests No. 13A, 13B, and 13C) and accomplished separate ground vehicle tests for runway characterization on 17, 18, 24, and 25 March 1973 and 9 and 10 June 1973. These separate ground vehicle tests also included tests designed to establish the effects, if any, on the runway skid resistance properties of (1) the foam concentration in the foam/water mixture, (2) the high rubber content on portions of runway surfaces, and (3) the runway paint stripes.

The Mu-Meter was a small trailer unit which had been designed and manufactured by M.L. Aviation, Maidenhead, Berks, England, specifically to evaluate the coefficient of friction of runway surfaces (figures 21 to 24). It was towed by a pickup truck and had a continuous recording device that graphically recorded the coefficient of friction versus distance along the pavement. This system was also equipped with instrumentation which integrated the coefficient of friction versus distance curve to obtain the average coefficient of friction between any two selected points. The Mu-Meter had two smooth-tread tires which were toed out with respect to the direction of travel during the measurements and a third knobby-tread tire which served to move the graph paper. The Mu-Meter was towed at a constant speed of 40 miles per hour (a speed calculated to be above the hydroplaning speed of the smooth tires). It physically evaluated the side slip force between the smooth tires and the pavement surface by measuring the force exerted in the trailer tow bar.

The DBV was a specially designed and highly instrumented station wagon (figures 25 to 28) developed by NASA for the Combat Traction program to evaluate the stopping characteristics of runway surfaces. The DBV primarily recorded the stopping distance of the vehicle in a diagonally-braked, locked-wheel mode initiated from a speed of 60 miles per hour. Instrumentation in the vehicle recorded such parameters as stopping distance, deceleration versus distance, velocity versus distance, brake pressure, etc. The diagonal braking was obtained through cutoff valves in the brake lines. By appropriate valve selection, one pair of diagonal wheels on the automobile could be braked while the opposite pair of wheels remained unbraked and freely rolling for vehicle stability and directional control. All wheels were equipped with smooth tread tires which eliminated the effects of tire tread design on braking traction.

During the aircraft landing test operations, the Mu-Meter and DBV made their first measurements immediately after the water trucks wetted the test section before the aircraft landed. The DBV made two stops in the wet test section on the southeast side of the centerline, and the Mu-Meter made one continuous pass on the northwest side of the centerline. The timing of the measurements was such that both vehicles exited the runway with the water trucks. Immediately after the aircraft had landed and exited the test section, both the Mu-Meter and DBV made return measurement runs, each traversing the same side of the test section as before. The results of these measurements, as well as the runway skid resistance properties, will be published in a separate AFWL report.

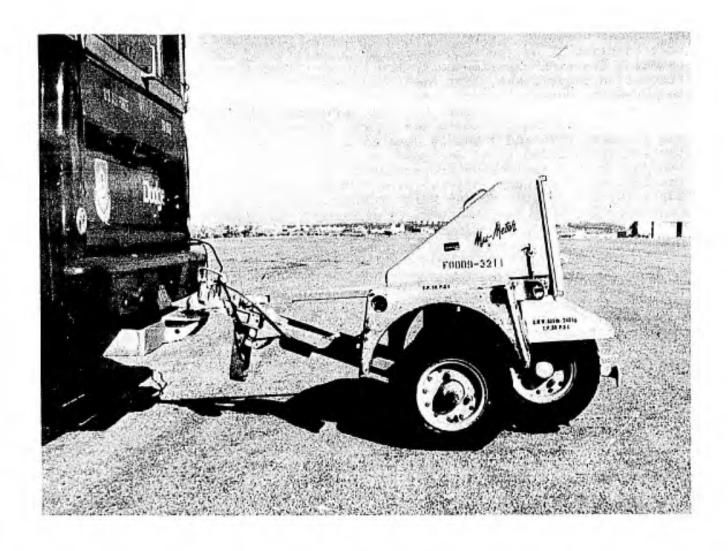


Figure 21 Mu-Meter

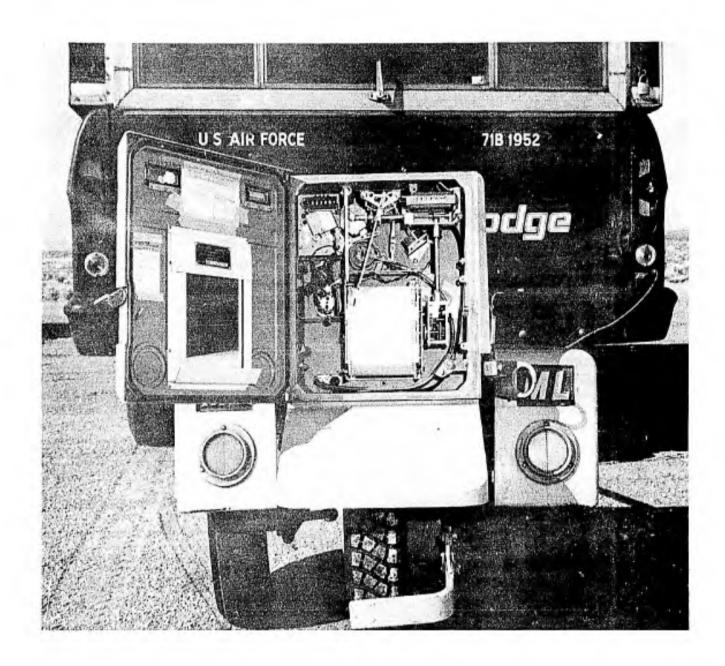


Figure 22 Mu-Meter



Figure 23 Mu-Meter



Figure 24 Mu-Meter



Figure 25 Diagonally Braked Vehicle

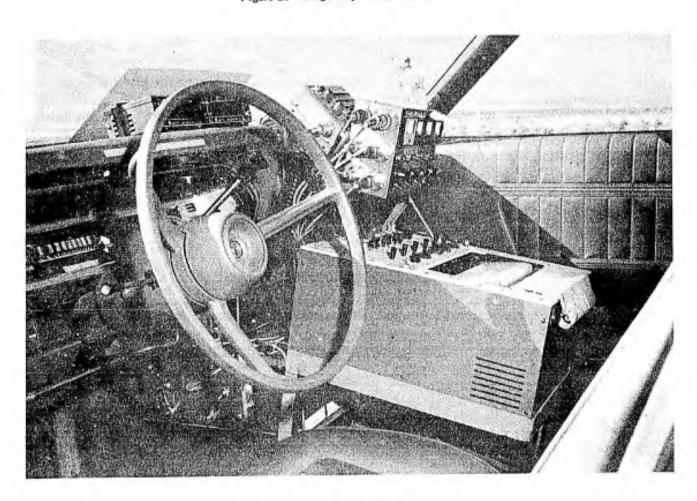


Figure 26 Diagonally Braked Vehicle

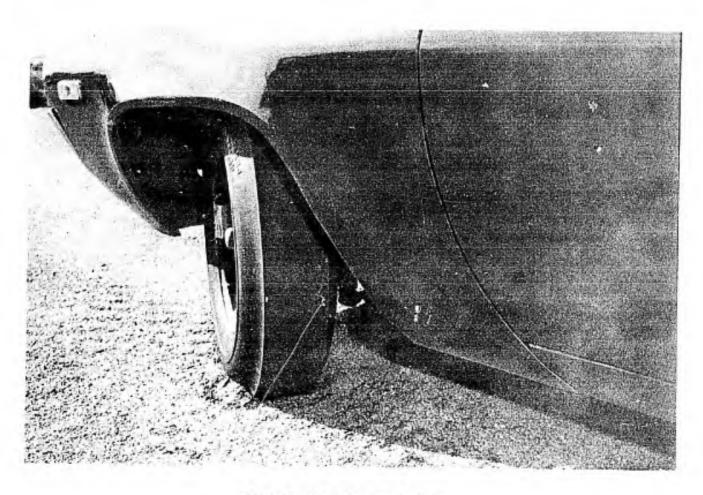


Figure 27 Diagonally Braked Vehicle



Figure 28 Diagonally Braked Vehicle

TEST INSTRUMENTATION.

The instrumentation was specifically designed by McDonnell Aircraft Company to use the data recording system (centerline-mounted instrumentation pod) and instrumentation which were already available on F-4E S/N 66-368 from previous test programs. The additional instrumentation was fabricated and installed by AFFTC personnel. However, instrumentation maintenance, pre- and post-flight calibration and services, and installation support were provided through an AFFTC/McDonnell-Douglas Corporation cortract in support of the AFFTC F-4 Test Team. The following parameters were measured and recorded on magnetic tape onboard the aircraft:

	Parameter	Range	Remarks
1.	Rudder pedal position	0 to 20 deg (10 to 50 vdc)	Measurement taken from com- mand potentiometer wiper circuit in nose gear steering system
2.	Nose gear angle	0 to 70 deg (10 to 50 vdc)	Measurement taken from follow- up potentiometer wiper circuit in nose gear steering system
3.	Nose gear strut pressure	0 to 1,800 psig	Measurement of air pressure in strut upper chamber
4.	Pilot-metered pres- sure (left and right)	0 to 3,000 psig	Measured on input side of antiskid control valve
5.	Brake pressure (left and right)	0 to 3,000 psig	Measured on output side of antiskid control valve
6.	Antiskid control valve signal	0 to 12 vdc	Output of valve driver amplifier measured at J2 test connector on antiskid control box
7.	Main gear wheel speed (left and right)	0 to 2,500 rpm (0 to 20 vdc)	Output of velocity circuit measured at J2 test connector on antiskid control box
8.	Acceleration (longi- tudinal, lateral, and normal)	$+2$ g's (N_X, N_Y) -3 g's to $+9$ g's (N_Z)	Accelerometers mounted at approximate center of gravity
9.	Main gear strut de- flection (left and right)		Potentiometer measurement of MLG scissors angle

10. Brake temperature (left and right)

11. Fuel quantity

- - Measurement taken from forward cockpit fuel quantity gauge

12. Angle of attack (AOA) -10 to +40 deg Measurement taken from pro-

In addition to the onboard recording, both the wheel speed and brake temperature measurements were displayed in the rear cockpit (figure 29). The aircraft vertical speed, taken from the inertial navigation system, was also displayed in the front cockpit as shown in figure 3. Control switches for the onboard recording system as well as an event button were located in both cockpits. Pushing the event button caused an audible tone to be transmitted on the aircraft radio frequency and simultaneously put a signal on the data recording tape. The tone was used for time correlation between the onboard recorded data and the phototheodolite data.

The Askania phototheodolite facility was used on each test landing to

record the aircraft time and ground distance profile.

duction AOA indicator

MAGNETIC TAPE CONTROL PANEL

WHEELSPEED INDICATORS

BRAKE TEMPERATURE GAUGES

PAREL

P

Figure 29 Rear Cockplt Instrument Panel

BRAKE TEMPERATURE MEASUREMENT

The temperature of each brake was measured by a thermocouple inserted in a hole on the inner diameter of one brake stator as shown in figure 30. The wire was routed through a hole in the torque tube and then through the brake housing to a connector on the strut. The intent was to have this instrumented stator put in the center of the brake stack when the brakes were assembled to provide a representative temperature for the entire brake stack. However, during the actual test program the position of the instrumented stator was not always certain and on many occasions was found to be one stator position off of the center position when the brakes were disassembled.

Since the brakes had to be disassembled every time the tires were changed, there was extensive wear and tear on the thermocouples. This, in addition to the heat and vibration environment during the test landings, resulted in constant thermocouple replacement. When possible, the thermocouple was reattached to the same stator to avoid having to "burn in" the brakes when a new stator was used.

At the beginning of the test program, the thermocouples and temperature gauges were installed and temperature limits established (100 degrees C for landing and 900 degrees C for takeoff) to ensure that the brakes were cool enough on landing for good stopping performance data and that enough energy absorbing capability remained after a maximum braking stop to safely accomplish an aborted takeoff. Therefore, initially, both temperature gauges and thermocouples were required to be functioning before any test landings could be accomplished. However, after gaining experience with a number of landings, a cooling time was established and it was found that an adequate temperature margin existed. Therefore, the temperature gauges were deemed not essential for safety or good data and non-functioning temperature gauges were not considered an abort item. However, an attempt was made to always have at least one temperature gauge functioning.

Although the thermocouples proved to be a maintenance problem, they were well worth the effort required since the brake temperature measurement greatly enhanced the safety of the test program. In fact, the procedure of taking off and flying around to air-cool the brakes could not have been safely done initially without the temperature measurement. Even after the temperature display was not required for safety due to experience gained, it provided a qualitative means of monitoring what was going on within the brakes. Since measurement of the brake temperature and displaying it in the cockpit proved to be valuable, it should be considered for use on all brake, antiskid, and/or stopping tests.

WATER DEPTH

Water depth was measured with a gauge designed by NASA for the Project Combat Traction tests (figure 31). The gauge worked on the principle of reflectivity. Plexiglass rods of different lengths that protruded through its body were marked with numbers from 0.010 to 0.100 inch to indicate water depth. Since water is highly reflective and will reflect more light than a runway surface, rods that were not touching the water would appear lighter than those that were touching or submerged in the water. The dark rod with the highest number therefore indicated the local water depth.

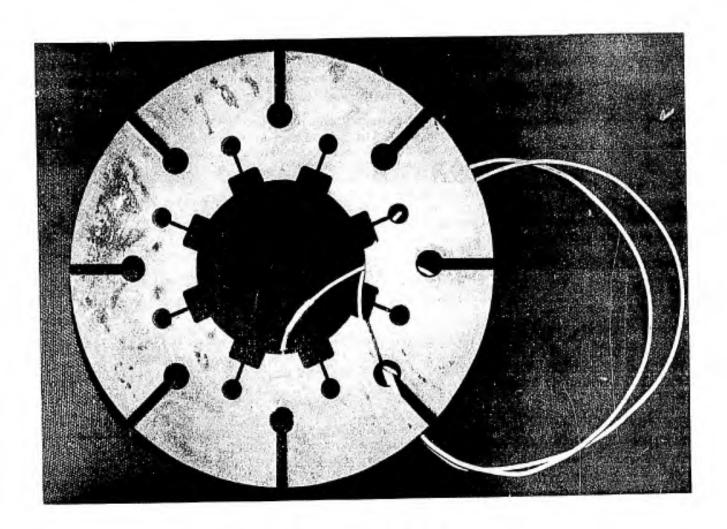


Figure 30 Insrumented Brake Stator

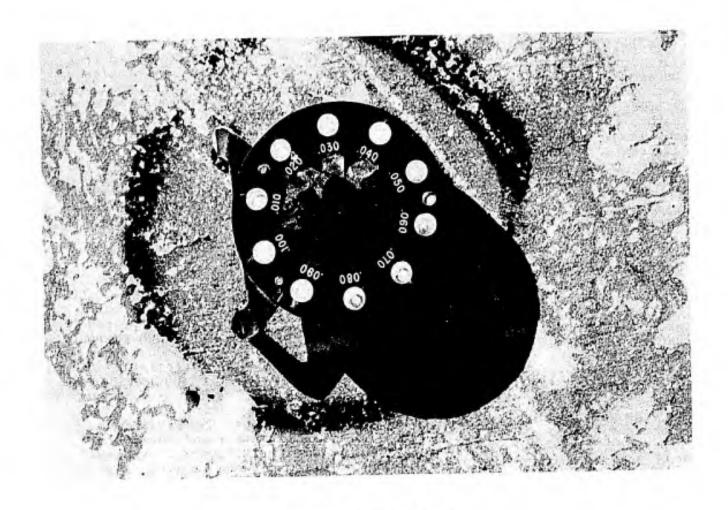


Figure 31 Water Depth Gauge

ATMOSPHERIC DATA

Wind direction and velocity, ambient air temperature, and pressure altitude were measured by a portable weather station. The station was set up approximately 1,300 feet beyond the start of the wet test section and was about 75 feet from the north edge of the runway. Continuous strip chart recordings of wind direction and velocity were made during each test landing from touchdown to brake release.

MAIN GEAR NORMAL FORCE

Prior to the beginning of the test program, ASD/ENFL requested that additional MCAIR (McDonnell Aircraft Company) designed instrumentation be added to the aircraft to measure the main landing gear strut position. Using this information along with a MCAIR-furnished static load versus displacement curve for the two-inch MLG strut high pressure chamber, the normal force of each main gear could be determined. The instrumentation design had been used by MCAIR on other test aircraft and is shown in figures 32 to 34. As shown, the instrumentation consisted of a potentiometer mounted on one leg of each MLG strut scissor with a lever arm attached to the other leg. This arrangement essentially measured the angular change of the strut scissor which was a measure of the strut displacement.

The MLG strut had two (high and low pressure) air chambers. If the strut had been serviced correctly, any load on the MLG strut over approximately 8,200 pounds would begin to compress the high pressure chamber. There would be approximately 1.5-inch displacement for a 20,000-pound load increase on the MLG strut, so the range of the measurements of interest was very small. If the strut had not been serviced correctly prior to flight, then the aircraft would ride on top of the high pressure chamber of the strut and the potentiometer output would not accurately correlate to the load on the MLG strut. The damping characteristics of the strut and friction of the strut seals also contributed to inaccurate measurements.

Because of the shocks associated with landing and the vibrations caused by flying with the gear down, the potentiometers and lever arms repeatedly broke and slipped in flight, resulting in constant replacement and recalibration. The slippage occurring between landings resulted in an invalid potentiometer calibration for many landings. Because of these problems, this type of instrumentation and technique should not be used to obtain MLG strut loads on future F-4 flight test programs. (R 17)

To determine the coefficients of friction for this report the main gear normal force was calculated using the gross weight of the aircraft, the angle of attack measurement to determine lift, and the nose gear strut pressure to determine nose gear normal force.

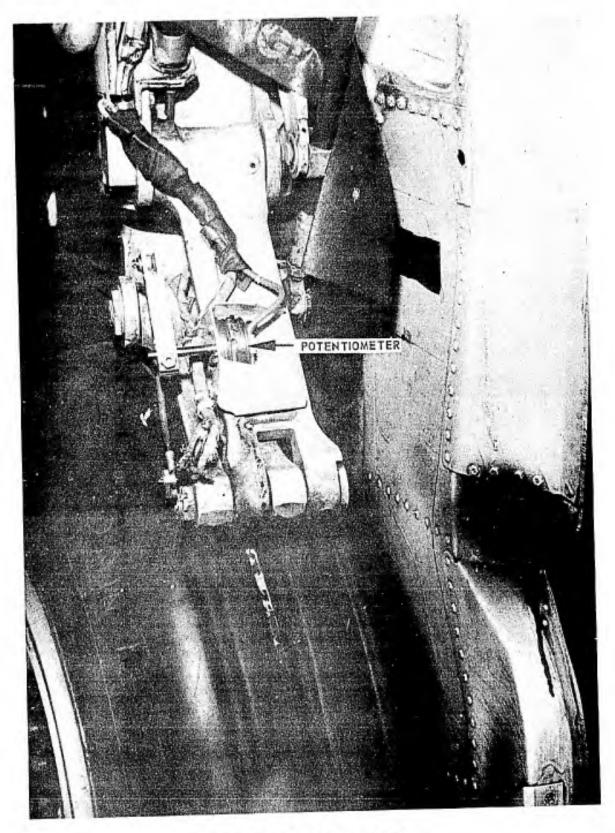


Figure 32 MLG Strut Instrumentation

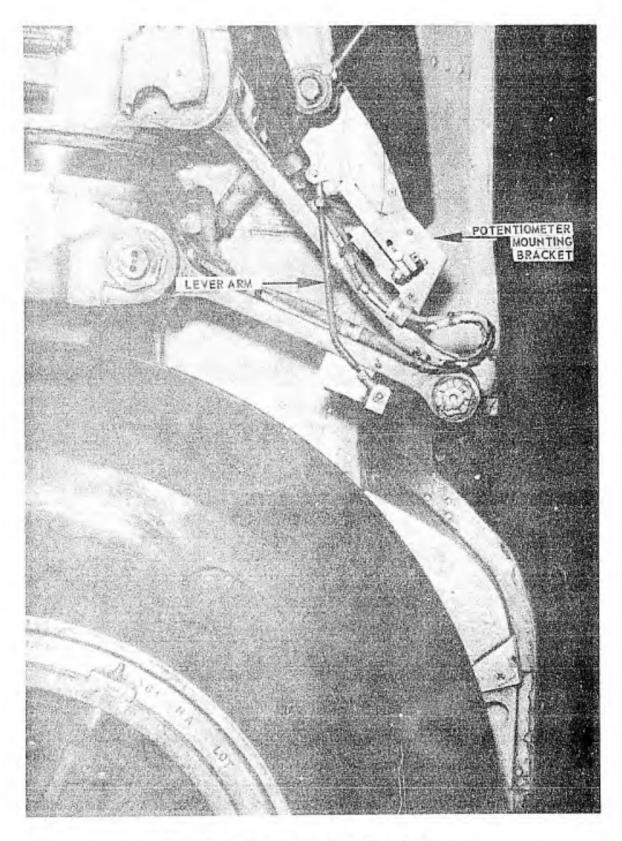


Figure 33 MLG Strut Instrumentation (Weight on Gear)

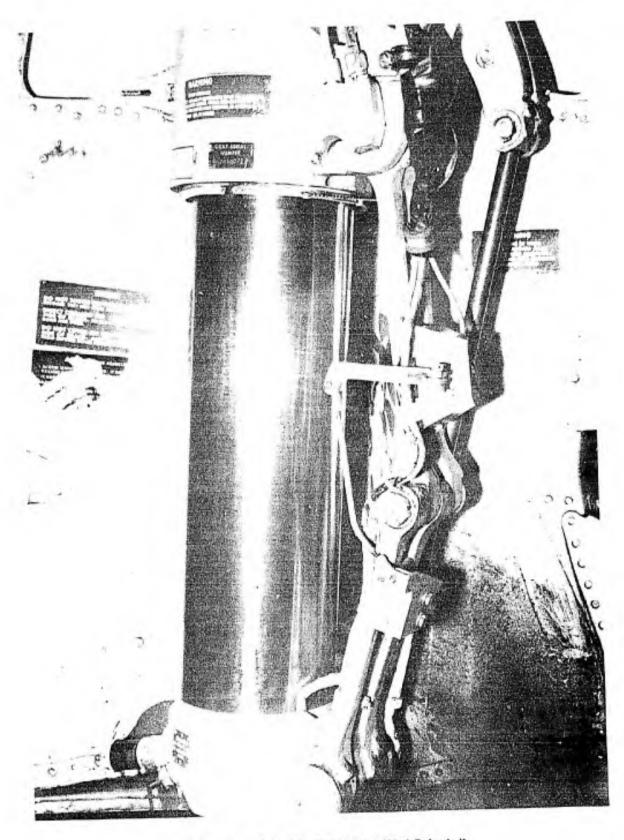


Figure 34 MLG Strut Instrumentation (Strut Extended)

NOSEWHEEL STEERING

The pilot-selectable, two-mode authority, nosewheel steering system was on the aircraft for 90 percent of the test flights. Ground tests during aircraft taxi operations were done to aid in the qualitative evaluation of this steering system as well as to allow each of the two test pilots to "feel" the response of both of the steering modes and the effect of switching from one to the other during turning operations. When this system was on the aircraft, the +15 degrees mode was used for all takeoffs and landings. Both pilots noted that, during the takeoffs and landings, aircraft control was unchanged compared to the production (+70 degrees only) steering system and that there was no change in the control effort required. The advantages of the +15 degrees mode could not be demonstrated during the normal Rain Tire operations because the steering demands during the test landings and takeoffs were always within the region in which the response of the +15 degrees mode would be equal to that of the +70 degrees mode. The value of the +15 degrees mode would not be realized unless a situation, such as a strong crosswind landing or takeoff, requiring large rudder pedal deflections existed. For safety reasons, this type of test could not be done on the wet runway during the Rain Tire program. For normal flight operations of the F-4 aircraft, the switchology of the pilot-selectable, two-mode authority, nosewheel steering system was unacceptable as flight tested. In the test configuration, a two-position toggle switch was used to select the desired mode of steering. It would be easy to forget the switch and have the steering authority in an undesired mode as a result. For instance, after landing, the switch could inadvertently be left in the +15 degrees mode for taxiing off of the runway. Since the response of the steering system is the same for both modes over the first 35 percent of rudder pedal deflection, as the pilot turned off the runway onto a taxiway, he would not be aware of the problem until he "reached" for the full 70 degrees of steering and obtained only 15 degrees of steering. This could result in an accident involving either running off the runway or running into another aircraft. The same thing could happen when leaving the chocks, resulting in hitting a power unit or a parked aircraft on the ramp. When the pilot realized that the switch was in the wrong position, he would be confronted with the question of whether to reposition the switch to the +70 degrees mode, which would immediately command a full 70-degree nosewheel turn (if he had full rudder pedal deflection), or to center the rudder pedals before repositioning the switch, which would delay the turn further.

During the Rain Tire test program, the procedure adopted was to position the steering mode switch to the +15 degrees mode anytime the antiskid control switch was placed to the ON position, and to the +70 degrees mode anytime the antiskid control switch was turned to the OFF position. This procedure provided the desired mode of nosewheel steering system operation during takeoff and landing as well as during taxi operations. However, this required that a separate item be added to the pilot's already lengthy checklist.

If a two-mode authority, nosewheel steering system is adopted for use on the F-4 aircraft, a separate steering mode select switch should not be used. The system should be wired so that the +15 degrees steering mode would be available when the antiskid control switch is in the ON position and the +70 degrees steering mode would be available when the antiskid control switch is in the OFF position. Use of nosewheel steering should still be controlled by the nosewheel steering button on the control stick grip. For situations when operation of the antiskid system is not desired but the +15 degrees steering authority is desired, the system should be wired such that use of the paddle switch on the control stick to drop out the antiskid system would not drop out the +15 degrees steering mode. The logic of this switchology is that, under current operational procedures, anytime the aircraft is in a takeoff or landing phase the antiskid system switch is required to be ON, thus providing the correct +15 degrees steering mode. During taxi operations, the antiskid system Is required to be OFF, thus the correct nosewheel steering mode for taxiing, +70 degrees, would be selected.

NOSEWHEEL TIRES

Three nosewheel tire designs were qualitatively evaluated during the Rain Tire program and compared with the performance of the Standard nosewheel tire. There was no noticeable difference observed, from the pilot's standpoint, in the performance characteristics of the different nosewheel tire tread designs. If performance differences do result from the different nosewheel tire tread designs, the effect would not have been demonstrated during the Rain Tire program, again, because large steering inputs were generally not necessary during testing. Figures 35 to 38 are typical of the minimal amount of wear shown on the nosewheel tires during testing.

One interesting characteristic of the USAF and BFG tire tread designs was noted. During the wet runway tests, the water spray pattern off of these shoulder-grooved tires was very low to the ground. Since this effect may have an application in reducing water ingestion problems of other aircraft, this type of nose tire tread design should be evaluated as a possible method of preventing water ingestion. (R 11)

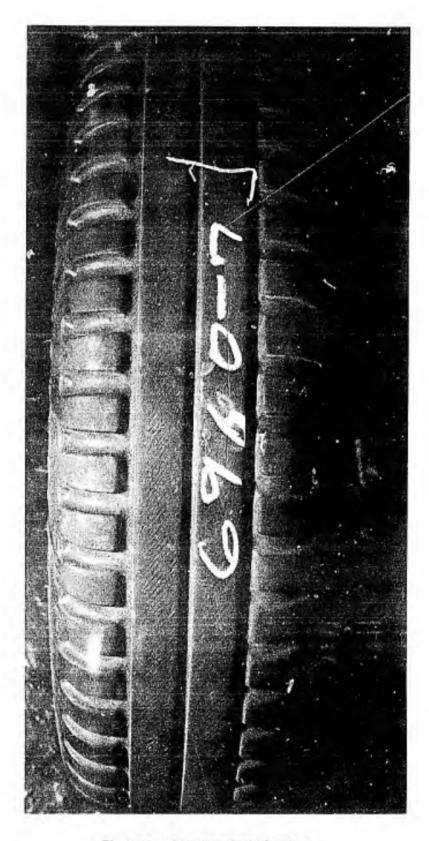


Figure 35 USAF Nosewheel Tire Wear

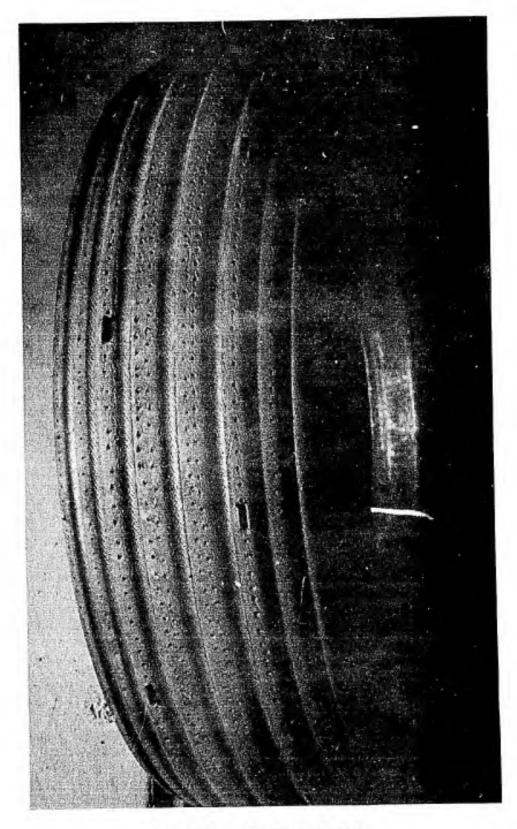


Figure 36 Dunlop Nosewheel Tire Wear

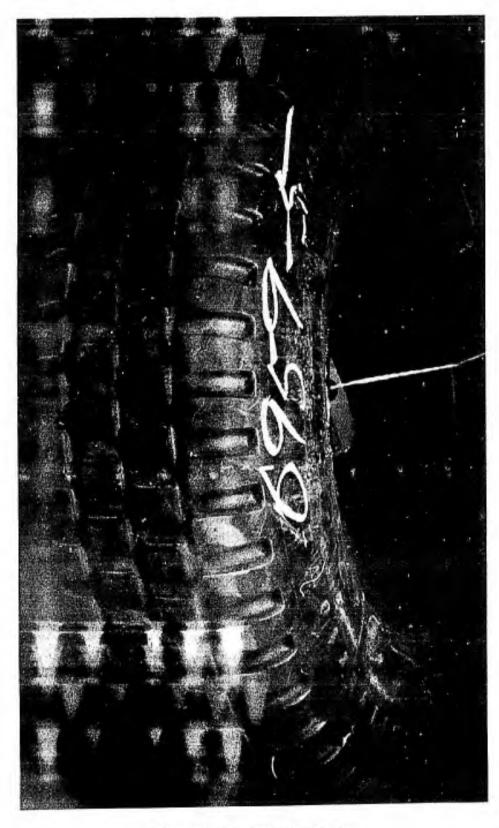


Figure 31 BFG Nosewheel Tire Wear

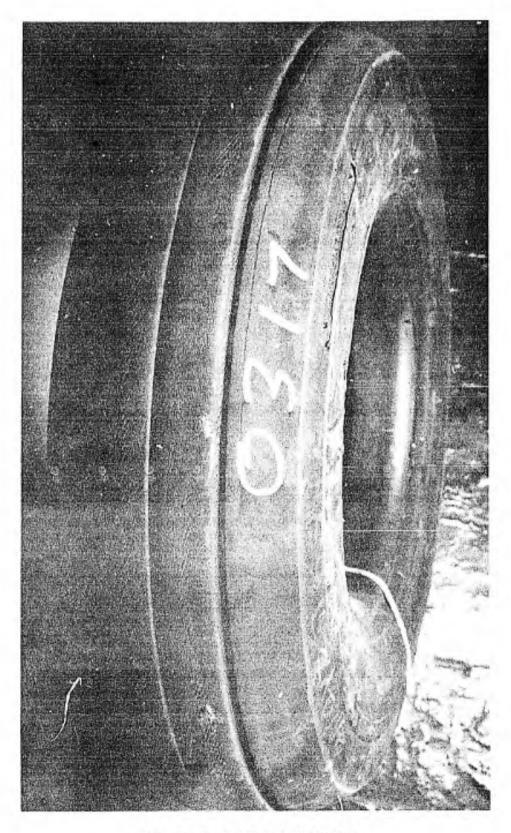


Figure 38 Standard Nosewheel Tire Wear

DRY RUNWAY PERFORMANCE

Seventeen landings were performed on a dry concrete runway using the Standard tire to establish the dry baseline stopping performance of both the Mark II and Mark III antiskid systems. Three dry landings, two with the Mark II system and one with the Mark III, were also performed using the BFG tire to determine what effect the reduced footprint of this tire tread design would have on the dry runway stopping performance. The test day and standard day stopping distances and test conditions are shown in tables 2, 3, and 4. The standard day stopping performance and the braking coefficient of friction developed are shown in figures Al through Al2.

Table 2
MARK II ANTISKID, STANDARD TIRES, DRY CONCRETE RUNWAY

Flt	Date	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (106 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-lb)
NO. 349	(1973) 22 Feb		41,850 39,850	-2.0 -2.4	3.0	2,126 2,120	136/14 140/31	2,883 2,962	27.13 25.33	2,921 3,078	34.13 34.45
352	8 Mar	6A 6B	43,700		8.5	2,411	152/30 144/26	3,645 3,253	32.34 26.80	3,791 3,368	44.84 35.86
353	9 Mar	7A 7B	41,350 35,700	-4.3 -5.2	2.0	2,335 2,326	150/49 141/35	3,663 3,400	26.48 20.79	4,138 3,592	41.09 31.49
354	10 Mar	8B	37,550			2,253	148/23	3,257	28.44	3,290	36.49
	16 Mar	9A	40,200		4.2	2,020	145/30	3,389	26.35	3,452	37.63
355 370	27 Apr		40,800		15.8	2,317	141/38	2,761	26.78	2,930	35.73

		Pot Tire Wear					
Test	Acft Gross Weight (1b)	Brakes Cn (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)	Before Flight After Flight L R		
1A 1B	42,000	136	2,954	34.44	%.	%	
6A 6B	43,000	149 143	3,588	42.36 36.13	6/25	6/87	
7A 7B	42,000	149	4,163	41.16	9/22	0/27	
88	38,000	137	2,896	31.73	-	-	
98	40,000	146	3,469	37.76	- /34	- /31	
19A	40,000	134	2,612	31.70	-	-	

Table 3

MARK III ANTISKID, STANDARD TIRES, DRY CONCRETE RUNWAY

Fit No.	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed [kt]	Distance Brakes On (ft)	Energy Absorbed by Brakes (106 ft-1b)	Extrapolated Stopping Distance (ft)	Kimetic Energy at Brakes On (196 ft-lb)
350	24 Feb	2A 2B	42,850	1.4	6.5	2,168	143/41 140/29	3,705 2,542	26.62 25.17	2,633	38,80
151	3 Mar	4A 4B	43,200	-3.1 -3.3	3.0	2,108	144/33	2,925	30.46 26.95	3,099 2,638	39.80 33.60
157	21 Mar	11A	40,050	-10.4	5.5	2,282	147/31	2,958	29,68	3,113	38.35
160	29 Mar	14A	43,200	-0.1	4.0	2,241	144/34	2,717	30.59	2,866	39.46
351	30 Max	15A 15B	38,875	-0.3	10.0	2,202	139/33 126/38	2,653	24.82 17.11	2,824 2,529	33.19 24.41

	Test		Pot Tire Wear				
		Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)	Before Flight After Flight L R	
	2A 2B	43,000	146 142	4,314	40.56 34.13	0/25	0/25
	4A 4B	43,000	143	3,048 2,688	39.03	0/25	9/35
	11A	40,000	138	2,761	33.64	- /14	- /14
	14A	43,000	145	2,907	40.02	0 /16	0 /31
	15A 15B	38,000	138	2 572	31.71 24.90	0/22	22

Table 4
BFG TIRES, DRY CONCRETE RUNWAY

Plt No.	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (105 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)
399	8 Jun Mark II Antiskid	37A 37B	42,700 38,350	1.0	19.8	2,253 2,249	147/27 141/26	3,504	29.87 24.89	3,646 3,158	40.63 33.71
410	5 Jul Mark III Antiskid		42,400	-3.2	20.0	2,251	160/36	3,686	34.69	3,888	48.12

-		Pot Tire Mear				
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)	Before Flight After Flight	
37A 37B	43,000	147 138	3,691	41.22 32.22	23/100	14/100
475	43,000	156	3,731	46.05	0/100	0/100

Throughout this report, in order to make consistent numerical comparisons among the stopping performances of 'b various antiskid and tire combinations, a kinetic energy at each of three gross weights was chosen, as follows:

Kinetic Energy (10 ⁶ ft-1b)	Aircraft Gross Weight (1b)	Airspeed (KTAS)
37.32	43,000	140
28.43	38,000	130
21.68	34,000	120

Therefore, stopping distance comparisons made for an aircraft gross weight of 38,000 pounds, for example, are made at a kinetic energy of 28.43×10^6 ft-1b which is equivalent to an airspeed of 130 knots.

As shown in the summary plots (figures 39 and 40), with both tires there was a slight improvement in the dry stopping performance using the Mark III antiskid system rather than the Mark II. For the Standard tire, the improvement was approximately 150 feet at 43,000 and 38,000 pounds gross weight, which corresponds to approximately a 5 percent and a 6 percent reduction in stopping distance, respectively. For the BFG tire, the improvement was approximately 200 feet at 43,000 pounds gross weight, which is a 6 percent reduction in stopping distance over the Mark II system. The Mark III/Standard tire combination developed an average braking coefficient of friction of 0.40, whereas the Mark II/Standard tire combination had an average braking coefficient of friction of from 0.34 at 120 knots ground speed to 0.39 at 40 knots ground speed. The average braking coefficient of friction for the BFG tire ranged between 0.33 and 0.35.

In comparing the stopping performance of the two tires at 43,000 pounds gross weight, the BFG tire had a longer stopping distance than the Standard tire by 200 feet for the Mark III system and 300 feet for the Mark II system. These figures represent degradations in stopping performance of 7 and 10 percent, respectively.

Four of the dry landings (Tests lA, lB, 2A, and 2B) were made before the antiskid control valve was changed. After evaluating the first wet runway landing with the Mark III antiskid system (test 3A), the Hydro-aire engineers suspected that the valve was giving a brake pressure on the low side of the specification curve. As a result, the valve was removed and replaced by a valve provided by Hydro-aire having the known calibration curve shown in figure A76. Subsequently, Hydro-aire did a calibration on the original valve which showed that it was indeed slightly out of specification range on the low side, as shown in figure A77. Ignoring the inconsistency of test 2A for the moment, this difference in the calibration of the two antiskid control valves apparently had no effect on the dry runway stopping performance with either antiskid system. A typical Mark II antiskid operation on a dry runway is shown for test 19A in figure B1.

The approximately 1,100-foot increased stopping distance for test 2A (figure A2) was attributed to having a new stator placed in each brake stack prior to this test and not having them "burned in". The effect on the operation of the Mark III antiskid system of having new brake parts which are not "burned in" can be seen by comparing the antiskid system parameters of test 2A and 2B as shown in figures B2 and B3. The antiskid operation shown by test 2B is typical of the Mark III performance on a dry runway. The deep skids and attendant full brake pressure releases shown on test 2A were also observed during the "burn-in" of all replacement brake discs. This antiskid action appeared to be typical of having new brake parts in the brake stack which had not been "burned-in." Since test 2A served to "burn-in" the brakes, test 2B exhibited normal antiskid operation. To avoid the effect on the antiskid operation shown on test 2A, a procedure of "burning-in" new brake parts was adopted for use during the test program. This procedure consisted of doing a refused takeoff from approximately 80 to 90 knots at maximum test gross weight and then cooling the brakes before any test landings were made. The affects of not "burning-in" new brakes on the wet runway performance are discussed in the Sommers tire section. As discussed there, not "burning-in" new brake parts caused a substantial degradation in the wet runway stopping performance and may have significantly delayed the wheel spinup time. A procedure should be developed and used to "burn-in" new brake parts whenever they are installed. (R 8)

The wear on a Standard tire resulting from the dry runway, maximum braking stops is shown in figures 41 and 42. These tires were used on tests 2A, 2B, and 3A, and the result is typical. For all of the dry runway tests with the Standard tire, regardless of the antiskid system, chunking occurred on the inboard tread of the left main tire and the outboard tread of the right main tire. The chunking, in general, appeared to be more severe with the Mark III antiskid system, which would be expected since the Mark III would make the tire work harder due to the scrubbing caused by trying to maintain a constant slip velocity between the tire and the pavement. No explanation for this peculiar wear pattern was apparent.

Another interesting result of tests 2A and 2B is that, during these two dry tests, the left main tire slipped approximately 1 1/2 inches on the rim of the wheel. The right main tire also slipped but to a lesser extent. As a result, tire pressure was measured and found to be 15 psi less in both tires than that before the two tests. This was the most severe tire slippage noted during the dry tests; however, slippages ranging from I/16 to 1 inch also occurred on tests 8B, 9A, and 14A.

Four of the Mark III landings (tests 2A, 2B, 4A, and 4B) were performed before the final "tuning" of the Mark III control box. After evaluation of the first three Mark III, wet runway landings following the control valve change (tests 5A, 5B, and 5C), Hydro-aire engineers determined that the compensating network in the control box needed to be adjusted slightly. This adjustment essentially started the re-application of brake pressure earlier in the antiskid cycle to better match the Mark III antiskid system to the F-4 aircraft hydraulic lag. As shown in figure A2, this "tuning" had no appreciable effect on the dry runway stopping performance of the Mark III/Standard tire combination.

On test 6B, which used the Mark II antiskid system, the outboard tread on the right main tire was stripped down to the cord all the way around the tire as shown in figure 43. The left tire (figure 44) showed hardly any chunking. No explanation for this peculiar event could be determined. For this reason, the data from this test was not considered when fairing a curve through the other data.

It had rained the night before tests 7A and 7B were performed. As a result, the runway was still damp with some puddling when the first landing (test 7A) was made. On the second landing (test 7B), the runway still had some damp spots, but had no puddling. This is why the results of these two tests are not consistent with the rest of the data in figure Al.

On test 14A, the pilot released the brakes at approximately 35 knots ground speed; however, the right brake did not release immediately, causing the aircraft to swerve to the right. After the test, it was found that the right tire had been flat-spotted through two plys of cord (figure 45) and there was a 50- to 75-foot skid mark on the runway. Examination of the antiskid parameter data (figure B4) revealed that the deep skid started approximately 3/4 of a second before the pilot commanded brake pressure release. The antiskid system reacted to it properly by dumping pressure at both brakes. When the pilot-metered pressure was released, the pressure at the brake was released; however, the wheel stayed in the locked-up condition for approximately three seconds after brake pressure release.

Before the tires were changed after this test, a tensiometer and rope were used to measure the amount of force required at the outer radius of the tire to rotate the wheel. The left main wheel required 50 pounds of force to keep the wheel rotating with the brake discs still in the wheel and only 4 pounds after the brake discs had been taken out. However, the right main wheel required 110 pounds of force to start the wheel rotating and 100 pounds of force to keep it rotating with the brake discs in the wheel, and only 10 pounds of force after the brake discs had been removed. Examination of the brake discs showed that the right brake had indeed seized and that a considerable amount of mix (sintered metal) had been transferred from the rotor next to the pressure plate (figures 46 to 48). The mix had been transferred both to the pressure plate on one side and to the stator on the other side. Four stators were also warped out of limits in the right brake and four rotors from both brakes were worn beyond limits. All new brake parts had been installed prior to test 11A, which meant that there was a total of one brake "burn in", one dry runway test, and five wet runway tests, all with the Mark III antiskid, prior to this event on test 14A. The force required to overcome the friction in the wheel was again measured when a dragging wheel was noted during the BFG tire/wet runway tests. The results are discussed in detail, and a recommendation is made, in that section of this report.

On test 15B, there was an extremely deep skid on the right tire immediately after brake application and another extremely deep skid on the left tire later in the test (figure B5). As a result, there was a considerable reduction in pressure at the brake for a large portion of the run. This was the only low aircraft gross weight (34,000 pounds) test landing made on a dry runway with either the Mark III or Mark II antiskid systems during the Rain Tire test program. It is unknown whether the Mark III antiskid action shown on this test was an anomoly or typical of the operation of the Mark III and/or Mark II antiskid systems at low aircraft gross weights. However, this same type Mark III antiskid action occurred at low aircraft gross weight on one of two dry runway test landings made during the USAF evaluation of the F-4F aircraft at the AFFTC (reference 4)4.

The wear on the BFG tire resulting from the dry runway tests was extreme compared with that exhibited by the Standard tire. The tires used on tests 37A and 37B are shown in figures 49 and 50, and those used on test 47A are shown in figures 51 and 52. It should be noted that the same peculiar wear pattern pointed out on the Standard tires was present on the BFG tires, that is, there appeared to be more wear on both the outboard treads of the right main tire and on the inboard treads of the left main tire.

是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们 第一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们就是一个时间,我们

The tires used on test 47A with the Mark III antiskid system were unused before the test. After only one maximum braking dry runway landing, most of the tread was gone, rendering the tires useless for further tests. However, prior to tests 37A and 37B with the Mark II antiskid system, the tires already had 23 and 14 percent wear and showed about the same wear after two maximum braking, dry runway stops as that shown on test 47A. This is not surprising since the Mark III system works the tire harder as previously mentioned. The action of the Mark II and Mark III antiskids with the BFG tire are shown in figures B6 and B7, respectively.

The left tire in figure 50 was flat-spotted during a 90-degree turn off of the main runway after testing was completed rather than during the test. The aircraft was at minimum gross weight (less than 34,000 pounds) at the time because, afte test 37B, the aircraft took off again to cool the brakes and made a free oll landing at 34,000 pounds. The turn off the runway was made with the antiskid system turned off, at a normal slow speed (less than 20 knots) using a slight amount of even braking on a completely dry runway. When the turn was established, the aircraft entered a slight skid that was terminated by releasing brake pressure, centering the nosewheel steering, and reapplying brakes until the aircraft was stopped. The turn was then resumed without further difficulty. It can be seen from the wear pattern that the shoulder portion of the tread becomes "fluted". These fluted pieces of rubber may have broken off of the inside shoulder of the tire and gotten under the tire in the turn, thus causing the skid. Because of this incident and the extreme wear shown by these tires, further wear tests should be conducted if the BFG tire is considered for use in the field. (R 12)

Anderson III, Leslie B., Captain USAF, German F-4F Evaluation, AFFTC Technical Letter Report, Air Force Flight Test Center, Edwards AFB, California, September 1973. CONFIDENTIAL



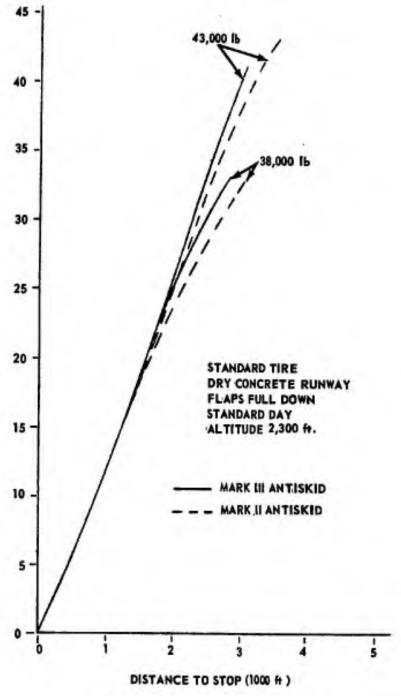


Figure 39 Standard Tire Performance

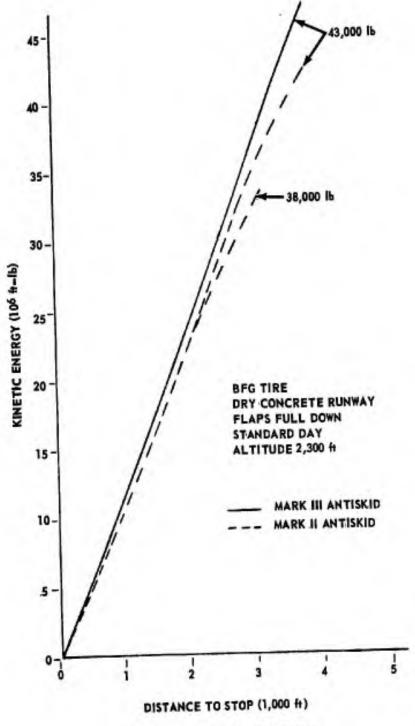


Figure 40 BFG Tire Performance



Figure 41 Right Standard Tire (After Tests 2A, B & 3A)



Figure 42 Left Standard Tire (After Tests 2A, B & 3A)



Figure 43 Right Standard Tire (After Tests 6A, B)

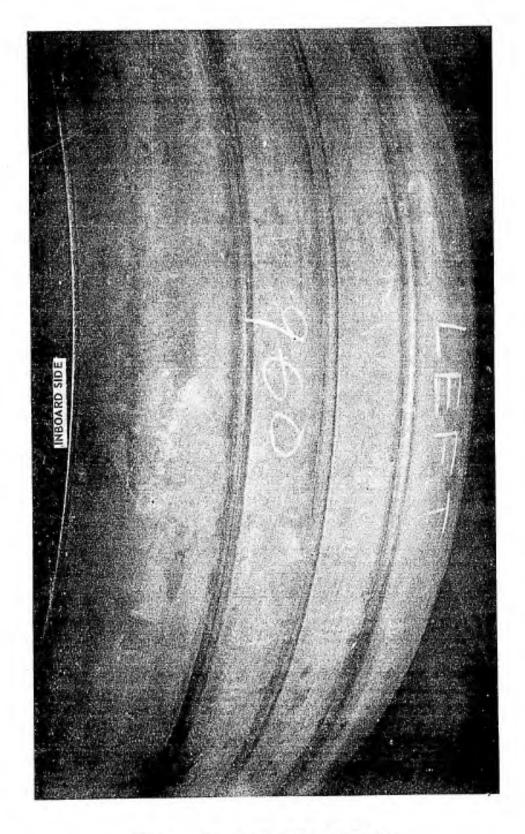


Figure 44 Left Standard Tire (After Tests 6A, B)



Figure 45 Right Standard Tire (After Test 14A)

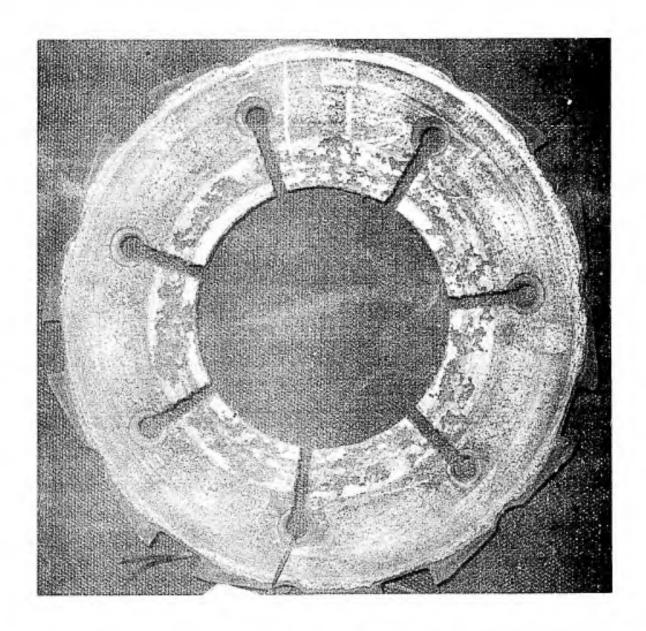


Figure 46 Brake Rotor

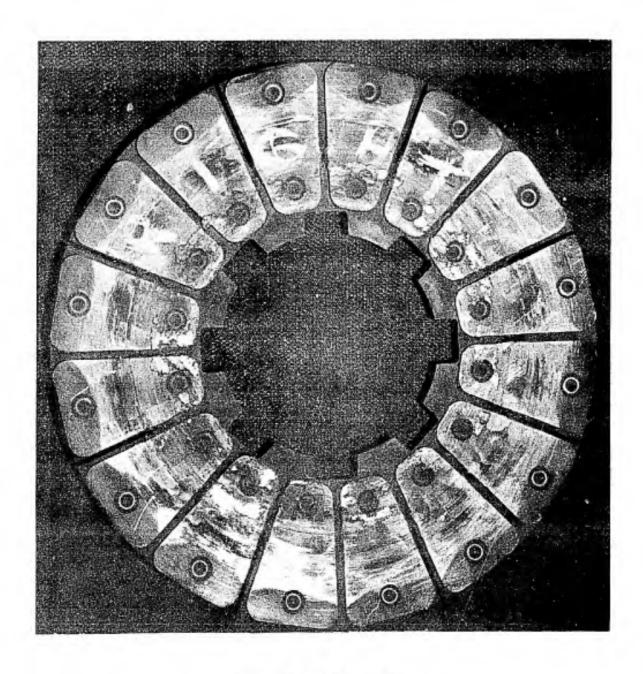


Figure 47 Brake Pressure Plate

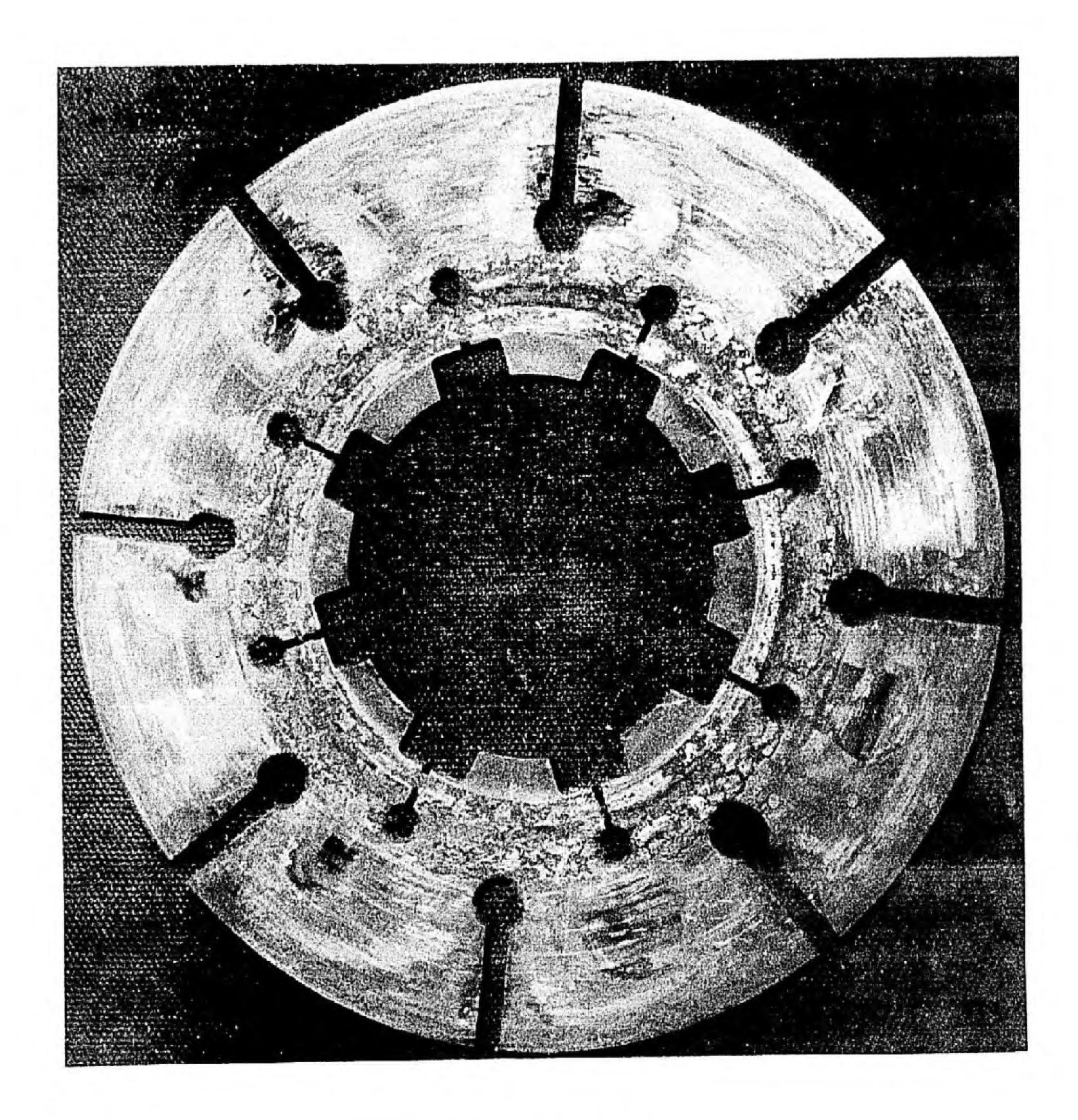


Figure 48 Brake Stator



Figure 49 Right BFG Tire (After Tests 37A, B)

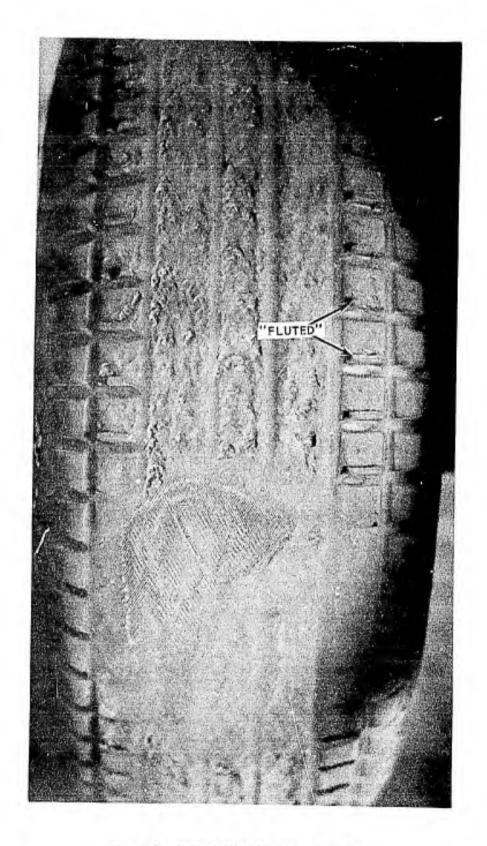


Figure 50 Left BFG Tire After Tests 37A, B)

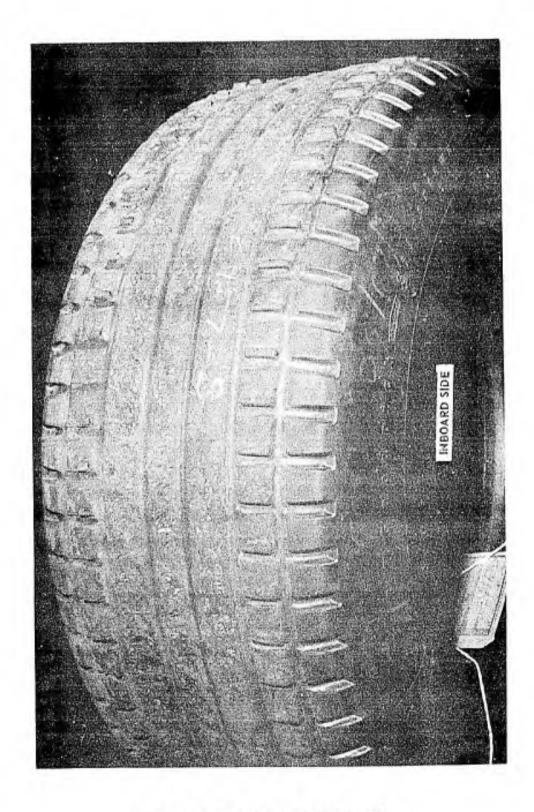


Figure 51 Right BFG Tire (After Test 47A)



Figure 52 Left BFG Tire (After Test 47A)

WET RUNWAY PERFORMANCE

STANDARD TIRE

A total of 21 test landings was performed on a wet runway using the Mark II antiskid system with the Standard tire. The test day conditions and stopping distances for these tests are shown in table 5. Six of these landings were done to establish a baseline stopping performance against which the performance of the other tires was compared. Six landings were done to investigate the effects of tire wear on stopping performance. A total of nine landings were made, touching down in the wet test section, to evaluate the effects of aircraft sink rate on wheel spinup. Since brakes were applied on these nine tests as soon as possible after wheel spinup, the stopping performance can be compared with the baseline performance. The standard day stopping performance and braking coefficient of friction for these Mark II antiskid/Standard tire combination tests are presented in figures Al3 to A24.

Table 5
MARK II ANTISKID, STANDARD TIRES, WET CONCRETE RUNWAY

FIL	Date	Test	Acft Gross Welght	Wind	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brake On (ft)	Energy Absorbed by Brakes (106 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b) 44.32
No.	(1973)	No.	(1b)	(kt)			157/70	7,802			42.32
	-	10A	40,350	-6.3	12.0	2,297	•	Wheel S	pindown	7,557	33.22
356	17 Mar	Lun		9 .1	13.9	2,253	149/	7,388	13,40	6,380	25.84
77	10 May	24A	42,936	-1.4 -1.4	17.5	2,254	141/25	6,222	13.05	•	38.78
		24B	37,786		20.8	2,257	132/26		10.98	8,408	28.01
		24C	33,636			2,288	148/63	7,210	13.45	6,308	
	11 May	25A	40,086	-2,2	15.5	2,282	132/24	5,161		11,622	49.84
79	II tout	2.5B	36,086	2.4	18.8		162/120	4,977	0.95	10,466	41.05
		2.00		-4.1	21.5	2,370	156/112	4,843	1.77	9,325	33.18
111	6 Jul	468	43,025		23.0	2,363	147/98	5,306	2.88		39.02
		48b	38,300		25.5	2,360		5,306	4.23	8,973	31.40
		49C			15.0	2,202	143/93	5,516	6.08	7,745 7,819	29.80
112	9 Jul	49A	43,200		19.5	2,197	135/76	5,972	5.84	·	45.52
***		49B	38,700	0.0	20.2	2,193	139/72		2.84	10,691	34.10
		49C	34,900	-0.9		2,276	154/104	5,674	4.19	9,016	30.19
		50A	43,500	-2.0	21.0	2,272	141/83	6,250	3.80	8., 563	
413	10 Jul	50B	38,700	-3.6		2,272	140/80	6,133		11,635	49.02
		50C	34,700	-4.4	26.5		160/95	7,441	4.73	9,570	36.93
					.19.0	2,304	147/68	7,648	6.73 8.18	9,083	31.30
415	11 Ju.	51A	38,350			2,302	143/57	7,833		10,76B	47.44
		51B				2,301			7.13	8,738	34.75
		510				2,228	157/	7,629	11.35	7,872	28.55
434	14 Se	D 67A	43,200			2,227	143/55	7,339	11.37	1,512	
43.		671		0 -5.5		2,226	137/39	.,			
		670	34,50	0 -1.	13.0						

		Standard	Day Condi	ions	Pct Tire Wear Before	Water Depth Before/After	Touchdown Ground	_	Spinup	Time
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-lb)	Flight After Flight	Landing (in.) 0.04/0.04	Speed (kt)	Sink Rate1 (fps)	L (sec	R
NO.	40,000	150	9,072	39.92	14 14	0.09/0.02				
24A 24B 24C	38,000	138 127	7,331 6,045	32.18 24.41	25 27	0.04/0.03				
25A 25B	40,000	133	7,999 6,303	36.82 28.07	34 30	0.05/0.05	172	7.0/4.6 9.0/4.6	4.80 3.75	3.80 1.95
48A 48B 48C	43,000 38,000 34,000	154 145 134	10,627 9,091 7,662	45.41 35.43 27.02	31 25	0.09/0.03 0.08/0.01 0.06/0.02	157	7.5/4.8 3.5/2.6 5.0/1.7	3.85	2.35 3.20 2.80
49A 49B 49C	43,000 38,000 34,000	142 132 134	8,777 7,260 7,110	38.16 29.44 27.07	31 31 31	0.07/0.02	148	5.0/3.4 2.6 1.0	 	1.95 2.20 3.2
50A 50B 50C	43,000 38,000 34,000	133	9,837 7,934 7,338	41.80 29.89 25.75	45 48	0.10/0.04	154 2 153	1.3		3.9
51A 51B	43,000	151 143	10,413 8,950 7,849		56 55	0.04/0.0	4			
51C 67A 67B 67C	43,000 38,000	151 135	9,857 7,700 6,792	43.19 30.43	59 64 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.06/0.0	3 2	at touchdow	ı. Sing	le

¹The first entry is the sink rate established on final approach; the second entry is the sink rate at touchdown. Single entries are touchdown sink rates.

Test 10A was the first on a wet test section using the Mark II antiskid and is of particular interest. Braking was initiated at 157 knots groundspeed. From the antiskid parameters in figure B8, one can see that the left wheel started to spin down immediately after brake application and had spun down to zero speed in approximately five seconds. The wheel remained in this locked-up condition for the entire braking run, approximately 7,800 feet. The wheel did not spin back up to aircraft speed after the brake pressure was released until it hit the dry pavement at the end of the wet section. The aircraft exited the test section at approximately 70 knots. Since there had been no plan to display wheelspeed in the aircraft during this test program, the aircraft crew and test team were not aware that one of the wheels had locked up until the crew chief inspected the tires after the braking test. The pilot indicated after the test that the aircraft directional control had not been degraded due to the one locked wheel and that the crew was unaware from aircraft response that the wheel was locked. The flat-spotted condition of the left tire after this test is shown in figure 53.



Figure 53 Left Standard Tire (After Test 10A)

The important fact to note is that the wheel lock-up did not occur due to a malfunction of the Mark II antiskid system. The control logic of the Mark II system compared the wheel deceleration to a fixed reference of 16 radians per second2. The system released the brake pressure when the wheel decelerated faster than this reference speed and then reapplied it when the deceleration again became less than the reference deceleration. There was a slight lag between when brake pressure was commanded and when it was applied due to the large hydraulic volume displacements required in the low brake pressure ranges of the initial braking. After the initial deep skid at brake application, the left wheel did not recover as quickly as the right wheel did. Brake pressure was reapplied before the left wheel had fully recovered to the aircraft speed. This resulted in another skid on the left wheel, and again the wheel did not recover very fast. As a result, the control logic reapplied the brake pressure before the left wheel had recovered to the speed it had before the second skid. This process continued until the wheel finally locked up, at which time, due to the paired wheel logic, the right wheel became the controlling wheel for the antiskid system. The so-called "locked wheel" detection circuitry of the Mark II system would not protect the aircraft against this kind of gradual wheel spindown. All it was designed to do was to command a full brake pressure release whenever the wheel deceleration was greater than 120 radians per second². Since "locked wheel" detection circuitry is a misnomer, a new name should be given to the circuit, and all references to it in T.O. 1F-4E-2-5 should be changed to reflect the new designation. In addition, on page 2-28 of the Flight Manual (reference 2), the sentence in the paragraph on Wet or Icy Runway Landing which states, "The antiskid system protects against a locked wheel and can effectively and safely produce the maximum deceleration possible for the existing runway conditions.", should be changed to the following: "Use of the antiskid system can produce the maximum deceleration possible for the existing runway conditions." (R 3), (R 2))

Because the locked wheel condition occurred on this test, it was decided that further testing of the Mark II antiskid system on a wet runway could be unsafe unless both of the wheel speeds were displayed in the Therefore, two ammeters were installed in the rear cockpit, as shown in figure 29, and utilized as wheel speed indicators. signal "isplayed was the same one that was picked off the J2 connector of the .tiskid control box and recorded on magnetic tape. Since the gauges were ammeters and only an approximate indication was required, lines denoting 0 and 100 knots speed were marked on the face of each gauge with a grease pencil. Because of the difference in magnitude of the signal for the two antiskid systems, a toggle switch was used to change the range on the meters when the antiskid system was changed. As an example of the value of having wheel speed indicators in the rear cockpit, on the very next test with the Mark II system on a wet runway (test 24A), another spindown occurred. Braking was initiated at 149 knots groundspeed, however, this time a locked wheel was prevented by release of the brake pressure when it was determined from the wheel speed gauges that the wheel was spinning down. This event is shown graphically in figure B9. system proved to be so extremely valuable, both in preventing an undetected locked wheel and for day-to-day "quick-look" evaluations, that its use, where practical, is recommended on future braking tests.

On one of the worn tire tests (51B), the left wheel again spun down to zero wheel speed when the brakes were applied at 147 knots groundspeed (figure Bl0). Brake pressure was released when the wheel reached zero speed. However, this time, after the wheel had spun back up to aircraft speed (about 1-1/2 seconds), brakes were reapplied by the pilot. Partial wheel spindowns at brake application occurred on all five remaining worn tire braking tests. The brakes were applied at groundspeeds which varied from 137 to 160 knots. The brake pressure was not released by the pilot during these tests and the wheel eventually recovered to aircraft speed as shown in figures Bl1 to Bl5. For the sink rate tests, partial wheel spindown occurred after brake application on two landings, tests 48A and 48B (figures Bl6 and Bl7). The brake application groundspeeds were 162 and 156 knots, respectively.

Because this spindown phenomenon occurs even with a correctly functioning Mark II antiskid, the following should be added to the Flight Manual under the CAUTION at the end of the Wet or Icy Runway Landing paragraph: (R 1)

Avoid using brakes above 130 knots on a wet or icy runway. When friction levels are low it is possible, even with a correctly functioning antiskid, for one or both wheels to partially spin down or lock up when brakes are applied at high speeds.

The sink rate tests were done to determine the effect on wheel spinup time of touching down in the wet test section at sink rates of 7 to 9, 3 to 5, and 1 to 3 feet per second. The vertical velocity gauge described earlier was used by the pilot to establish on final approach the desired sink rate for the 7 to 9 and 3 to 5 feet per second tests. For the 1 to 3 feet per second sink rates, the pilot attempted to "grease" the aircraft onto the runway. Because of the cushioning due to the ground effect, touchdowns of 7 to 9 feet per second were not obtained, even though these sink rates were established on final approach and an attempt was made by the pilot to hold this rate through the ground effect by pushing the aircraft nose down.

In the results shown in table 5, the first number in the sink rate column represents the approximate sink rate established on final approach and the second number was the touchdown sink rate. Both of these numbers were obtained from the phototheodolite data. On six of these tests, the left wheel speed was not recorded due to an instrumentation malfunction. However, it was determined from the wheel speed gauges in the rear cockpit that the spinup time for the left wheel was of the same order of magnitude as that for the right wheel. Brakes were applied after wheel spinup on all of these tests. Examples of the spinup are shown in figures B16 and B17. Comparison of the stopping performance from the sink rate tests with the baseline performance (figures A13, A15, and A17) shows a considerable difference. The differences may be attributable, in part, to the higher brakes—on speeds and resultant antiskid action, to the fact that the engines may not have had a chance to spin down to idle before brake application, and to tire wear.

Thirty-two landings were performed on a wet runway using the Mark III antiskid system and the Standard tire. The test day conditions and stopping distances for these tests are shown in tables 6 and 7. A total of nine landings was done to establish baseline stopping performance for the Mark III/Standard tire combination and, as described earlier, to tune the Mark III antiskid system to the F-4 aircraft. Eleven landings were done to investigate the effects of sink rate, as with the Mark II system. Three landings each were done to look at tire wear effects and the effect of wetting the test section with only water instead of the foam/water mixture. In addition, a total of six landings were done to look at the effect of changing the landing flap configuration: three with no flaps, and three with half flaps. The standard day stopping performance and braking coefficient of friction for all of these tests are presented in figures A25 through A37.

As a result of test 3A, as mentioned in an earlier section, the antiskid control valve was changed because it was suspected that it was out of tolerance. Unlike during the dry tests, however, the valve change apparently had an effect on the wet runway stopping performance. From figure A26, comparing the stopping distance at a kinetic energy which corresponds to 130 knots true airspeed shows that changing the valve produced a 1,150-foot shorter stopping distance or 18 percent improvement. Antiskid control valves with calibrations on the extremes of the tolerance band apparently produced this significant difference in wet runway stopping performance. Further tests should be accomplished to better define the affects that antiskid control valves with calibrations on the extremes of the tolerance band have on wet runway performance. (R7)

Also, as mentioned earlier, tests 5A, B, and C were performed before the Mark III antiskid system was "tuned". Again, as with the dry stopping performance, there was no noticeable effect on the overall stopping performance from the adjustments made to the control circuits (figure A25, A27, and A29). Typical operation of the Mark III antiskid with the Standard tire is shown in figure B18.

The sink rate tests done with the Mark III antiskid were done in the same manner and with the same limitations as previously described. On four of these tests (41A, 42A, 42B, and 43B), however, brakes were applied by the pilot before both wheels had fully spun up. From figures B19 through B22, one sees that the Mark III system performed well in these cases and allowed the wheel to eventually spin up to aircraft speed and did not spin any of them down. The on-again/off-again pilot-metered brake pressure at the beginning of test 42A (figure B20) occurred because the aircraft began to lift back off the ground as the pilot came back with the stick at brake application. The pilot pushed forward on the stick and released brake pressure; when the aircraft was firmly on the ground again he reapplied brakes and slowly brought the stick back to a full aft position.

Table 6
MARK III ANTISKID, STANDARD TIRES, WET CONCRETE RUNWAY

Flt	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brake On (ft)	Energy Absorbed by Brakes (105 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)
No.	.1.23	3A	39,200		9.0	2,140	144/30	7,490	19.30	7,770	35.99
350 351	24 Feb 3 Mar	5A 5B 5C	42,500 38,050 34,550	-3.1 -1.4 1.6	11.5 15.3 17.0	2,105 2,117 2,133	145/30 128/21 119/27	7,382 5,564 4,600	19.08 15.97 12.29	7,588 5,654 4,819	39.61 27.72 21.87
358	23 Mar	12A 12B	40,350	-6.5 -5.7	3.7	2,263 2,253	151/25 137/19	7,429 6,129	20.18 16.35	7,509 6,202	41.15 30.17
359	24 Mar	1 3A 1 3B 1 3C	42,200 37,875 34,400	-1.5 -3.0	4.0 7.0 9.0	2,119 2,112 2,108	142/31 139/25 128/28	6,952 6,487 5,212	18,13 16,13 13,21	7,200 6,655 5,391	38.23 32.80 25.06
404	23 Jun	41A 41B	42,350	0.0	15.9 20.0	2,272	151/85 140/66	6,498 5,925	6.37 9.22	9,863 7,194	42.61 32.82
405	25 Jun	42A 42B 42C	43,200 38,850 34,550	-3.0 -3.6	16.5 20.0 22.2	2,253 2,248 2,243	159/104 161/96 144/62	5,990 6,318 6,453	4.02 4.63 8.89	9,887 9,517 7,551	48.17 44.46 31.58
406	27 Jun	43A 43B 43C	43,000 38,375 34,700	-4.0 -7.6	22.0 25.0 29.0	2,302 2,302 2,302	162/108 160/94 142/70	6,109 7,218 6,410	2.67 4.70 7.97	10,671 10,379 7,819	50.02 43.36 31.15
407	28 Jun	44A 44B 44C	43,200 38,200 34,550	-4.1 -4.2	22.5 25.0 27.6	2,356 2,357 2,360	151/96 148/84 139/63	5,903 6,119 6,219	6.10 5.99 7.75	9,114 8,463 7,345	43.91 37.16 29.62
416	12 [°] Jul	52A 52B 52C	43,200 38,350 34,550	-4 -4.2	19.8 21.4 22.5	2,334 2,332 2,331	160/97 145/42 140/25	6,759 7,749 7,126	6.14 14.03 13.32	10,093 8,267 7,297	49.16 35.50 30.04
4 32	5 Sep	65A 65B 65C	42,500 38,500 34,500	0.0		2,278 2,277 2,277	147/19 142/25 132/20	7,276 6,324 5,676	20.93 17.59 14.32	7,356 6,441 5,748	40.95 34.39 26.83

		Standard	Day Condi	tions	Pct Tire Wear		. :			
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)	Before Flight After Flight	Water Depth Before/After Landing (in.)	Touchdown Ground Speed (kt)	Sink Ratel (fps)	Spinup (se L	
3A	40,000	134	6,93/	31.71	25 25	0.03/0.04				
5A 5B 5C	43,000 38,000 34,000	143 126 119	7,482 5,467 4,699	38.93 26.76 21.37	25 36 48	0.03/0.03 0.04/0.05 0.05/0.05				
12A 12B	40,000	147 133	6,979 5,817	38.00 28.12	14 30 9	0.02/0.01 0.04/0.02				
13A 13B 13C	43,000 38,000 34,000	145 138 127	7,545 6,558 5,191	40.00 32.22 24.08	30 9	0.04/0.01 0.07/0.03 0.03/0.01				
41A 41B	43,000	151 139	8,969 7,074	43.12 32.28	0 9 0 6	0.09/0.01	156 145	8.0/1.4 9.0/2.3	2.60	1.45
42A 42B 42C	43,000 38,000 34,000	154 153 137	9,275 8,458 6,753	45.06 39.37 28.15	9 6 12 12	0.09/0.05 0.09/0.02 0.09/0.01	169 165 149	4.5/2.9 6.0/3.6 5.5/3.0	- 2.90	2.40
43A 43B 43C	43,000 38,000 34,000	155 148 131	9,785 8,844 6,506	45.70 36.68 27.75	12 12 12	0.10/0.05 0.09/0.04 0.09/0.02	172 160 150	4.0/2.3 4.5/1.1 4.5/1.5	5.85 7.20 3.40	4.05 2.00 2.50
44A 44B 44C	43,000 38,000 34,000	144 140 129	8,211 7,534 6,285	39.40 32.94 25.22	12 12 19	0.09/0.01 0.09/0.02 0.09/0.03	168 160 151	1.4 3.1 2.0	6.00 4.70 4.25	5.95 3.70 4.10
52A 52B 52C	43,000 38,000 34,000	153 137 132	9,336 7,388 6,421	44.30 31.58 26.31	56 56 62 62	0.03/0.01 0.04/0.02 0.05/0.03				
65A 65B 65C	43,000 38,000 34,000	148 141 131	7,526 6,232 5,508	41.90 33,28 25.72	6 6	0.03/0.01 0.04/0.02 0.08/0.02				

The first entry is the sink rate established on final approach; the second entry is the sink rate at touchdown. Single entries are touchdown sink rates.

Table 7
MARK III ANTISKID, STANDARD TIRES, WET CONCRETE RUNWAY

Flt	Date	Tost	Acft Gross Weight	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brake On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)
No. 408	(1973) 2 Jul No Flaps		(1b) 43,200 38,550	0.0	18.0 20.5 22.0	2,315 2,312 2,305	170/142 161/129 156/118	5,641 5,759 5,725	4.81 5.02 6.69	55.30 44.30 37.34
409 H	3 Jul alf Flaps	45C 46A 46B	34,700 43,200 38,375 34,700	-3.0 -0.4 -0.4	17.8 19.4 22.5	2,240 2,238 2,238	158/115 155/114 145/88	5,896 5,828 6,090	13.04 9.77 13.26	48.08 41.11 32.30

	Test	, , ,		Water Depth Before/After Landing (in.)	Touchdown Ground Speed (kt)	Sink Rate ^l (fps)	Spinup (se L	
-	45A 45B 45C	19 19	/22	0.09/0.06 0.06/0.02 0.06/0.01	177 172 168	1.7 1.4	5.35 5.00	4.35 5.00 4.15
	46A 46B 46C	25 22	25	0.09/0.03 0.06/0.03 0.06/0.04	169 165 155	2.4 2.6 2.2	4.55 5.50 5.05	2.40 1.85 2.95

¹ These are touchdown sink rates.

Another point of interest was the unintentional application of a small amount of pilot-metered brake pressure on both brakes prior to brake application during the touchdown on test 42B (figure B21). The pilot was carrying a slight amount of left rudder at touchdown on this landing. The technique he used was to operate the rudder using the balls of the feet and sliding the heels on the floor of the cockpit. At touchdown, the pilot moved his feet up to where his heels were on the rudder bar and his feet were ready for brake application. The position of the pilot's feet at the time of this small pressure input is unknown since it occurred in the region of transition from one position to the other. This small amount of pressure on the left brake was sufficient to cause the left wheel to skid and slow down its spinup considerably. In addition, the pilot was unaware of this small pressure input, and, as with all test landings, was making a conscious effort to avoid applying pressure prior to intended brake application. A few days prior to this incident while flying around to cool the brakes, data was recorded while the pilot went through full rudder pedal travel, both left and right. The results are shown in figure B23. The technique he used was the same as described above; the balls of his feet on the rudder bar and his heels on the floor of the cockpit. He was completely unaware of the pilot-metered brake pressure which occurred during both the full left (approximately 600 psi) and full right (approximately 200 psi) rudder pedal travel. more inflight tests were done similar to this test, one with another pilot. These failed to produce any pilot-metered brake pressure. The results indicated that it was possible to unintentionally apply brake pressure while operating the rudder.

Two of the longer wheel spinups resulting from the sink rate tests occurred on tests 43A and 44A (figures B24 and B25). Comparison of the stopping performance from the Mark III sink rate tests with the Mark III baseline performance (figures A25, A27, and A29) shows, as with the Mark II, a considerable difference in stopping distance. Again, the reasons are unknown, and the comments made in the Mark II discussion apply here as well.

Comparison of the stopping performance results, as shown in figure 54, reveals that use of the Mark III antiskid system with the Standard tire provided a considerable improvement in stopping distance over that of the Mark II/Standard tire combination. At 38,000 pounds gross weight, this improvement was 800 feet or 12 percent, and was 700 feet or 13 percent at 34,000 pounds gross weight. From figures A20 and A31, the average braking coefficient of friction developed for the Mark II/Standard tire combination varied from 0.03 at 120 knots to 0.19 at 40 knots, and with the Mark III/Standard tire combination, varied from 0.06 to 0.23 over these same speeds.

The effect of tire wear on the overall stopping performance of the Standard tire at an aircraft gross weight of 38,000 pounds is illustrated in figures 55 and 56. With the Mark II antiskid system, the degradation in stopping distance when the tire wear was increased from approximately 20 percent to 65 percent was 700 feet, or approximately an 11 percent degradation. With the Mark III antiskid system, when the tire wear was increased from approximately 30 percent to 60 percent, the stopping distance was degraded by 900 feet, or approximately 16 percent.

The six landings done to determine the effects of landing with half flaps and no flaps on the wet runway stopping performance were inconclusive. Since the aircraft exited the wet test section at such a high speed, no meaningful stopping distances could be extrapolated. Also, from the antiskid parameter traces (figures B26 to B31), it can be seen that full pilot-metered brake pressure was applied throughout the braking run on only two of these landings, test 46A (figure B29) and test 46C (figure B31). The other landings had reductions in pilot-metered pressure to varying degrees throughout the test. In fact, on test 45A (figure B26), the pilot-metered pressure was at half of full value for the entire test. Some of these reductions in pilot-metered pressure resulted in negligible pressures at the brakes. This also occurred on two of the BFG tire tests and is discussed further in that section of this report.

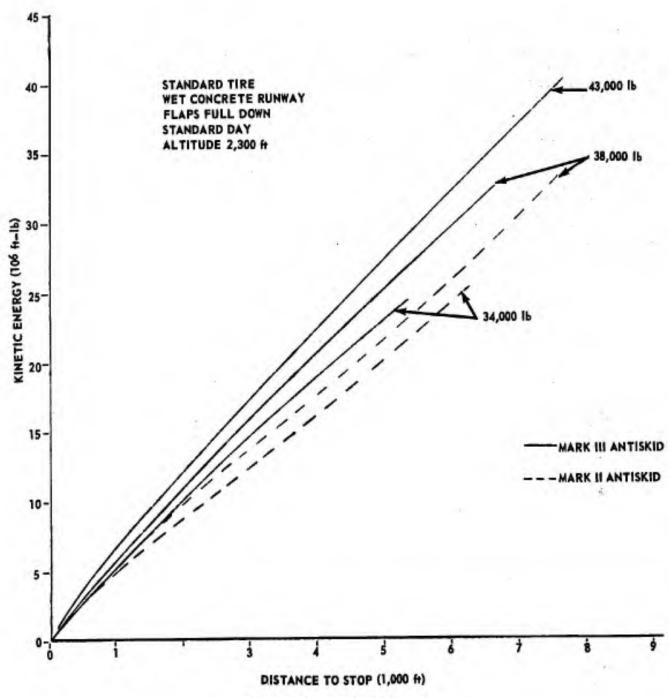


Figure 54 Standard Tire Performance

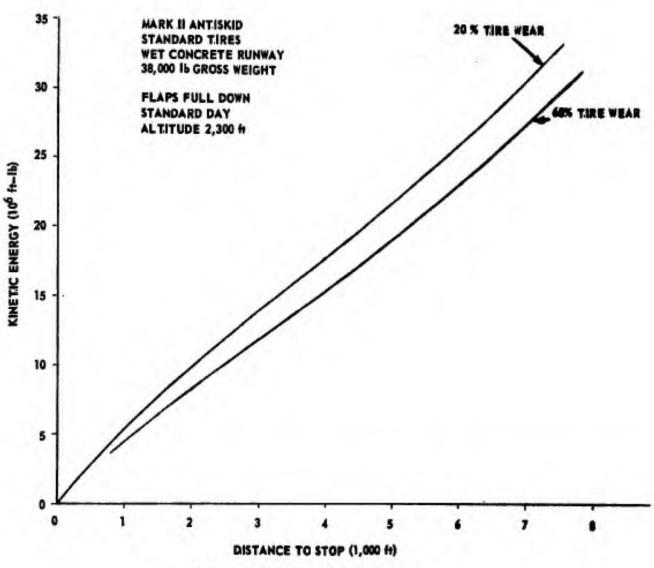


Figure 55 Worn Standard Tire Performance

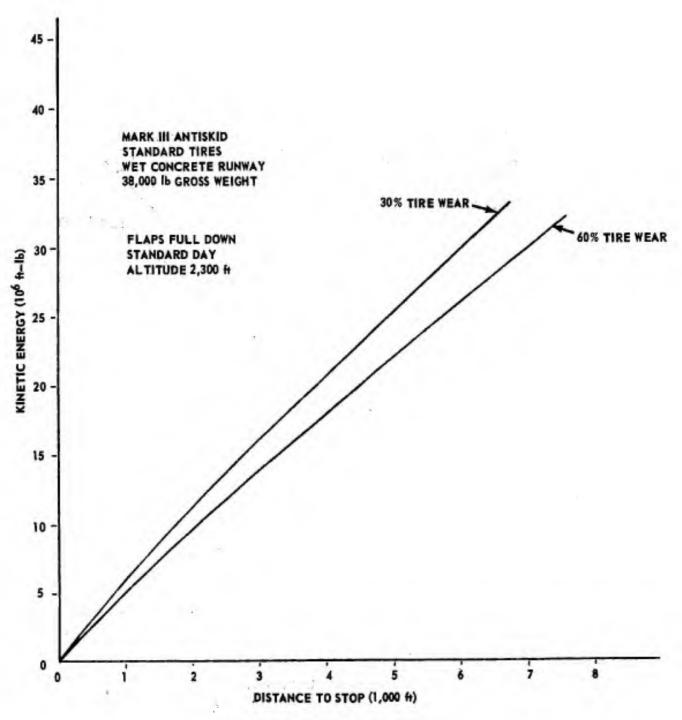


Figure 56 Worn Standard Tire Performance

SOMMERS TIRE

A total of 41 test landings was performed on a wet runway using the Sommers tire, 20 with the Mark II antiskid system and 21 with the Mark III antiskid system. Ten landings, five using each antiskid system, were initially performed for comparison with the stopping performance of each of the other new tire designs. From this comparison, it was determined that the Sommers tire provided the best stopping performance on a wet runway. Since the tire giving the best stopping performance was to be used in conjunction with the Standard tire results to determine the effect of sink rate on the wheel spinup, 18 landings (9 using each antiskid) were made ir the wet test section varying the touchdown sink rate. In addition, seven landings, three with the Mark II and four with the Mark III, were made to examine the effects of tire wear on the stopping performance. The test day conditions for all of these tests are given in tables 8 and 9. The standard day stopping performance and braking coefficient of friction data are shown in figures A38 through A56. Typical operation of the Mark II antiskid (test 27B) and Mark III antiskid (test 28B) with the Sommers tire is shown in figures B32 and B33, respectively.

Table 8
MARK II ANTISKID, SOMMERS TIRES, WET CONCRETE RUNWAY

Flt No.	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brake On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-lb)
380	12 May	26A 26B	39,436 35,786	-2.3 -1.0	15.8 19.0	2,272 2,272	152/27 139/23	7,249 6,011	18.49 15.70	7,394 6,123	40.27 30.50
361	15 May	27A 27B 27C	43,200 38,350 34,550	-3.5 -5.7 -5.2	12.1 14.2 16.0	2,073 2,067 2,063	148/34 143/22 135/16	6,696 6,238 5,450	21.82 19.58 16.62	6,933 6,322 5,493	41.96 34.76 27.86
20	18 Jul	56A 56B 56C	43,250 38,700 35,200	-4.0 -4.8 -4.4	17.5 19.6 21.0	2,266 2,260 2,253	159/100 148/47	5,842 No 6,875	6.46 Askania Data 13.26	9,039 7,353	48.73 34.15
21	19 Jul	57A 57B 57C	43,200 38,300 34,550	-4.3 -4.9 -6.6	18.3 18.3 21.1	2,229 2,228 2,225	158/93 148/64 147/58	6,094 6,514 6,744	7.67 11.93 10.65	8,755 7,674 7,699	47.65 37.10 33.14
26	4 Aug	61A 61B 61C	42,900 38,150 34,300	+0.1 -0.7 -1.2	22.2 23.9 23.9	2,228 2,226 2,225	147/88 145/78 144/61	5,931 6,320 6,497	6.18 6.74 8.57	8,826 8,493 7,604	41.22 35.37 31.41
23	28 Jul	58A 58B 58C	43,500 38,550 34,550	-3.7 -2.4 -2.8	17.8 20.0 22.8	2,274 2,271 2,268	156/81 146/55 138/27	7,856 7,960 7,464	9.18 10.13 12.42	10,282 8,922 7,681	47.17 36.30 29.21
35	17 Sep	68A 68B 68C	42,600 37,800 34,100	-2.1 -4.8 -2.1	10.0 12.2 15.0	2,190 2,185 2,183	153/ 141/22 136/20	6,880 6,327	15.36 13.75	8,174 6,977 6,416	44.38 33.35 27.76

			Standard	Day Condi	LIONS	PCt Tire Wear						
	Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)	Before Plight After Flight L R	Water Depth Before/After Landing (in.)	Touchdow Ground Speed (kt)	sink Rate ¹ (fps)		p Time ec)	
	26A 26B	40,000	149 136	7,264 5,941	39.47 29.57	0 6 0 6	0.03/0.02 0.05/0.02					
	27A 27B 27C	43,000 38,000 34,000	144 137 128	6,583 5,731 4,894	39.69 31.33 24.68	6 6 10	0.07/0.02 0.04/0.02 0.08/0.05					
	56A 56B 56C	43,000 36,000	153	8,329 7,018	44.73 32.45	11 12 14	0.06/0.04 0.04/0.04 0.06/0.04	168 153	9.0/3.5 7.0/3.9	2.70 2.05 2.45	1.75 0.95 0.95	
	57A 57B 57C	43,000 38,000 34,000	151 141 137	8,033 6,925 6,617	43.54 33.32 28.28	15 14	0.04/0.03 0.03/0.04 0.04/0.06	162 150 152	6.0/3.4 8.0/2.8 6.0/4.0	2.15 1.70 2.05	1.35 1.45 1.65	
	61B 61C	43,000 38,000 34,000	145 141 139	8,545 7,987 7,035	39.92 33.23 29.02	23 23 28	0.06/0.02 0.09/0.03	155 153 150	9.0/4.2 8.0/3.5 7.0/3.9	4.45 3.50 2.90	1.70 1.80 2.00	
	58A 58B 58C	43,000 38,000 34,000	150 140 132	9,374 8,141 6,870	42.85 33.04 26.05	50 50 56	0.03/0.02 0.09/0.06 0.05/0.03					
	68A 68B 68C	43,000 38,000 34,000	152 137 133	8,161 6,601 6,118	44.22 31.39 26.40	0 0 5	0.09/0.04 0.05/0.02 0.09/0.02	162 146 141	2.2 3.0 3.2	2.35 1.76 1.40	2.05 1.45 1.25	

¹The first entry is the sink rate established on final approach; the second entry is the sink rate at touchdown. Single entries are touchdown sink rates.

Table 9

MARK III ANTISKID, SOMMERS TIRES, WET CONCRETE RUNWAY

Flt	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brake On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)
382	16 May	28A 28B 28C	43,500 38,500 34,450	-2.5 -2.0	12.6 16.9 17.7	2,060 2,055 2,051	153/44 139/25 131/25	6,811 5,731 4,622	20.54 18.37 15.81	7,246 5,841 4,73B	45.34 33.04 26.18
383	17 May	29A 29B	40,500 36,375	-5.2	16.6 18.7	2,126 2,122	152/27 138/21	7,297 5,647	20.62 17.80	7,441 5,721	41.27 30.82
417	13 Jul	53A 53B 53C	43,200 38,200 34,550	-3.1	16.5 19.0 21.0	2,333 2,332 2,332	158/86 148/24 149/43	5,779 6,057 6,113	12.67 20.31 15.39	7,714 6,173 6,529	47.96 36.92 33.79
418	16 Jul	54A 54B 54C	43,200 38,550 35,050	-6.6 -6.3	17.2 18.5 21.3	2,291 2,287 2,286	163/82 153/39 150/23	6,154 6,574 6,530	14.05 20.55 18.63	7,933 6,923 6,609	50.95 39.93 34.75
419	17 Jul	55A 55B 55C	43,200 38,350 34,400	-6.4	17.0 22.0 22.5	2,289 2,287 2,285	156/64 150/25 145/16	6,278 6,455 6,038	18.98 21.28 18.39	7,225 6,575 6,080	46.27 38.03 32.06
424	28 Jul	59A	43,350	-3.5	35.0	2,308	160/86	7,654	8.99	10,418	49.13
436	21 Sep	69A 69B	43,300 38,500	-5.5	12.8 13.6 15.1	2,248 2,243 2,240	154/78 144/41 134/24	7,403 7,575 6,869	10.67 14.05 13.13	9,493 8,047 6,978	45.44 35.53 27.42

		Standard	Day Condi	tions	Pct Ti							
Test No.	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft- <u>lb</u>)			Water Depth Before/After Landing (in.)	Touchdown Ground Speed (kt)	Sink Rate ¹ (fps)		p Time ec) R	
28A 28B 28C	43,000 38,000 34,000	150 135 127	6,876 5,460 4,373	42.92 30.82 24.10	10 25	10	0.05/0.02 0.04/0.02 0.08/0.05					
29A 29B	40,000 36,000	145 132	6,699 5,182	36.97 27.79	25 35	25 35	0.04/0.02 0.05/0.04					
53A 53B 53C	43,000 38,000 34,000	153 142 139	7,172 5,693 5,632	44.44 33.94 28.96	0,	0	0.09/0.02 0.09/0.02 0.09/0.04	163 151 151	8.5/5.3 8.0/5.7 6.0/3.3	-	0.35 0.30 0.90	
54A 54B 54C	43,000 38,000 36,000	154 144 142	7,114 6,048 6,114	45.41 34.66 31.90	0/6	0	0.06/0.06 0.05/0.06 0.06/0.05	169 157 154	4.5/2.1 6.0/2.0 4.5/1.5	=	1.20 1.05 1.60	
55A 55B 55C	43,000 38,000 34,000	148 140 134	6,570 5,720 5,178	41.86 32.87 27.09	6 11	6	0.04/0.02 0.03/0.04 0.06/0.04	167 157 150	1.7 2.7 1.3	3.60 2.95 2.20	2.25 1.90 1.80	
59A	43.000	150	9,052	42.55	57	56	0.02/0.01					
69A 69B 69C	43,000 38,000 34,000	148 137 126	8,751 7,222 6,161	41.68 31.70 24.03	44 46	47	0.09/0.03 0.08/0.02 0.09/0.01					

¹The first entry is the sink rate established on final approach; the second entry is the sink rate at touchdown. Single entries are touchdown sink rates.

The summary plot (figure 57) shows that use of the Mark III antiskid system provided a slight improvement over use of the Mark II system in the stopping performance of the Sommers tire. The difference in stopping distance at 43,000 pounds gross weight was 250 feet, and at 34,000 pounds was 300 feet, which represents improvements of 4 percent and 7 percent, respectively. This improvement in stopping performance is considerably less than that shown when the Mark III was used with the other tires tested. This difference in stopping improvement may be the result of tire wear, however, since the tires used with the Mark III system were approximately 20 percent worn, and those used with the Mark II system were only about 8 percent worn. The average coefficient of friction developed with the Mark II system (figure A44) varied from 0.06 at 120 knots groundspeed to 0.24 at 40 knots, and with the Mark III system (figure A54) varied from 0.07 to 0.25 over the same speed range.

The stopping performance of the Sommers tire on a wet runway was considerably better than that of any other tires tested. With both the Mark II and Mark III antiskid systems, there was a substantial improvement in stopping distance when compared with the Standard tire performance (figures 58 and 59). The stopping distance with the Mark II system was 5,150 feet at a gross weight of 38,000 pounds and a true airspeed of 130 knots. This is a 22 percent improvement in stopping distance compared with that of the Standard tire. With the Mark III system, at the same aircraft gross weight and true airspeed, the stopping distance was 4,800 feet, which is an improvement of 17 percent over that of the Standard tire. However, comparing the Mark III/Sommers tire performance with that of the Mark II/Standard tire, there was a difference in stopping distance of 1,800 feet which is a 27 percent improvement.

Although the improvement in stopping performance was dramatic when the Sommers tire was used, there appeared to be a substantial degradation due to tire wear (figures 60 and 61). Again making a comparison at an aircraft gross weight of 38,000 pounds and 130 knots true airspeed, with the Mark II system, there was a 2,000-foot difference in stopping distance between tire wears of approximately 8 percent and 53 percent. This represents a degradation in stopping performance of about 39 percent. With the Mark III system the difference was 1,600 feet between the stopping distance of a tire with approximately 20-percent wear and one with 45-percent wear. This was a degradation in stopping performance of 33 percent. Comparing these results with the 60-percent worn Standard tire results shows that there was essentially no difference between the stopping performance of the two tire tread designs when the tires were worn. The Sommers tire stopping performance would be expected to approach that of the equivalently worn Standard tire as the tread wear increased since the Sommers tire tread was essentially the Standard tire tread with knife cuts across it.

The sink rate tests were done in the same manner as those done with the Standard tire. The sink rates and spinup times are tabulated in tables 8 and 9, and examples of the wheel spinup are presented in figures B34 through B37 for tests 55A, 55B, 56A, and 68B. On six of the tests with the Mark III system, the left wheel speed was not recorded due to an instrumentation malfunction. However, from the wheelspeed gauges in the rear cockpit, the spinup times for the left wheel were of the same order of magnitude as those for the right wheel. Comparison of the spinup times of the Sommers tire with those of the Standard tire show that, in general, the spinup times were shorter with the Sommers tire.

Comparing the Mark II/Sommers tire combination stopping performance exhibited during the sink rate tests with that resulting from the initial tire comparison tests (figures A38 through A42), reveals the same type of difference between the two as was exhibited by the Standard tire results and discussed earlier. Again, the reason for this difference is unknown. The inconsistency shown by the results from test 61A, 61B, and 61C compared with the data from the other sink rate tests was believed due to having entirely new brakes which were not "burned in" prior to the test series. The brakes were deliberately not "burned in" to determine what effect new brakes would have on the wheel spinup times and wet runway stopping performance. As shown graphically in figures B38, B39, and B40, the left wheel partially spun down on two of the three tests in the flight. The first section in each figure shows the after-takeoff free spindown of each wheel recorded during the takeoff just prior to

the braking test depicted. Figure B41 is typical of the takeoff free spindown which occurred during the rest of the test program. The dragging effect of the new brakes is graphically depicted by comparing the spindown in this figure with the other takeoff free spindowns in figures B38 through B40. The free spindown times for the left wheel prior to tests 61A, 61B, and 61C were approximately 3, 12, and 5 seconds, respectively. The typical free spindown times during the test program ranged between approximately 15 and 25 seconds.

Another instance of a dragging brake occurred a few days previously on test 60A. The results are shown in figure B42. Again entirely new brakes had been installed for this flight. The intention was to use the first landing to "burn in" the brakes. On the initial takeoff, the left wheel free spindown was extremely rapid, (approximately 1-1/2 seconds) compared with the right wheel spindown of approximately 13 seconds. For the landing, touchdown was made in the wet test section with a final approach sink rate of 8 feet/second. The left wheel did not spin up to aircraft speed; therefore, brakes were not applied and the decision was made to go around. As the go-around was initiated, the left wheel finally spun up to aircraft speed. The free spindown after liftoff was again approximately 1-1/2 seconds. The cause of the dragging brake on test 60A is uncertain. Whether it was an effect of just having new brakes, per se, or whether it was a result of not properly reseating the grip tubes on the brake pistons during brake installation, or perhaps some other factor could not be determined. However, for tests 61A, B, and C, it was determined that the grip tubes had been reseated in accordance with T.O. procedures.

After going around on test 60A, the decision was made to land on the dry side of the runway to "burn in" the brakes. On touchdown, both wheels spun up immediately to aircraft speed. Moderate braking, without any cycling of the antiskid system, was used to stop the aircraft in about 7,000 feet. After coming to a stop, the pilot did not release the brakes. Normal practice had been to release brakes at about 20 knots and roll a few hundred feet before reapplying them to hold the aircraft while the crew chief inspected the tires. A flicker of flame was noticed in the left brake by the crew chief; therefore, the decision was made to not take off and air cool the brakes. When the pilot advanced the throttles to taxi back to the hot gun line, the aircraft did not move because both brakes had fused.

Examination of the brakes revealed that one rotor and one stator had fused together in the right brake. They were broken apart during removal from the wheel and exhibited the mix (sintered metal) transfer shown in figures 62 and 63. In the left brake, two rotors and two stators had fused together, and they could not be broken apart.

In addition to the partial spindowns exhibited on tests 61A and 61C, one or both of the Sommers tires partially spun down on all three of the tests performed to determine the effects of worn tires on the stopping performance with the Mark II antiskid (tests 58A, 58B, and 58C). The antiskid parameters depicting these spindowns are shown in figures B43 through B45.

The Mark III/Sommers tire combination stopping performance obtained during the sink rate tests, when compared with that from the initial tire tests (figures A48 through A52), shows that, unlike the results of the Standard tire and the Mark II/Sommers tire tests, there was essentially no difference in the stopping performance. Since tire wear had such a large effect on the stopping performance of the Sommers tire, as discussed earlier, this lack of difference in stopping performance may be due to The sink rate tests with the Mark-III antiskid were all done tire wear. with relatively new tires with wear ranging between 0 and approximately 12 percent. However, tests 28A, B, and C, and tests 29A and B were done with tires having 10 to 35 percent wear. If these initial tire comparison tests had been done with new tires, there might have been a further improvement in the stopping performance with the Mark III antiskid. This would have caused a difference in performance similar to that shown between the sink rate and tire comparison tests for the Mark II/Sommers tire combination.

Since the Sommers tire exhibited the best stopping performance, documentation of the condition of the tire at various points in the test program was made. Figures 64 and 65 show the condition of the tires after use on test series 26, 27, 28, and 29. The tire wear at this point was approximately 35 percent. Figures 66 and 67 show the condition of these same tires prior to their use on test series 58 and 59 and show a wear of approximately 50 percent. Figures 68 and 69 show the condition of these same tires after the worn tire test series 58 and 59. The wear at this point is approximately 57 percent. The chunk pulled out of the left tire occurred on test 59A and goes all the way down to the cord. This was the only occasion on which this chunking occurred with the Sommers tire. Figures 70 and 71 show the condition of a different set of tires after use on test series 68 and 69 and show approximately 50 percent tire wear.

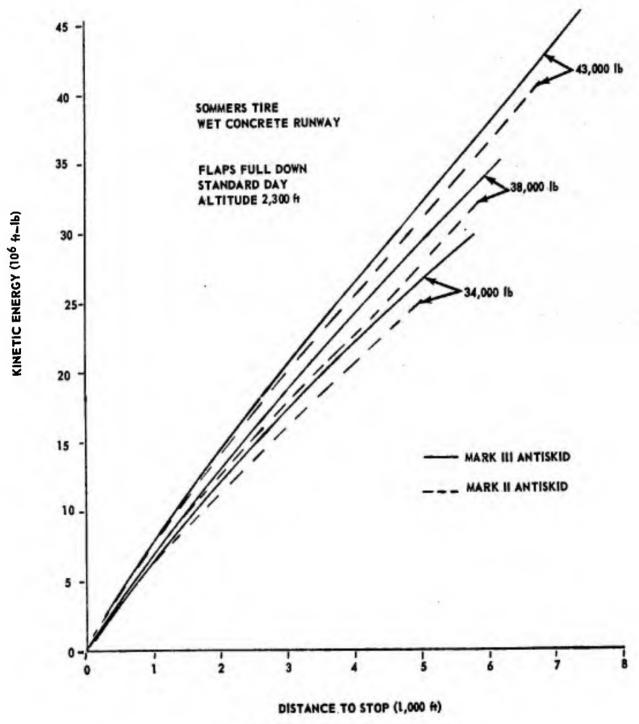
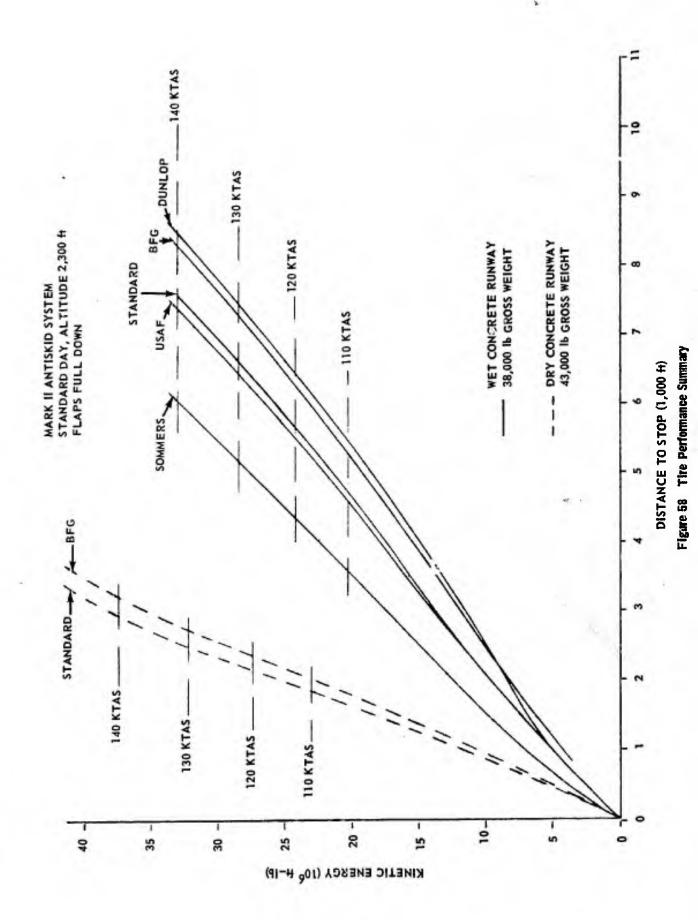


Figure 57 Sommers Tire Performance



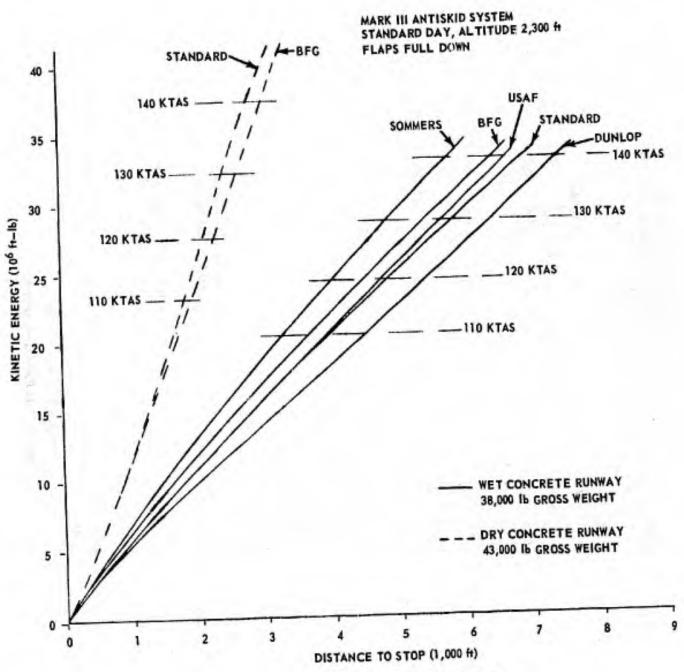


Figure 59 Tire Performance Summary

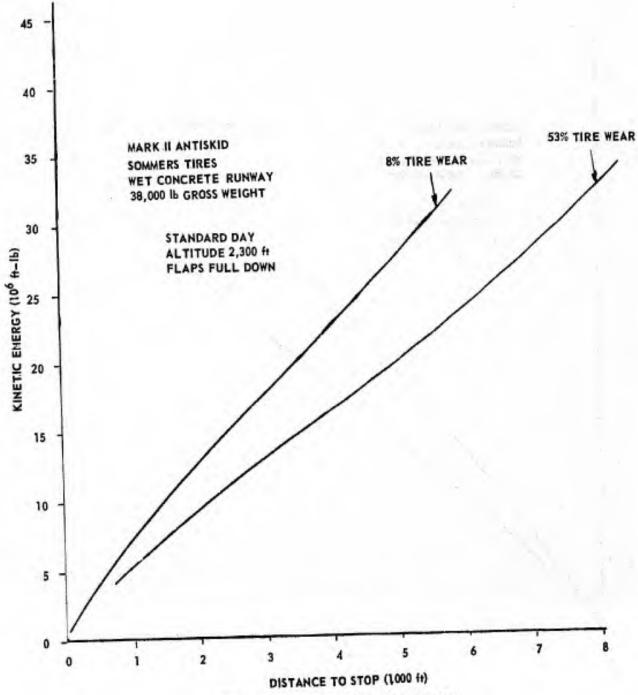


Figure 60 Performance of Worn Sommers Tire

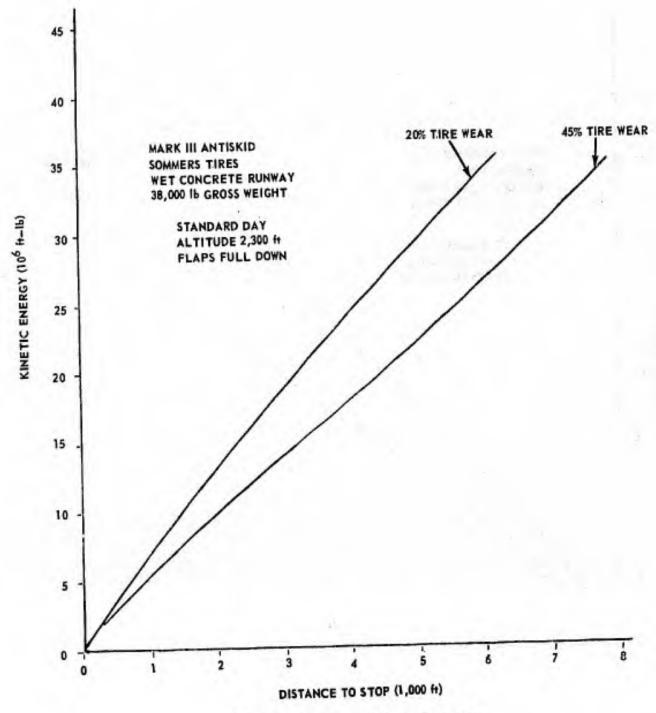


Figure 81 Performance of Worn Sommers Tire



Figure 62 Brake Rotor



Figure 63 Brake Stator



Figure 64 Right Sommers Tire (After Test Series 26, 27, 28, 29)



Figure 65 Left Sommers Tire (After Test Series 26, 27, 28, 29)

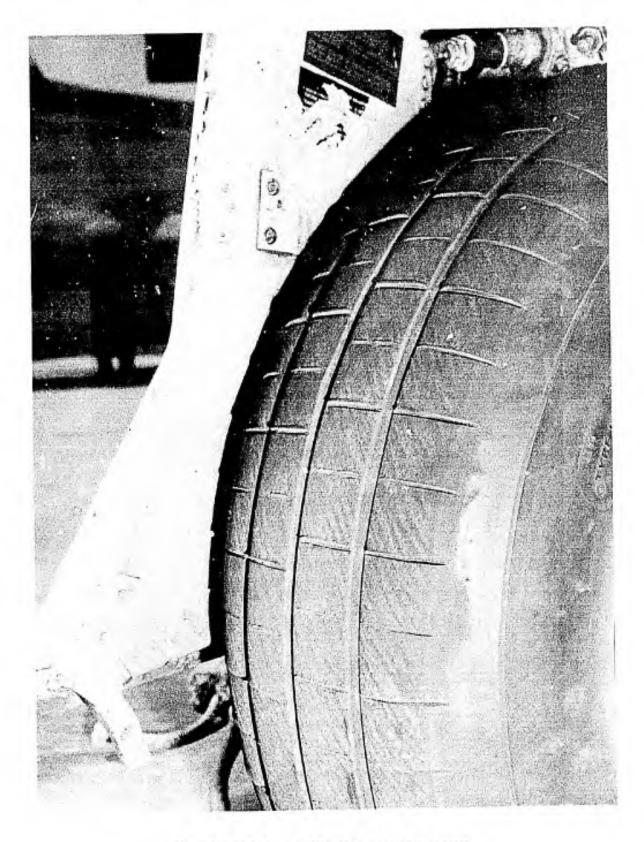


Figure 66 Right Sommers Tire (Before Worn Tire Tests)



Figure 67 Left Sommers Tire (Before Worn Tire Tests)

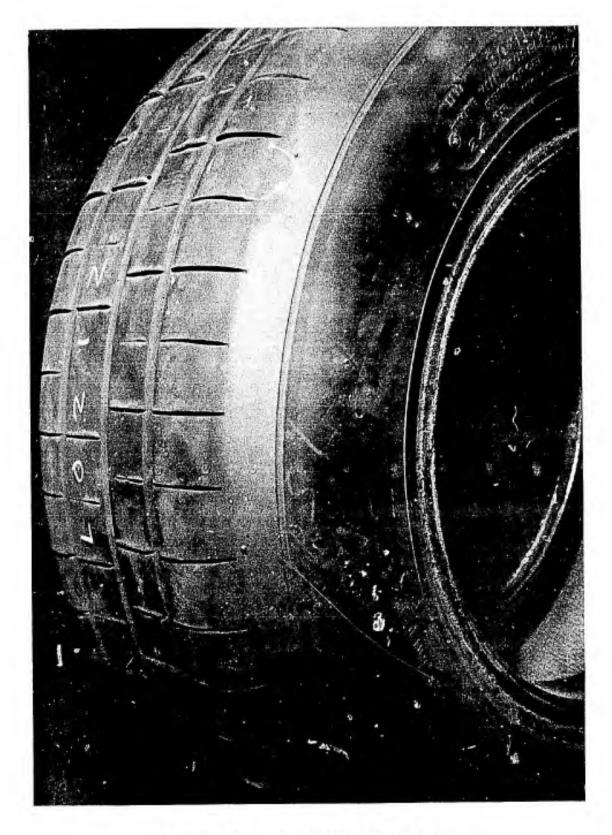


Figure 68 Right Sommers Tire (After Worn Tire Tests)

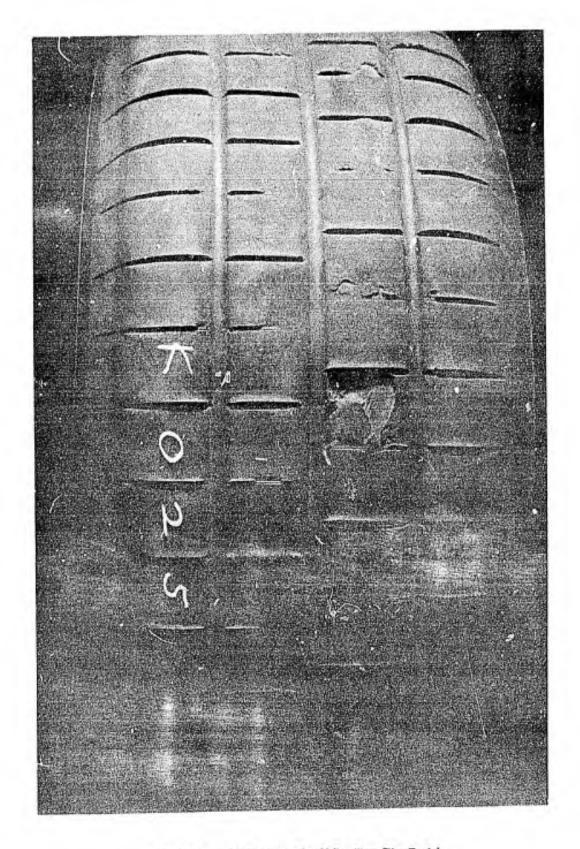


Figure 69 Left Sommers Tire (After Worn Tire Tests)

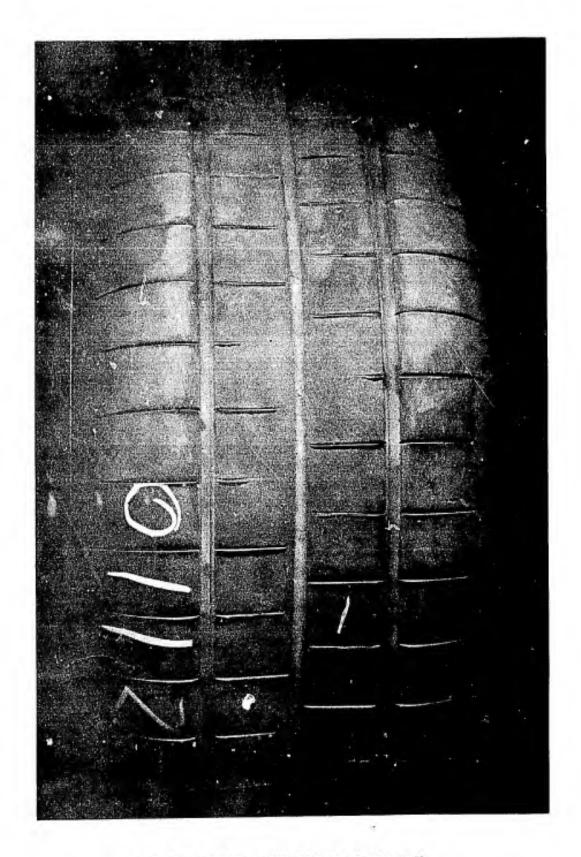


Figure 70 Right Sommers Tire (After Tests 69A, B, C)

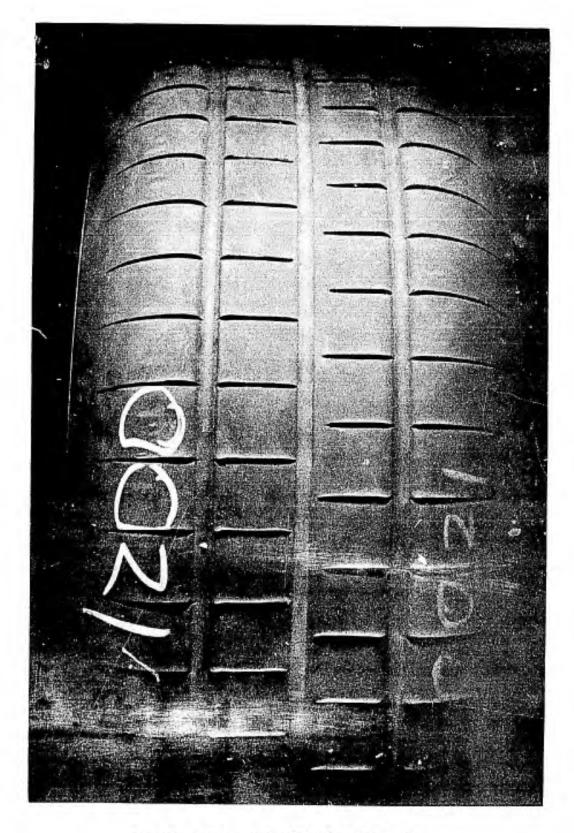


Figure 71 Left Sommers Tire (After Tests 69A, B, C)

BFG TIRE

Thirteen landings were performed on a wet concrete runway using the BFG tire, five with the Mark II antiskid and eight with the Mark III antiskid. The test conditions are shown in tables 10 and 11. Tests 38A, 38B, and 38C were done using only water to wet the test section instead of the foam/water mixture and are discussed in another section of this report. The standard day stopping performance and braking coefficient of friction data for all the other wet runway tests with the BFG tire are presented in figures A57 through A60.

Table 10 MARK II ANTISKID, BPG TIRES, WET CONCRETE RUNNAY

Flt No.	Date (1973)	Test	Acft Gross Weight (1b)	Mind (kt)	Amblent Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Extrapolated Stopping Distance (ft)	Kimetic Energy at Brakes On (10 ⁵ ft-1b)
391	27 May	32A 32B	40,200	2.0	25.6 27.0	2,235	128/30 125/22	7,446 6,930	13.58	7,753 7,081	29.27 35.44
396	31 May	36A 36B 36C	43,350 38,550 35,400	-6.7 -6.1 -6.7	15.3 17.0 18.0	2,417 2,414 2,413	156/78 145/56 138/38	7,596 7,752 7,836	10.98 11.67 12.72	10,211 8,988 8,257	46.48 36.04 30.07

	-	Standard	Day Condi	Pot Ti	re Wear			
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)	Hefore Flight		Water Dopth Before/After Landing (in.)	
32A 32B	40,000	127 122	7,515 6,585	28.44 23.68	18/23	14/14	0.05/0.02	
36A 36B 36C	43,000 38,000 36,000	147 136 131	9,061 7,847 7,550	40.98 31.26 27.29	21 30	21 12	0.06/0.02 0.09/0.02 0.05/0.01	

Table 11
MARK III ANTISKID, BFG TIRES, WET CONCRETE RUNWAY

Fit	Date (1973)	Yest No.	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (106 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)
366	8 Apr	17A 17B	40,350 36,200	3.4	11.0	2,055	127/26 127/24	5,469	15.77 13.20	5,637 5,596	29.02 25.69
366	8 Apr	18A 18B 18C	42,850 37,875 34,550	8.1 5.8 9.5	15.8 16.2 16.5	2,017 2,012 2,010	139/25 132/23 108/20	6,141 5,571 3,488	17.71 14.61 10.96	6,269 5,692 3,583	36.68 29.23 17.86
400	1) Jun	38A 38B 38C	43,200 38,200 34,225	-4.8 -6.0 -7.3	15.5 18.5 22.0	2,381 2,381 2,383	155/68 151/46 140/59	7,335 7,682 6,214	13.72 15.79 10.70	8,737 8,160 7,215	45.14 36.52 29.86

		Standard	Day Condi	Pet Tir	e Mear		
Tost	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁵ ft-1b)	Before Flight	After Flight	Water Depth Before/After Landing (in.)
17A 17B	40,000	131 130	5,858 5,798	30.28 26.71	0/11	0/11	0.03/0.03
18A 18B 18C	43,000 38,000 34,000	147 137 116	6,951 6,132 4,012	41.02 31.68 20.25	11 21	21	0.02/0.05 0.06/0.03 0.02/0.06
38A 38≥ 38C	43,000 38,000 34,000	147 142 130	7,994 7,254 6,096	41.11 34.04 25.34	12/	30	0.09/0.03 0.05/0.01 0.05/0.01

As shown in figure 72, the Mark III antiskid system provided a substantial improvement in the stopping performance with the BFG tire over that of the Mark II/BFG tire combination. Using the Mark III system, the stopping distance was reduced by approximately 2,100 feet at 43,000 pounds and approximately 1,850 feet at 38,000 pounds. Both of these represent a 25-percent improvement in stopping distance over the Mark II system. The average braking coefficient of friction varied from 0.04 at 120 knots groundspeed to 0.20 at 40 knots for the Mark III system, and from 0.03 to 0.13 at these same groundspeeds for the Mark II system. Comparison of the stopping performance of the BFG tire at 38,000 pounds gross weight with that of the other tires (figures 58 and 59) shows that, with the Mark II antiskid system, the stopping distance was 7,200 feet at the kinetic energy corresponding to 130 knots true airspeed and, with the Mark III antiskid system, the stopping distance was 5,350 feet at the same kinetic energy. With the Mark II, this represents a 9-percent degradation in stopping performance when compared with that of the Standard tire and, with the Mark III, it represents a 7-percent improvement. The BFG tire was the only tire to exhibit this reversal in relative performance with a change in antiskid. No exact explanation for this phenomenon was found, however, the difference in tire wear between the tires used could have contributed to this difference in relative performance.

On test 32A and 32B, during the latter part of the braking runs, the pilot inadvertently reduced the pilot-metered brake pressure on one or both brakes while making small steering corrections. As shown in figure B46, there was a considerable reduction in pressure to the brake and, in some instances, the brake pressure was reduced to zero. Other examples of this occurred on test series 45 and 40 as discussed earlier. This reduction in brake pressure during the test may be the reason why the stopping performance data from test 32A (figure A57) is not consistent with the rest of the test data. The occurrence of a negligible brake pressure resulting from a reduced pilot-metered pressure was not due to an abnormal operation of the antiskid system, but rather resulted from the requirement for a differential braking capability and the gain characteristics of the antiskid control valve. In order to achieve maximum antiskid braking, the pilot must apply maximum pilot-metered brake pressure to both brakes.

The Flight Manual is misleading in this regard. On page 2-28, in the paragraph on Wet or Icy Runway Landing, it states: "If maximum deceleration is desired, sufficient brake pressure must be applied to keep the antiskid system active. For this purpose any amount of excess pedal displacement is satisfactory, up to and including full deflection." Since these statements are not correct, they should be deleted from the Flight Manual and the following NOTE should be inserted at the end of the same paragraph: (R 6)

NOTE

If maximum deceleration is desired, full brake pedal deflection is required. It is not sufficient to only apply enough brake pressure to keep the antiskid system active.

On test 36A with the Mark II antiskid system, the left wheel spun down to approximately half of the aircraft speed immediately after brakes were applied, but recovered four seconds later without release of pilot-metered brake pressure (figure B47). This was the only BFG tire test in which one of the wheels partially spun down. The aircraft was at 43,350 pounds gross weight and the brake application ground speed was 156 knots. New brakes were installed on the aircraft prior to this test flight; however, the day before the flight a refused takeoff from approximately 90 knots was performed on a dry runway to "burn in" the brakes.

The after-test condition of the tires used on tests 17A, B, and tests 18A, B, C is shown in figures 73 and 74, and represents approximately 21percent wear. Before these tires were changed, however, it was noted that the right main wheel required a considerable amount of force to turn the wheel by hand. Therefore, a tensiometer and rope were again used to obtain some measure of the force required to turn the wheel. The left main wheel required only 45 pounds of force to keep the wheel rotating before the brake discs were removed, and only 5 pounds after the brake discs had been taken out. However, the right main wheel required 110 pounds of force to start the wheel rotating and 100 pounds of force to keep it rotating with the brake discs in the wheel, and only 10 pounds of force after the brake discs had been removed. Examination of the pressure plates, brake discs, and back-up plates of both brakes after this test showed that, unlike the test 14A brake parts discussed earlier, all parts were within acceptable limits of wear and warpage. This indicated that the high internal friction in the wheel brake assembly could be experienced even with brake parts within the established warpage limits. The torque required to overcome this internal friction is significant if one looks at the tire to pavement friction coefficient necessary to generate the 100 to 110 pounds of force measured. Typically, for speeds of 120 to 130 knots and at low aircraft gross weight (34,000 pounds), the normal force on each main gear was in the 11,000- to 12,000-pound range. Therefore, in this instance, a friction coefficient on the order of 0.01 would be required to overcome the internal wheel brake assembly friction and This is of the same order of magnitude as the coefficient of friction generated during braking at high speeds on a wet runway. This high internal friction could significantly effect wheel spinup on a wet runway and could contribute to wheel spindowns with either antiskid system. This problem of high internal friction in the wheel brake assembly should be investigated further. (R9)

USAF TIRE

Fifteen landings were performed on a wet runway using the USAF tires, ten were done with the Mark III antiskid system (table 12) and five with the Mark II antiskid system (table 13). The standard day stopping performance and braking coefficient of friction resulting from these tests are presented in figures A61 through A64. As shown by the comparison in figure 75, use of the Mark III system provided an improvement in stopping performance with respect to that when the Mark II system was used. At 43,000 pounds gross weight, the Mark III/USAF tire combination gave a 650-foot shorter stopping distance, and at 34,000 pounds the stopping distance was 700 feet shorter. These correspond to improvements in stopping distance of 9 percent and 12 percent, respectively. For the Mark III/USAF tire combination, the average braking coefficient of friction varied from 0.03 at 120 knots groundspeed to 0.18 at 40 knots groundspeed. With the Mark III, the friction coefficient varied from 0.05 to 0.2 over this same range.

Table 12
MARK III ANTISKID, USAF TIRES, WET CONCRETE RUNWAY

Flt	Date	Test	Acft Gross Weight	Wind	Ambient Temp	Pressure Altitude	Brake On/Brake Off Ground Speed [kt]	Distance Brakes On [ft]	Energy Absorbed by Brakes (106 ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (196 ft-1b)
No.	(1973)	4.4	(15)	(kt)	(deg C)			7,048	17.37	7,189	37.29
372	1 May	21.8	39,800	0	6.6	2,170	145/24	5,387	14.42	5,571	26,55
314	- 1107	218	34,550	-1.7	9.8	2,157	132/25		20.41	6,348	27.10
373	2 May	22A	43,200	1.7	10.4	2,042	139/22	5,200	16.35	5,375	28.96
313	4 may	228	38,200	1.7	12.7	2,037	131/28	1	15.05	9,175	48.17
205	18 May	AOE	43,000	-7.4	17.5	2,223	159/68	6,921	17.45	7,082	33.97
385	18 May	308	38,200	-5.5	20.0	2,226	142/28	6,072	13.08	6,404	27.28
		30C	34,200	-4.6	22.2	2,228	134/34		20.41	7,192	38.57
425	4 Sep	64A	43,250	0	11.6	2,302	142/21	5,910	16.53	6,008	29.73
431	4 ach	64B	38,150	0	16.7	2,302	133/20	5,561	12.58	5,654	24.55
		GAC	34.350	0	19.4	2,302	751/64				

		Standard	Day Condi	Put Tir	e Wear	Water Depth			
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)		Plight After Bo			
21A 21B	40,000	147 130	7,396 5,304	38.37 25.23	0/14	0/11	0.09/0.02		
22A 22B	43,000	141 132	6,488 5,451	37.98 29.43	14/25	14 21	0.06/0.03		
30A 30B 30C	43,000 38,000 34,000	150 134 127	8,217 6,317 5,713	42.83 30.12 24.21	36 43	30 43	0.07/0.02 0.09/0.05 0.08/0.03		
64A 64B 64C	43,000 38,000 34,000	141 131 124	7,076 5,829 5,367	37.95 28.85 23.30	0 11	0 18	0.09/0.02 0.09/0.05 0.09/0.01		

Table 13
MARK II ANTISKID, USAF TIRES, WET CONCREZE RUNMAY

Flt	Date	Test	Acft Gross Weight	Wind	Ambient	Altitudo	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (106 ft=1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)
No.	(1973)	No.	(1b)	(kt)	(deg C)	(Et)			14.68	8,846	44.87
374	3 May	23A 23B	43,500 38,200	-3.5 -3.5	9.5	2,159 2,159 2,162	153/62 140/24 133/28	7,523 7,209 6,491	16.33 13.23	7,417 6,728	33.23 26.70
		23C	34,200	-3.6	15.8	21.00	10.504		16.42	8,373	37.96
386	22 May	31A	40,350		11.7	2,329	138/26	7,811	15.40	7,389	30.55

		Standard	Day Condi	Pot Ti	re Wear		
Test	Acft Gross Meight (1b)	Brakes On (XTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)	Before Flight		Mater Depth Before/After Landing (in.)
23A 23B 23C	43,000 38,000 34,000	149 136 128	8,347 6,964 6,227	42.20 31.08 24.61	25/36	21/30	0.06/0.01 0.06/0.02 0.07/0.04
31A	40,000	139	7,573 6,569	34.12 26.96	13/	43/	0.09/0.02

Comparison of the USAF tire stopping performance with that of the other tires, figures 58 and 59, shows that for a gross weight of 38,000 pounds and at a kinetic energy corresponding to 130 KTAS, the stopping distance with the Mark II antiskid was 6,400 feet and with the Mark III system was 5,600 feet. These distances represent performance improvements of only 2 percent and 3 percent, respectively, when compared with that of the Standard tire.

The antiskid parameters for test 23B and test 30B are typical, respectively, of the Mark II and Mark III antiskid operation with the USAF tire, and are presented in figures B4B and B49. Figures 76 and 77 show the condition of tires after tests 23A, B, C and represent approximately 30- to 35-percent wear. These same tires were used on tests 21A and B and 22A and B. No wheel spindowns occurred during testing of this tire with the Mark II or Mark III antiskid systems.

The first attempt to test the USAF tires occurred a few days prior to test 21A and B, and resulted in the flat-spotted tires shown in fig-This was the first test with the Mark III system after the wheel speed indicators had been installed in the rear cockpit. The indicators showed no wheel speed during the taxi checkout but the test team thought the problem at that time was due to faulty indicator instal-Investigation revealed that no wheel speed information was available to the antiskid system during the test because the wheel speed sensors had not been installed correctly by maintenance personnel. The installation procedure in T.O. 1F-4E-2-5 says that the sensor is to be screwed into its hole in the brake housing until it bottoms lightly. After bottoming, the sensor is to be unscrewed 1-1/4 turns, with a tolerance of plus 1/4 turn and minus zero turns. The sensors, in this case, had been unscrewed approximately three turns too far or not screwed in far enough to begin with, resulting in no wheel speed pickup for the antiskid system. As a result, when the brakes were applied, the antiskid system sensed either no speed or a speed below its threshold of operation and allowed full brake pressure to be applied and held, causing the wheels to skid and lock up. The aircraft reaction during this incident is noteworthy. Unlike the results of test 10A where only one wheel was locked up, on this test after 4,000 feet of travel with both wheels locked up, the aircraft directional control had degraded to the point where the aircraft was deviating 10 degrees off the runway heading in a diverging lateral oscillation. This oscillation was evident from the pattern of the flat spot on the tires. When the brakes were released, however, directional control was immediately regained.

This incident vividly illustrates a problem with the available methods of checking the antiskid system operation. Neither the AN/AJM-18 antiskid test set nor the automatic checkout circuit of either antiskid system can be used to determine whether or not the sensors have been installed correctly. Both methods could indicate an operable system though antiskid protection might not be available. A procedure or method should be developed which would allow the pilot and/or crew chief to readily determine whether or not the antiskid sensors have been installed correctly. (R 5)

DUNLOP TIRE

Thirteen stopping tests were performed on a wet runway with the Dunlop tire; eight using the Mark II antiskid (table 14) and five using the Mark III antiskid (table 15). The standard day stopping performance and braking coefficient of friction data for these tests are presented in figures A65 through A68. Comparison of the results using the two antiskid systems (figure 80) shows that the stopping performance when using this tire was improved considerably by use of the Mark III antiskid system. At 43,000 pounds gross weight, the stopping distance was 1,350 feet shorter when the Mark III was used and, at 38,000 pounds gross weight, the stopping distance was 1,050 feet shorter. This represents a stopping performance improvement of 15 percent at both gross weights. Comparison of the Dunlop tire performance with that of the other tires (figures 58 and 59) shows that it was the worst performer with both antiskid systems. The stopping distance for an aircraft gross weight of 38,000 pounds and brake application true airspeed of 130 knots was 7,400 feet using the Mark II and 6,350 feet using the Mark III. This represents a degradation when compared with the Standard tire stopping performance of 12 percent and 10 percent, respectively. The average coefficient of friction developed with the Mark II antiskid/Dunlop tire combination varied from 0.02 at 120 knots groundspeed to 0.15 at 40 knots while that developed with the Mark III antiskid/Dunlop tire combination varied from 0.03 to 0.17.

Table 14
MARK II ANTISKID, DUNLOP TIRES, WET CONCRETE RUNMAY

Flt No.	Date (1973)	Test	Acft Gross Weight (1b)	Wind (kt)	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (106 ft-1b)	
392		33A 33B	40,350	-0.2	13.6 15.5	2,234	146/24 136/20	7,484 7,052	17.76	7,623 7,110	37.87 30.25	
393	28 May	34A 34B 34C	43,200 38,700 34,700	0.3 0.3 0.5	24.0 24.6 24.7	2,234 2,238 2,243	152/143 135/25 129/22	7,515 6,966	Wheel Spindown 15.01 12.06	7,695 7,087	31.33 25.61	
429	30 Aug	62A 62B	42,900	-4.4 -3.2	16.1 17.1	2,328	153/80 147/67	7,863 7,799	7.97 6.08	9,493	44.23 36.55	
430	31 Aug	63A 63B	40,300	-6.8 -8.3	15.0	2,376 2,376	152/92 149/77	6,825 7,389	4.07	9,368	41.45 35.99	

	-	Standard	Day Condi	Pet Tir	e Wear		
Test	Acft Gross Weight (1b)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)	Before Flight	After Flight R	Water Depth Before/After Landing (in.)
33A 33B	40,000	144	7,400 6,791	36.76 28.88	0/10	0/6	0.04/0.02
34A 34B 34C	38,000 34,000	131 125	7,105 6,535	28.93 23.63	10/19	6/21	0.03/0.02 0.09/0.03 0.09/0.03
62A 62B	43,000 38,000	147 141	9,771 8,729	41.04 33.50	0/19	0/19	0.09/0.04
63A 63B	40,000	144 139	9,484	36.55 30.57	19/27	19/27	0.09/0.07

Table 15
MARK III ANTISKID, DUNLOP TIRES, WET CONCRETE RUNWAY

Flt	Date	Test	Acft Gross Weight	Wind	Ambient Temp (deg C)	Pressure Altitude (ft)	Brake On/Brake Off Ground Speed (kt)	Distance Brakes On (ft)	Energy Absorbed by Brakes (10 ⁶ ft-1b)	Extrapolated Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-lb)
No.	(1973)	No.	(1b)	(kt)	(ueg C)	1267			14 50	8,429	41.88
401	19 Jun	39A 39B	43,850 38,950	0.5	14.0 17.0 22.6	2,148 2,143 2,141	147/51 137/20 123/18	7,638 7,219 5,787	14.58 15.47 13.01	7,309 5,854	32.42 23.67
402	20 Jun	39C 40A 40B	35,200 41,500 37,550	0.7 0.2 1.3	16.8 17.5	2,150 2,147	139/22	7,294 6,495	17.22 14.69	7,396 6,610	35.71 29.94

		Standard	Day Condi	Pct Tir	e Wear			
Test	Acft Gross Weight (lb)	Brakes On (KTAS)	Stopping Distance (ft)	Kinetic Energy at Brakes On (10 ⁶ ft-1b)	Before Flight L	After Flight R	Water Depth. Before/After Landing (in.)	
39A 39B 39C	43,000 38,000 36,000	146 134 123	8,162 6,849 5,962	40.27 30.38 24.12	19 23	21 25	, 	
40A 40B	41,000 38,000	138 135	7,118 6,755	34.38 30.65	23 26	25 30	0.09/0.01 0.09/0.04	

The inconsistencies shown in the stopping performance data for the Mark II system can probably be attributed in part to water depth in one case and to wheel spindowns in general. For tests 33A and 33B, the procedure used to wet the test section was inadvertently altered from that used on all other tests. Inexperienced personnel drove the water trucks at a higher speed than that desired (11 MPH) when the test section was wetted. This resulted in less water being applied than was normal but was not indicated by the single water depth measurement made. For this reason, the data from these two tests were not considered when curves were faired to the rest of the test data.

Antiskid parameters for test 34B showing operation of the Mark II antiskid with the Dunlop tire are presented in figure B50.

On all of the Mark II antiskid tests with the Dunlop tire, except for tests 34B and test 62B, one wheel partially spun down immediately after brake application and stayed that way for varying lengths of time. These partial wheel spindowns are shown in figures B51 through B56. Except for test 34C, all recovered to full wheel speed without brake release. Brake pressure was released by the pilot when the spindown was noted on test 34C for about one second which allowed the wheel to spin back up to speed. The pilot reported that the right wheel may have been on the painted centerline of the runway when brakes were applied which could have contributed to wheel spindown in this case.

Figure B57 presents the results of test 34A on which a full wheel spindown occurred. The brakes were applied at a groundspeed of 152 knots and the aircraft gross weight was 43,200 pounds. The antiskid action is similiar to what happened with the Standard tire on tests 10A and 24A. However, in contrast to test 10A, the wheel was not allowed to lock up. The brake pressure was released by the pilot when the wheel reached zero speed.

Another fact to consider in evaluating the Mark II stopping performance data is the fact that the aircraft was in for Phase Inspection prior to test series 62 and 63. During this inspection, a new brake housing was installed on the left main landing gear of the aircraft as well as new grip tubes for the pistons in the right brake housing. What effect these changes had, if any, on these two tests series as well as all those that followed is unknown.

Test 39A was significant in that it was the only test using the Mark III antiskid on which a partial wheel spindown occurred. The antiskid parameters for this test are shown in figure B58. From this data, one can see that the left wheel skidded to almost half value when brakes were applied. The important thing to note, however, is that, unlike the Mark II system, the Mark III antiskid system did not aggravate the situation by contributing to further spindown and possible wheel lockup, but allowed the wheel to eventually recover. This can be attributed to the difference in the control logics of the antiskid systems. Since the Mark III antiskid compared the wheel speed to a predicted aircraft velocity and tried to maintain a constant difference, or slip velocity, the brake pressure was not reapplied when a skid occurred until the wheel speed had recovered to almost aircraft velocity.

The condition of the tires used for tests series 33, 34, 39, and 40 is shown in figures 81 and 82, and represents a tire wear of 26 and 30 percent.

WATER ONLY TESTS

Two landing test series were performed to determine the effect on the aircraft stopping performance, if any, of having the organic firefighting foam in the mixture used to wet the test section. These tests were all done using the Mark III antiskid system. Three landings (tests 38A, B, and C) were done using the BFG tire, and another three landings were done using the Standard tire (tests 65A, B, and C). The wetting procedures used were the same as those used during all other testing. Prior to each test series, however, the test section was washed down to remove any residual foam from previous tests. The standard day stopping performance and friction coefficient data are presented in figures A69 through A72.

The results of these tests, when compared with the results of the equivalent foam/water mixture tests (figures 83 and 84), proved to be inconclusive. At an aircraft gross weight of 38,000 pounds, using water only to wet the test section, a 600-foot increase in stopping distance resulted with the BFG tire; whereas, with the Standard tire there was a 450-foot decrease in stopping distance. This reversal in results can probably be attributed to the effects of tire wear. The BFG tires used for the water only tests were approximately 35 percent worn compared with the approximately 15-percent worn tires used on the tests where a foam/ water mixture was used. This could explain the longer stopping distance with the BFG tire. The Standard tires used for the water only tests, however, were almost new tires compared with those used on the foam/water mixture tests that had a tire wear of 25 to 35 percent. This difference could explain the shorter stopping distance with the Standard tire.

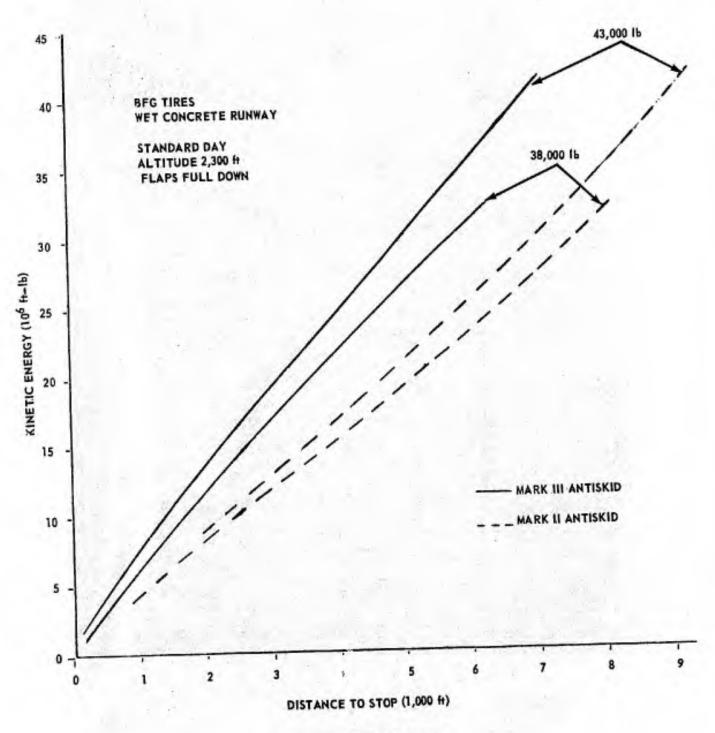


Figure 72 BFG Tire Performance



Figure 73 Right BFG Tire (After Test Series 17 & 18)

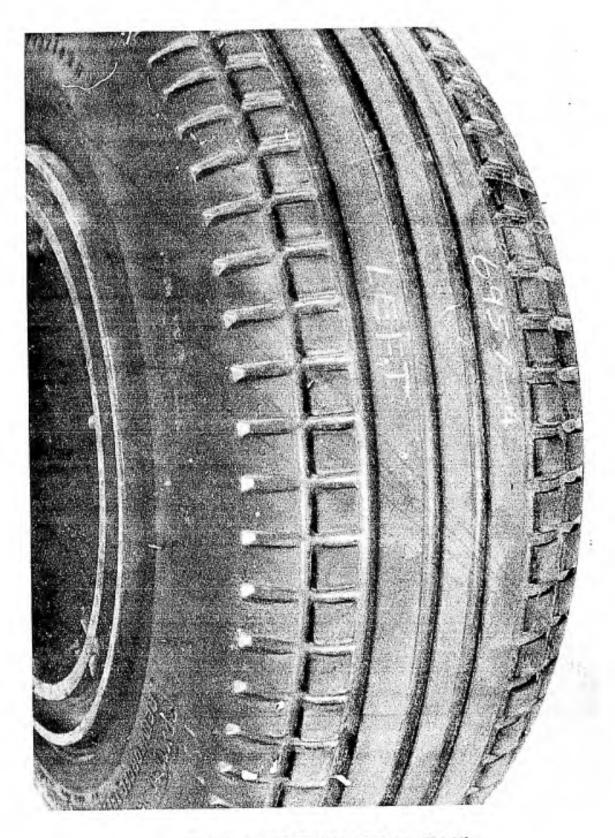


Figure 74 Left BFG Tire (After Test Series 17 & 18)

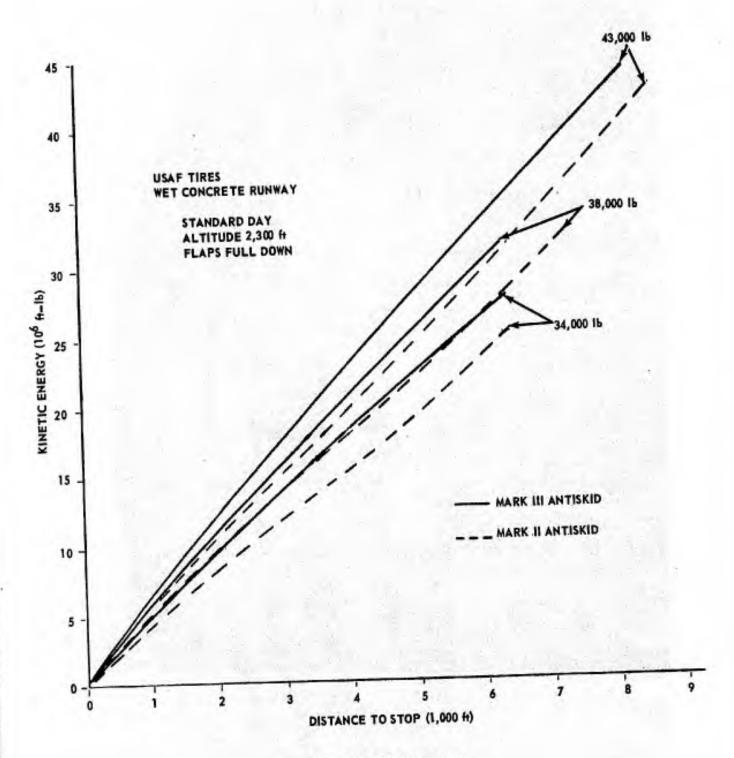


Figure 75 USAF Tire Performance



Figure 76 Right USAF Tire (After Test Series 21, 22, & 23)



Figure 77 Left USAF Tire (After TestSeries 21, 22, & 23)

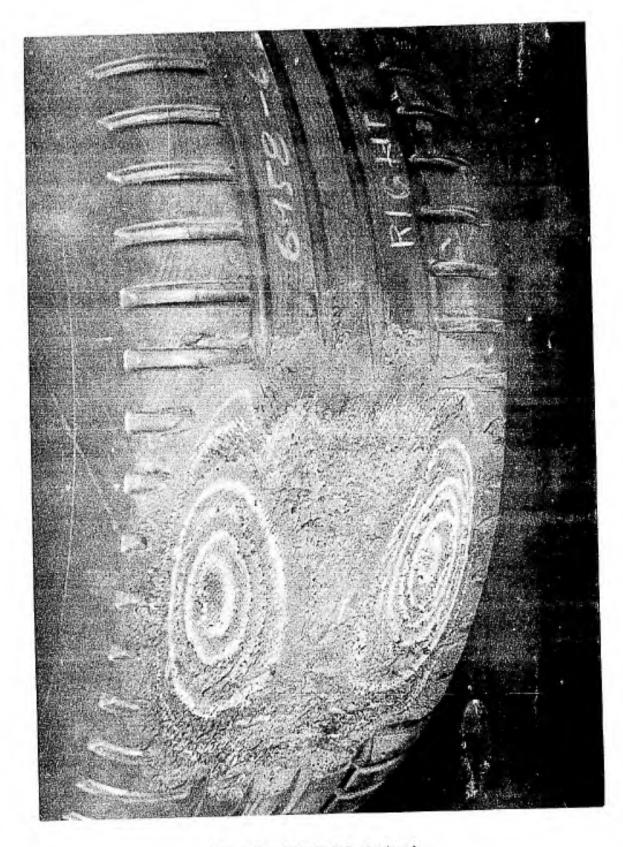
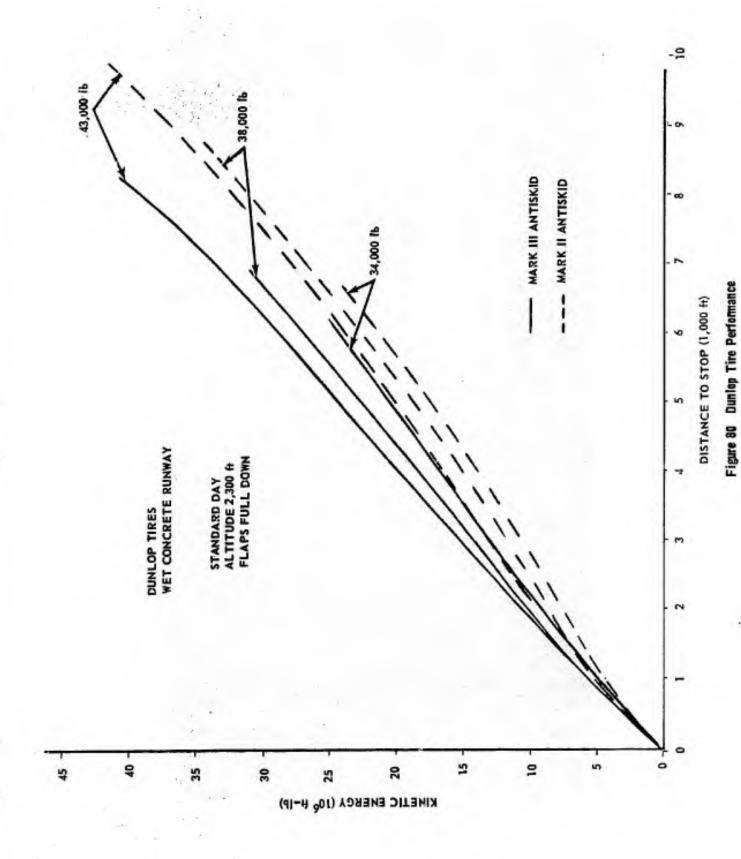


Figure 78 Right Tire (After Lock-up)



Figure 79 Left USAF Tire (After Lock-up)



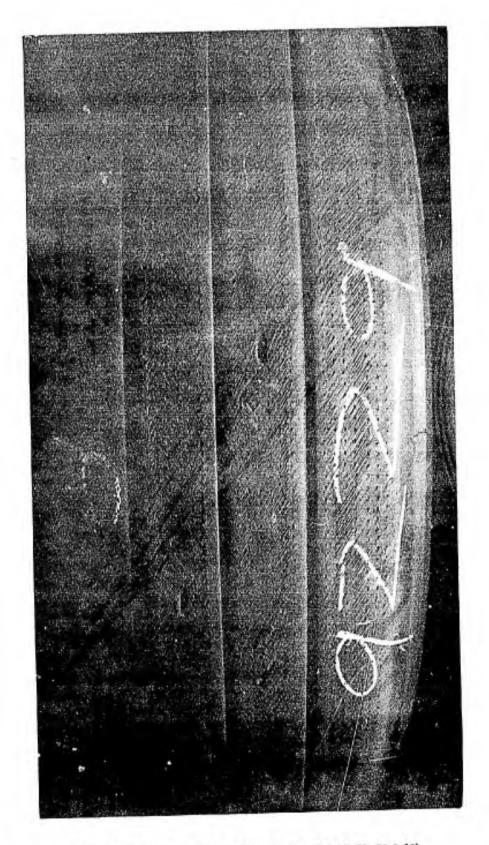


Figure 81 Right Dunlop Tire (After Test Series 33, 34, 39 & 40)

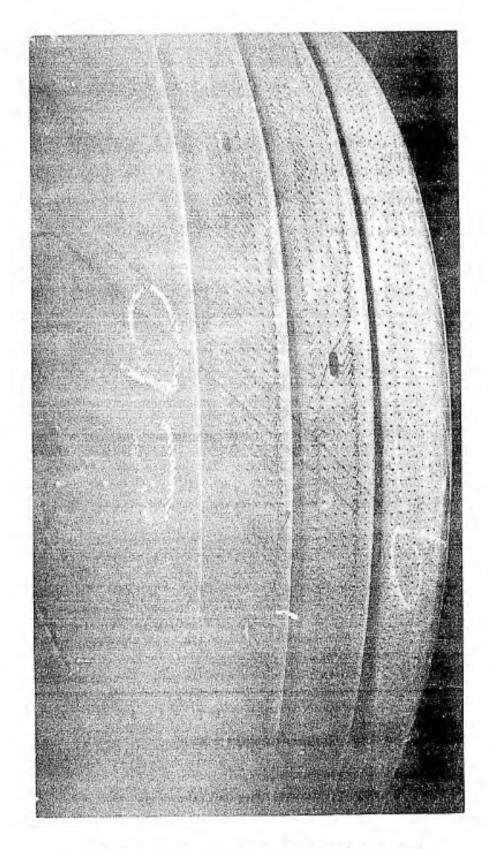


Figure 82 Left Dunloy Tire (After Test Series 33, 34, 39 & 40)

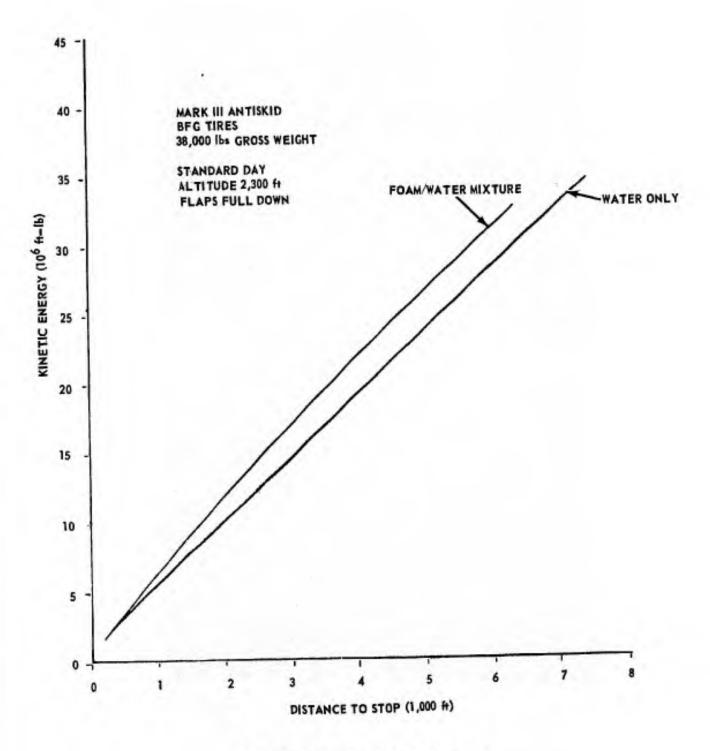


Figure 83 BFG Tire/Water Only Comparison

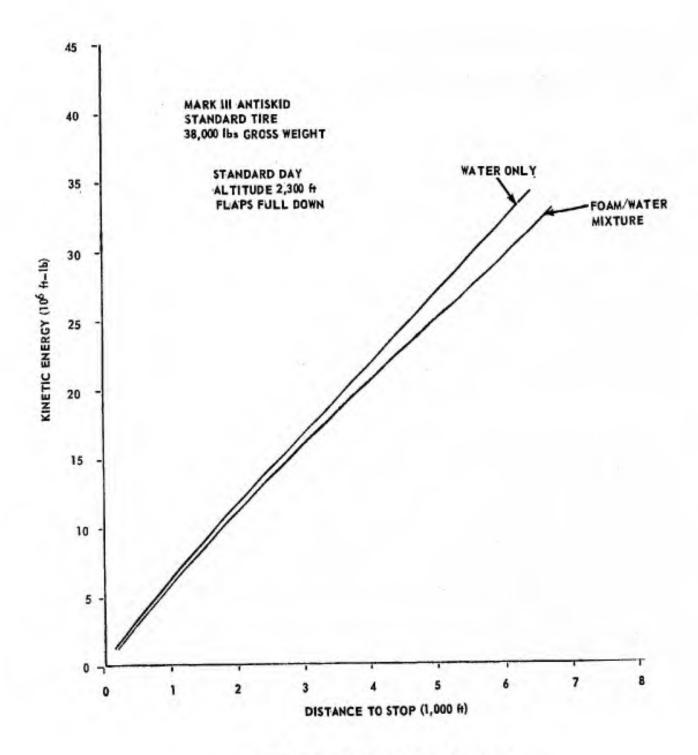


Figure 84 Standard Tire/Water Only Comparison

CONCLUSIONS AND RECOMMENDATIONS

The Mark III antiskid system provided an improvement in wet runway stopping performance with all five tire tread designs that were tested when compared with that of the Mark II antiskid system with the same tire tread designs. With the Mark III antiskid system, all five tire tread designs outperformed the Mark II/Standard tire combination. Wheel spindowns which could lead to serious locked wheel problems were noted at high brake application groundspeeds with the Mark II antiskid system on wet runways.

The Sommers tire tread design provided the best stopping performance of all the tires tested. The improvement in stopping performance resulting from use of the Sommers tire was so significant that both the Mark II/ Sommers tire and Mark III/Sommers tire combinations outperformed all other antiskid/tire combinations tested. The wet runway stopping performance was degraded when worn tires were used with either antiskid system. This degradation was substantial with the Sommers tire, which resulted in no difference between the stopping performance of the Sommers tire and Standard tire when both tires were worn.

Varying the touchdown sink rate affected the wheel spinup times on a wet runway. Brake application before full wheel spinup with the Mark III antiskid system had no significant effect on the wet runway stopping performance. The results of no-flap and half-flap landing configuration stopping performance tests were inconclusive.

Pilot evaluation of the pilot-selectable, two-mode authority, nose-wheel steering system showed that aircraft control, when the +15 degrees mode was used during takeoffs and landings, was unchanged compared to the production (+70 degrees only) steering system. The pilot also noted no change in the control effort required. Having two steering modes was considered advantageous; however, separate pilot selectability of the steering mode was believed to be unacceptable from a safety standpoint. The pilot observed no difference in the performance characteristics of the three new nosewheel tire tread designs when compared with the Standard nosewheel tire.

Partial spindowns, lasting from a few seconds to almost the entire braking run, of one or both wheels at brake application occurred on many of the tests with the Mark II antiskid system when brakes were applied at high groundspeed. On one test with the Standard tire, at brake application one wheel gradually spun down to zero speed and remained locked for the entire braking run. Because of this fact, brakes were not applied during the sink rate tests with the Mark II antiskid system until the wheels had fully spun up. Results from the Mark III sink rate tests showed that the pilot was capable of applying brakes before full wheel spinup. Because the wheel lockup occurred, wheel speed indicators were installed in the rear cockpit of the aircraft, and testing of the Mark II antiskid continued safely. Having the wheel speed indicators in the aircraft prevented a locked wheel from occurring when one wheel spun down to zero speed on three more occasions. The spindowns occurred even with a correctly functioning Mark II antiskid system and, in fact, resulted from antiskid action. This fact is contrary to Flight Manual statements. The so-called "locked wheel" detection circuitry of the Mark II system did not prevent the four gradual spin downs to zero speeds from occurring. The name of this circuit is misleading since its designed function is only to release brake pressure when the wheel decelerates faster than 120 radians/second2.

1. The following should be added to the Flight Manual under the CAUTION at the end of the Wet or Icy Runway Landing paragraph on page 2-28 (page 79):

Avoid using brakes above 130 knots on a wet or icy runway. When friction levels are low, it is possible, even with a correctly functioning antiskid, for one or both wheels to partially spin down or lock up when brakes are applied at high speeds.

- 2. The sentence in the Wet or Icy Runway paragraph on page 2-28 of the F1: ght Manual which states, "The antiskid system protects against a locked wheel and can effectively and safely produce the maximum deceleration possible for the existing runway conditions.", should be deleted and replaced by, "Use of the antiskid system can produce the maximum deceleration possible for the existing runway conditions." (page 78).
- 3. A new name should be given to the Locked Wheel Detection circuit of the Mark II antiskid system, and all references to it in T.O. 1F-4E-2-5 should be changed to reflect the new designation (page 78).
- Cockpit installed wheel speed indicators should be used, where practical, on future braking tests (page 78).

On one occasion both tires were flat-spotted because the wheel speed sensors had not been installed correctly. This incident illustrates a problem with the available methods of checking the antiskid system operation. Neither the AN/AJM-18 antiskid test set nor the automatic checkout circuit of either antiskid system can determine whether or not the sensors have been installed correctly.

5. A procedure or method should be developed which would allow the pilot and/or crew chief to readily determine whether or not the antiskid sensors have been installed correctly (page 111).

Reductions in pilot-metered pressure to the antiskid control valve resulted in a considerable reduction in pressure to the brake; and, in some instances, the brake pressure was reduced to zero. These inadvertent reductions occurred during the braking run on six tests, two with the Mark II and four with the Mark III. This phenomenon was not an abnormal operation of either antiskid system, but resulted from the requirement for a differential braking capability and from the gain characteristics of the antiskid control valve. To achieve maximum antiskid braking, the pilot had to apply maximum pilot-metered brake pressure to both brakes. This is contrary to statements in the Flight Manual.

6. The section of the Wet or Icy Runway Landing paragraph on page 2-28 of the Flight Manual which states, "If maximum deceleration is desired, sufficient brake pressure must be applied to keep the antiskid system active. For this purpose any amount of excess pedal displacement is satisfactory, up to and including full deflection.", should be deleted, and the following NOTE should be inserted at the end of the same paragraph (page 108):

NOTE

If maximum deceleration is desired, full brake pedal deflection is required. It is not sufficient to only apply enough brake pressure to keep the antiskid system active.

The antiskid control valve was changed at the beginning of the test program when it was suspected that it was out of tolerance. Subsequent calibration showed that it was slightly out of tolerance on the low pressure side of the specification curve. The difference in calibration between the two antiskid control valves had no discernible effect on the dry runway stopping performance of the Standard tire with either antiskid system; however, changing the valve did improve the wet runway stopping distance. Antiskid control valves with calibrations on the extremes of the tolerance band appeared to have a significant effect on wet runway stopping performance.

7. Further tests should be accomplished to better define the affects that antiskid control valves with calibrations on the extremes of the tolerance band have on wet runway performance (page 80).

Hydro-aire engineers "tuned" the Mark III antiskid system after four dry runway and three wet runway test landings. Tuning consisted of slightly adjusting the control box circuits to better match the F-4 hydraulic system. This "tuning" had no discernible effect on either the dry or wet runway stopping performance.

Having one new stator in each brake assembly during one dry runway test resulted in a considerably longer stopping distance. To avoid the effect on the antiskid operation shown on this test, a procedure of "burning-in" new brake parts was adopted for use during the test program. Completely new brakes had been installed for two wet runway test series and were deliberately not "burned-in". The results showed considerably longer stopping distances and significant delays in wheel spinup times. Not "burning-in" new brake parts appeared to cause a substantial degradation in both the wet and dry runway stopping performance.

 A procedure should be developed and used to "burn-in" new brake parts whenever they are installed (page 59).

On two occasions while the aircraft was on jacks, a force of 100 to 110 pounds was required at the outer radius of the tire to rotate the wheel. On the first occasion, unacceptable wear and warpage was found for a number of brake discs. However, the second time the measurement was made, all the brake parts were within wear and warpage limits. The tire/pavement friction coefficient required, at high speed and low aircraft gross weight, to overcome this high internal friction would be significant when compared with the coefficient of friction generated during braking at high speeds on a wet runway. The high internal friction in the wheel brake assembly could result even if the brake parts were within established warpage limits. It could significantly effect wheel spinup on a wet runway and contribute to wheel spindowns with either antiskid system.

 The problem of high internal friction in the wheel brake assembly should be investigated further (page 109).

During one test landing, a small amount of brake pressure was unintentionally applied at touchdown causing the wheel spinup to be delayed. On one test done inflight, significant pilot-metered brake pressures
occurred when the pilot exercised full left and right rudder pedal travel
with the balls of the feet on the rudder bar. These results indicated
that it was possible to unintentionally apply brake pressure while operating the rudder.

The +15 degrees mode of the pilot-selectable, two-mode authority, nosewheel steering system was used for all test takeoffs and landings, while the +70 degrees mode was used for all taxi operations. A two-position toggle switch was used to select the desired mode of steering. Procedures were developed and checklist items devised for the test program to insure that the switch was in the correct position. It would be easy to forget to change the switch position, which could result in accidents during taxi operations. Therefore, for normal flight operations, the switch logic of the nosewheel steering system tested was unacceptable from a safety standpoint.

10. If a two-mode authority, nosewheel steering system is used on the F-4 aircraft, a separate steering mode select switch should not be used. The system should be wired such that the +15 degrees steering mode would be available when the antiskid control switch is in the LN position and the +70 degrees steering mode would be available when the antiskid control switch is in the OFF position. Use of nosewheel steering should still be controlled by the nosewheel steering button on the control stick grip. For situations when operation of the antiskid system is not desired, but the +15 degrees steering authority is desired, the system should be wired such that use of the paddle switch on the control stick to drop out the antiskid system would not drop out the +15 degrees steering mode (page 51).

The USAF and BFG nosewheel tire tread designs incorporated grooves on the shoulder of the tire. During the wet runway tests, the water spray pattern off these tires was very low with respect to the ground. This effect could have application on aircraft with a water ingestion problem.

11. The USAF and BFG nosewheel tire tread designs should be evaluated as a possible method of preventing water ingestion (page 51).

Dry runway tests were done with only the Standard tire and BFG tire. There was a slight improvement in the dry stopping performance with both tires when the Mark III antiskid system was used. The BFG tire, however, had a degraded stopping performance with both antiskid systems when compared with that of the Standard tire. The wear on both the Standard tire and the BFG tire resulting from the dry runway maximum performance stops appeared to be more severe when the Mark III antiskid system was used. However, the BFG tire wear on the dry runway was excessive with both antiskid systems.

12. If the BFG tire tread design is considered for use in the field, further wear tests should be made (page 61).

A modified AN/AJM-18 test set and T.O. 1F-4E-2-5 procedures were used to checkout the antiskid system whenever it was changed. On one occasion, replacement of a good antiskid control valve was indicated when the problem was actually caused by the emergency braking system being in the actuated position while the checkout was made. On other occasions, checking the antiskid system connectors for bent pins and correct connection avoided replacement of good antiskid control boxes. In these instances, as well as other times during the test program, the published T.O. procedures for brake assembly and operational checkout of the antiskid and brake system proved to be inadequate.

13. The following NOTE should be added under the ANTISKID CONTROL VALVE CHECK prior to procedure 3a in paragraph 4-31, Antiskid System Operational Checkout, of T.O. 1F-4E-2-5 (page 32):

NOTE

Before proceeding, check the EMERGENCY BRAKE CONTROL VALVE and reset, if necessary.

14. The following NOTE should be added under the ANTISKID CONTROL BOX CHECK prior to procedure 4a in paragraph 4-31, Antiskid System Operational Checkout, of T.O. 1F-4E-2-5 (page 33):

NOTE

When the remedy for abnormal indication requires replacement of the control box, check all electrical connections in the antiskid system for bent pins and faulty connection before effecting the replacement.

15. Better overall procedures and/or equipment should be developed for the brake and antiskid system assembly and operational checkout. The procedures and/or equipment developed should address both the preflight checkout and assembly and checkout after any brake/antiskid system components are disturbed for replacement or other maintenance actions (page 33).

A temperature measurement was made on one stator in each brake stack and displayed in the rear cockpit. This was done initially to ensure that the brakes were cool enough before landing for good stopping performance data and that enough energy absorbing capability remained after a maximum braking stop to safely accomplish an aborted takeoff. The cockpit display also provided a valuable means of monitoring what was going on within the brakes.

16. Measurement of the brake temperature with a cockpit display should be considered for use on all future brake, antiskid, and/or stopping tests (page 43).

Potentiometers attached to each main landing gear scissor were used for measuring strut displacement in an attempt to determine the normal force on each main gear. Because of the shock loads and vibrational environment, they repeatedly broke and slipped out of calibration. In addition, the range of measurement was too small for this type of instrumentation, and the measurement was also highly dependent upon strut servicing and damping characteristics. As a result, this type of instrumentation and technique proved to be inadequate.

17. The technique of measuring strut displacement to determine the main landing gear loads and the use of potentiometers to make the measurement should not be used on future F-4 flight test programs (page 46).

REFERENCES

- Proposal for Nosewheel Steering and Skid Control Design, Instrumentation and Technical Support, MDC A1406, McDonnell Aircraft Company, St. Louis, Missouri, 12 November 1971. UNCLASSIFIED
- T.O. 1F-4C-1, Flight Manual, USAF Series F-4C, F-4D, and F-4E Air craft, 15 August 1973. UNCLASSIFIED
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- Anderson III, Leslie B., Captain USAF, German F-4F Evaluation, AFFTC Technical Letter Report, Air Force Flight Test Center, Edwards AFB, California, September 1973. CONFIDENTIAL
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APPENDIX A DATA REDUCTION AND PLOTS

DATA REDUCTION

Stopping Distance, Airspeed, and Kinetic Energy:

The extrapolated stopping distances were reduced to standard day, no-wind conditions at 2,300 feet pressure altitude (runway elevation of Edwards AFB). The standardization methods were based on reference 5^5 .

The equation used to correct to the no-wind condition was:

$$s_{gt} = s_{gt_w} \left(1 + \frac{v_w}{v_g}\right)^{1.85}$$

where:

Sg. = test day stopping distance, corrected for wind (ft)

Sgtw = test day stopping distance, not corrected for wind (ft)

V_W = component of wind along the runway, headwind (+), tailwind (-) (fps)

Vg = test day brake application groundspeed (fps)

The test day no-wind stopping distances were then corrected to standard day conditions using the following equation:

$$s_{g_s} = s_{g_t} \frac{\sigma_t}{\sigma_s} \left(\frac{W_s}{W_t} \right)^2$$

where:

S_{gs} = standard day stopping distance at 2,300 feet, corrected for wind (ft)

σ_t = test day density ratio (dimensionless)

 σ_s = standard day density ratio at 2,300 feet (dimensionless)

W+ = aircraft test gross weight (1b)

We = aircraft standard gross weight (1b)

Herrington, Russel M., Major USAF, et al., Flight Test Engineering Handbook, AF Technical Report No. 6273, Air Force Flight Test Center, Edwards AFB, California, May 1951, revised January 1966. UNCLASSIFIED

The test day true airspeed was corrected as follows:

$$V_{t_s} = (V_g + V_w) \left(\frac{W_s}{W_t} \frac{\sigma_t}{\sigma_s} \right)^{1/2}$$

where:

V_{ts} = standard day true airspeed at 2,300 feet (or standard day no-wind groundspeed)

The standard day and test day kinetic energies were calculated as follows:

$$E_{s} = \frac{W_{s}}{2g} (V_{t_{s}})^{2} \quad (ft-lb)$$

$$E_{t} = \frac{W_{t}}{2g} (V_{g})^{2} \qquad (ft-lb)$$

Braking Force, Coefficient of Friction, and Absorbed Brake Energy:

The braking force was calculated by summing forces as follows:

$$F_{BR} = F_{n_I} - \left(\frac{W_t}{g}\right) a - D - \mu_{r_n} N_n$$

where:

FRR = braking force (1b)

 $F_{n_{\bar{1}}}$ = net idle thrust, total (1b)

a = aircraft acceleration from phototheodolite data (fps per sec)

D = aircraft drag (lb)

 μ_{r_n} = rolling coefficient of friction; assumed to be 0.015 (dimensionless)

 N_n = normal force of the nose gear (1b)

g = acceleration of gravity (32.2 ft/sec2)

The coefficient of friction between the aircraft tires and the runway was calculated using the following equation:

$$\mu_{\rm BR} \ = \ \frac{F_{\rm BR}}{N_{\rm m}} = \ \frac{F_{\rm BR}}{(W_{\rm t} - L - N_{\rm n})} \label{eq:mu_br}$$

where:

 μ_{DB} = braking coefficient of friction (dimensionless)

N = normal force on the main landing gear (lb)

L = aircraft lift (lb)

The total energy absorbed by the brakes was calculated by summing, from brake application to brake release, the brake energy absorbed from one data point to the next. The incremental energy was calculated using the following equation:

$$\Delta E_{BR} = F_{BR} \Delta S$$

where:

AEBR = energy absorbed by both brakes during deceleration from one data point to the next (ft-lb)

AS = the distance travelled by the aircraft from one data point to the next (ft)

Idle Thrust, Lift, and Drag:

The net idle thrust as a function of true airspeed used for data reduction was provided by MCAIR and is shown in figure A73. The lift and drag values used in the data reduction were calculated from coefficients of lift and drag versus angle of attack ($C_{\rm L}$ and $C_{\rm D}$ versus a) curves provided by ASD and shown in figures A74 and A75.

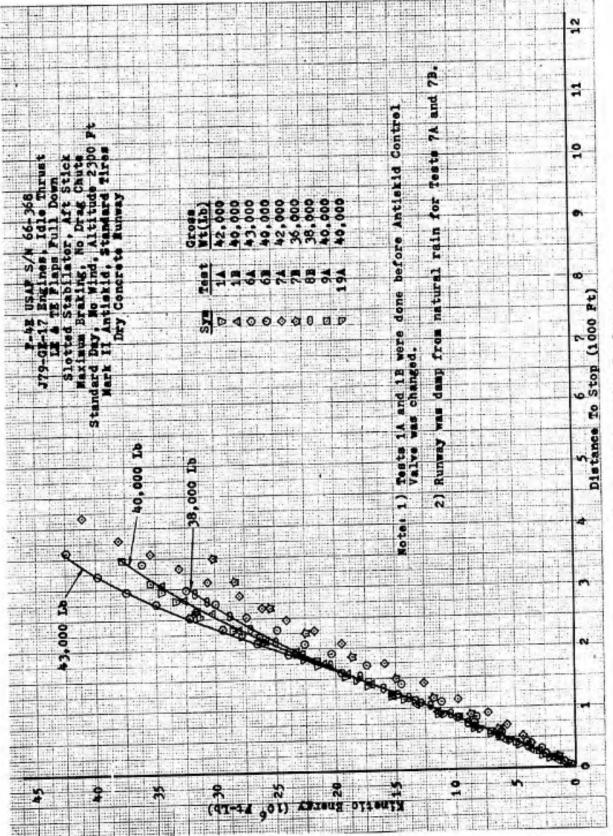


Figure Al Stopping Performance

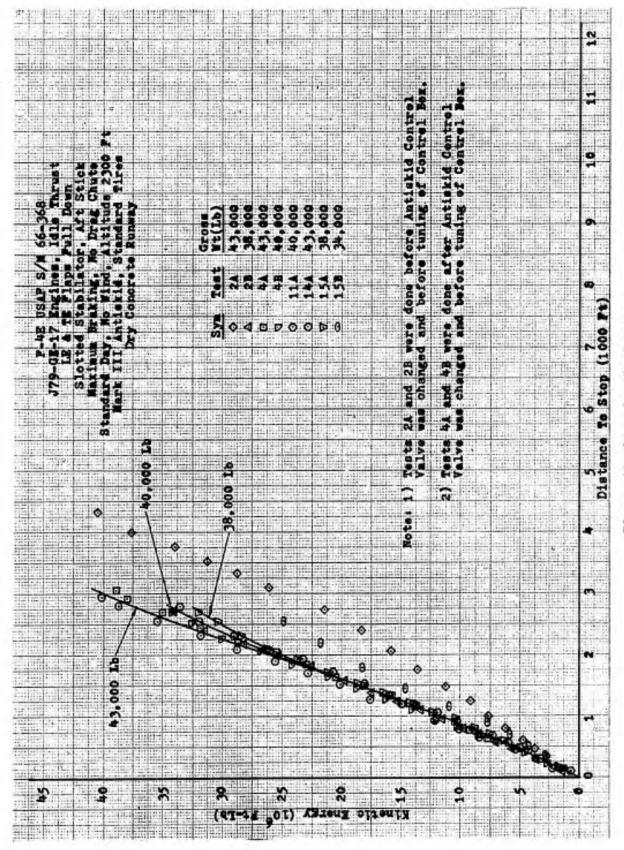
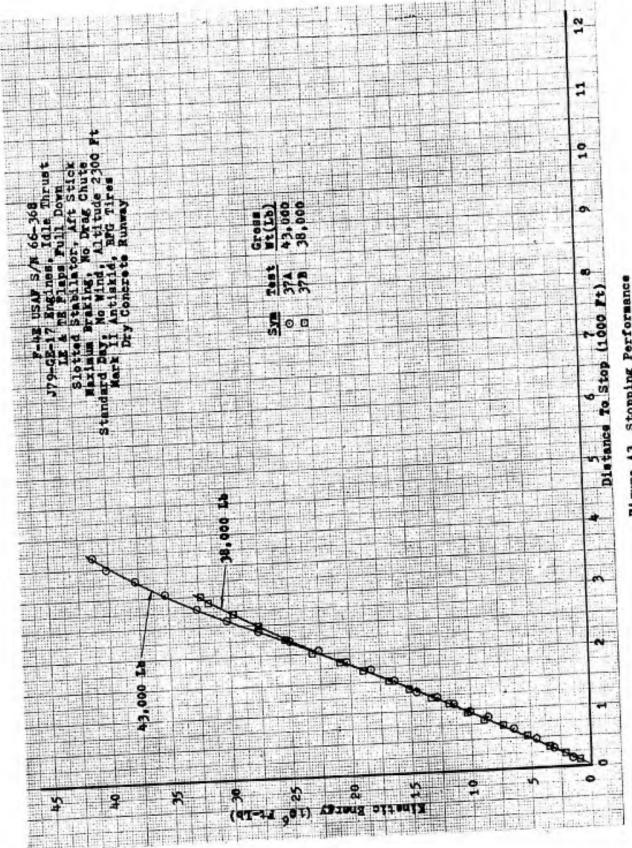
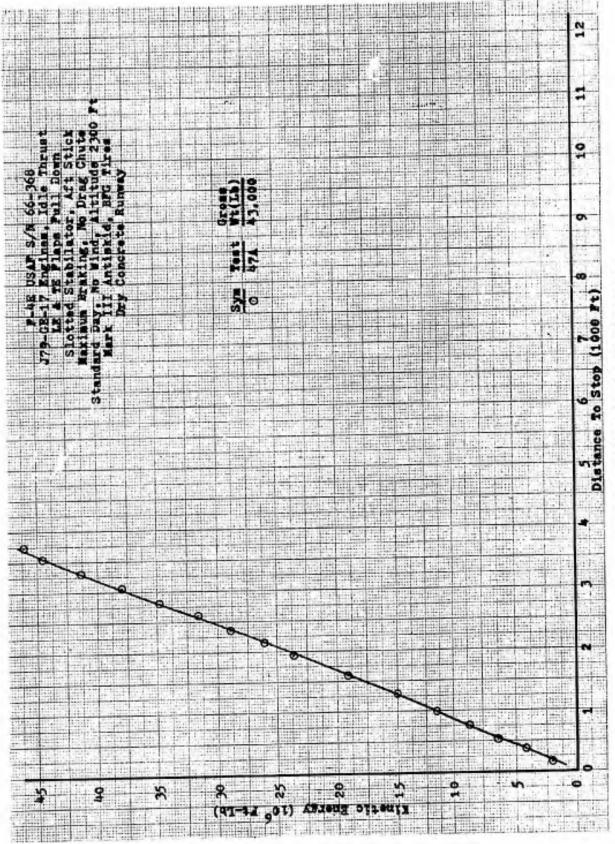


Figure A2 Stopping Performance

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Pigure A3 Stopping Performance



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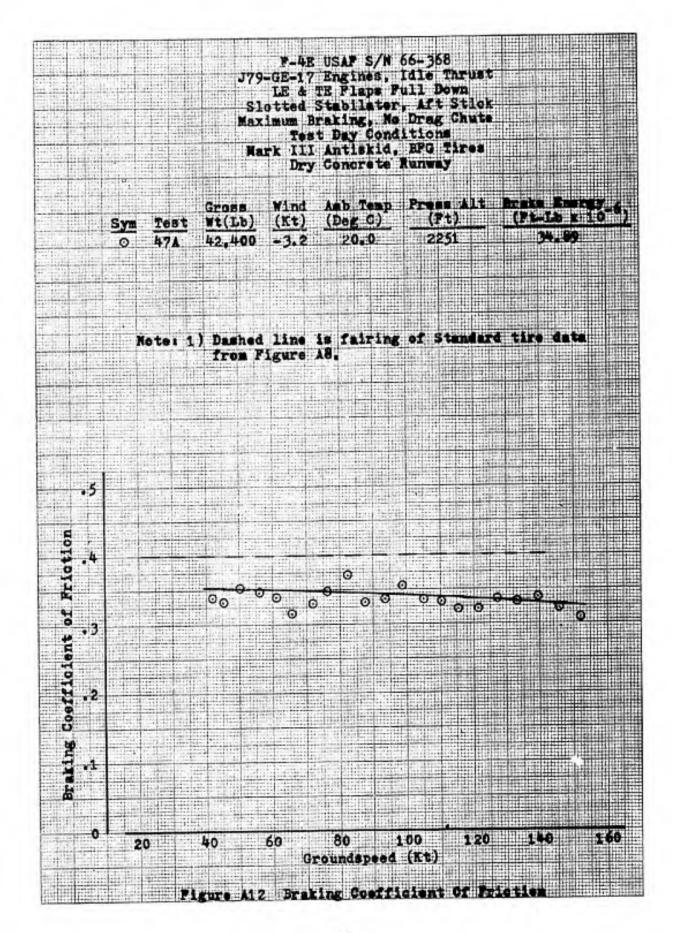
F-4E USAF S/N 66-368 J79-GE-17 Engines, Idle Thrust LE & TE Plaps Pull Down Slotted Stabilator, Aft Stick
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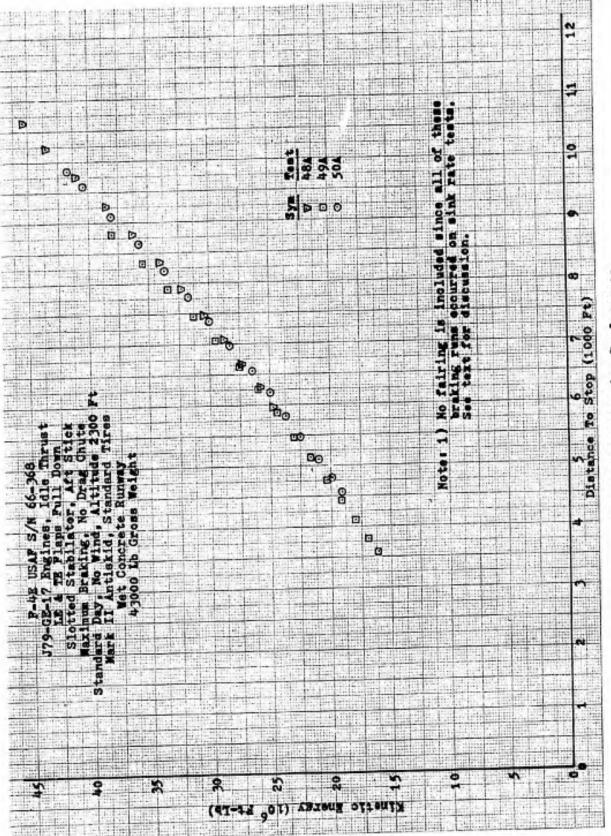
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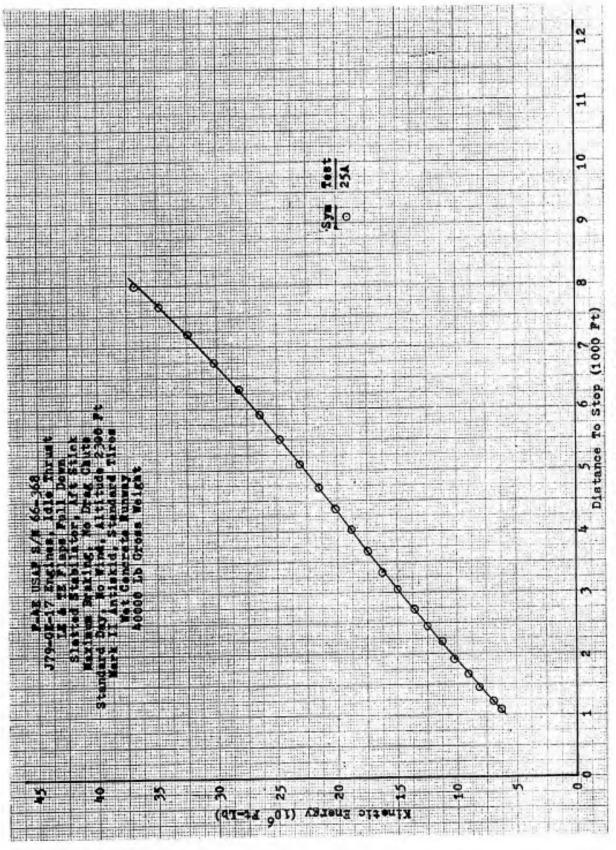
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Pigure A13 Stopping Performance



Pigure Al4 Stopping Performance

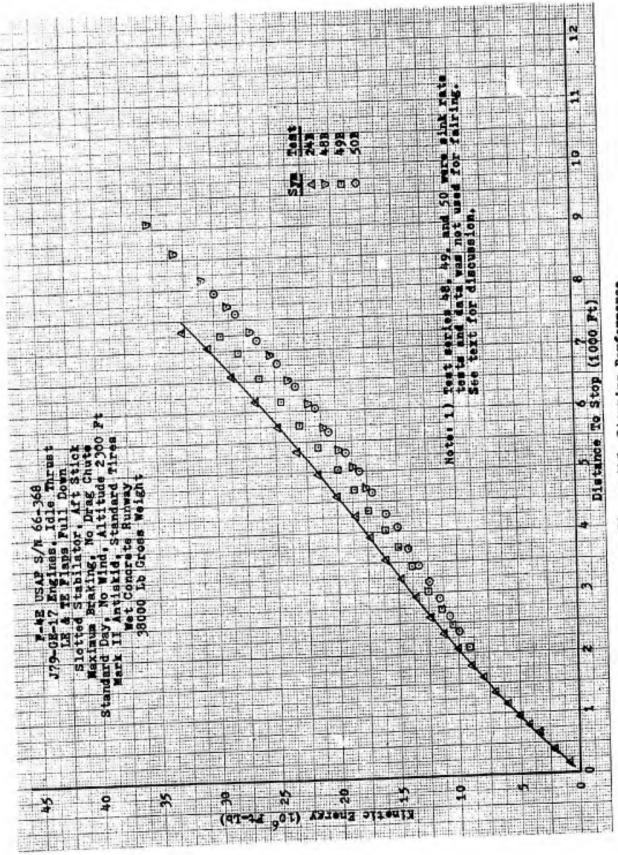


Figure A15 Stopping Performance

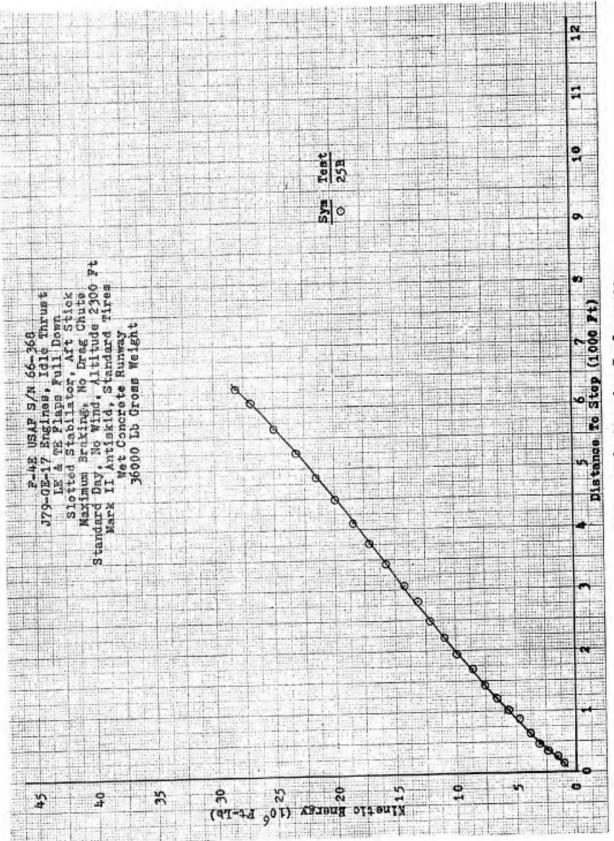


Figure A16 Stopping Performance

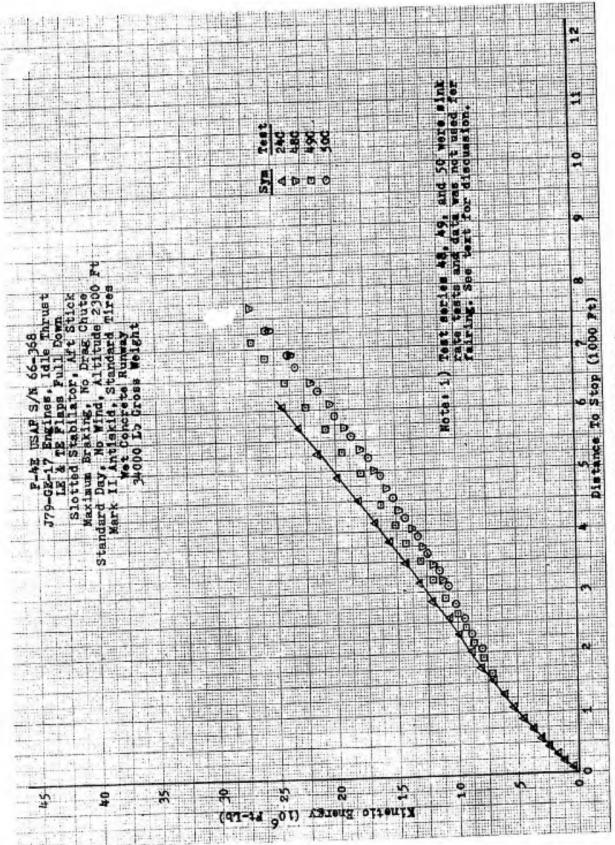
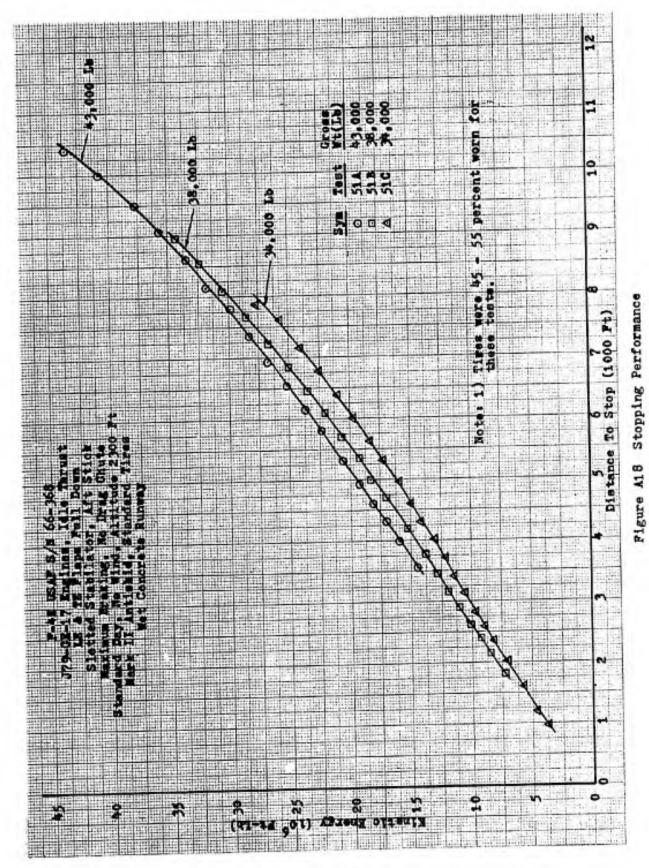
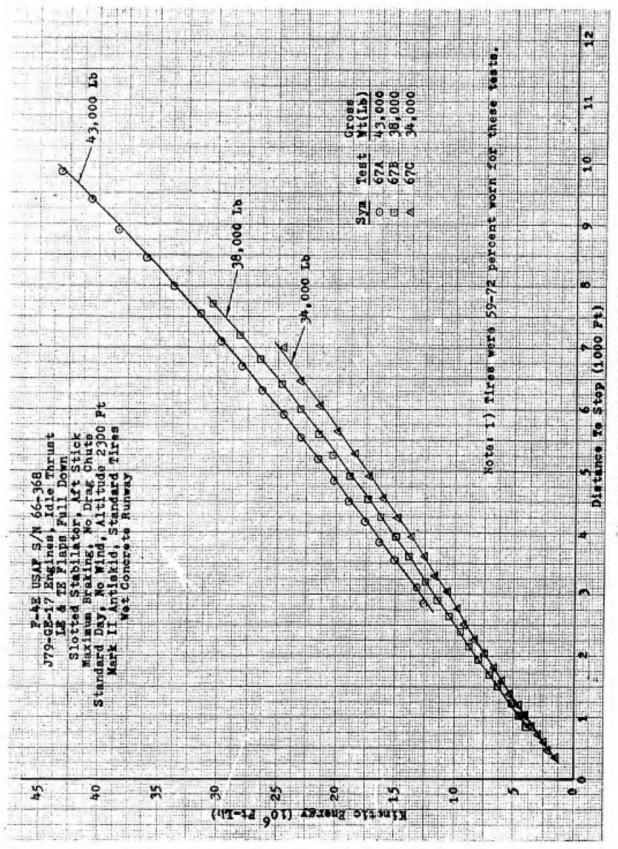


Figure A17 Stopping Performance





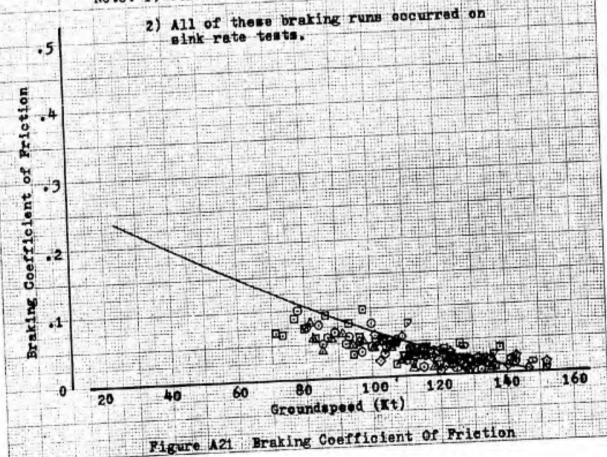
Pigure A19 Stopping Performance

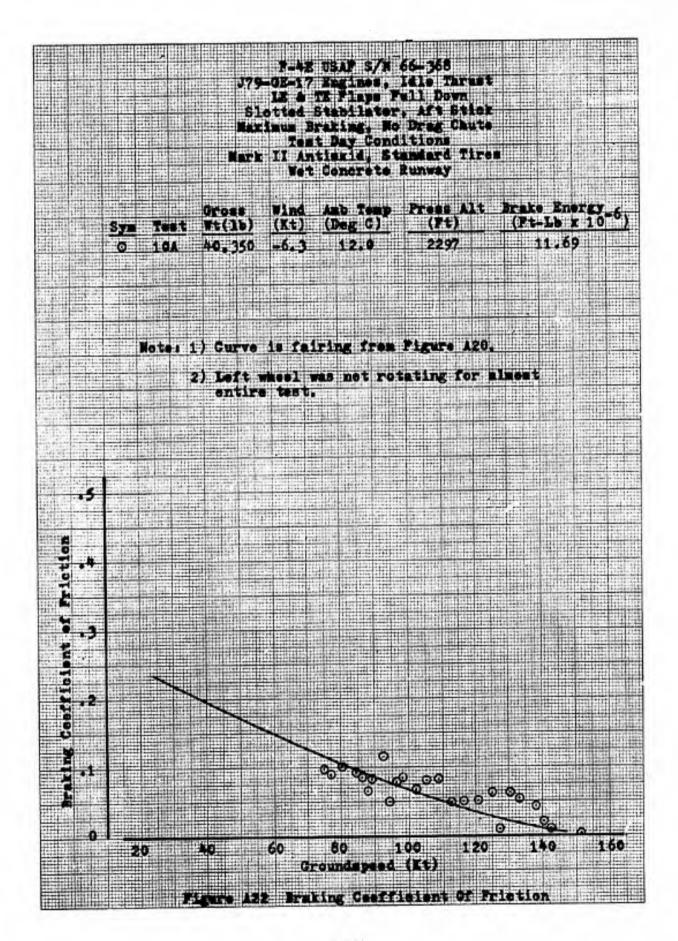
F-4E USAP S/N
GE-17 Engines, Idle Thrust
LE & TE Plaps Full Down
LE & TE Plaps F-4E USAF S/N 66-368 J79-GE-17 Engines, Idle Thrust Slotted Stabilator, Aft Stick Maximum Braking, No Drag Chute Test Day Conditions Mark II Antiskid, Standard Tires Wet Concrete Runway Wind Amb Temp Press Alt Brake Energy Gross Wt(Lb) (Kt) (Deg C) (Ft) (Ft-Lb * 10) Sym Test 0 243 37.786 -1.4 17.5 2254 15.48 33,636 -2.9 20.8 2257 13.05 40,086 -2.2 15.5 2288 10.98 36,086 2.4 18.8 2282 13.45 254 40,086 -2.2 25B 36,086 2.4 D Note: 1) Dashed line is fairing of Mark III data from Pigure A31. ent 20 40 60 80 100 120 140 160 Groundspeed (Kt)

F-AE USAP S/R 66-368 J79-GE-17 Engines, Idle Thrust IE & TE Flaps Full Down Slotted Stabilator, Aft Stick Estimus Braking, No Drag Chute Test Day Conditions Nark II Antiskid, Standard fires Wet Concrete Runway

		Gross.	Wind	Amb Temp	Press A	t Brace Energ	0-6
Sym	Test	Wt(Lb)	(Kt)	(Deg C)	2370	0.95	
Ò	48A	43.025	-4.1	21.5	2363	1.77	
0	48B	38,300	-6.5		· · · · · · · · · · · · · · · · · · ·	2,88	ii).
0	48C	34,550	-8.5	25.5	2360	4,23	
Ø	49A	43,200	0.0	15.0	2202	6.08	Till
0	49B	38,700	0.0		21 97	5,84	
0	49C	34,900	-0.9		2193	2.84	
D	50A	43,500	-2.0		2276	4.19	
0	50B	38,700			2272	3.80	
Δ	500	34,700		26.5	2272		
		1 1 100					

Note: 1) Curve is fairing from Figure A20,





F_4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust

LE & TE Plaps Full Down

Slotted Stabilator, Aft Stick

Maximum Braking, No Drag Chute

Test Day Conditions

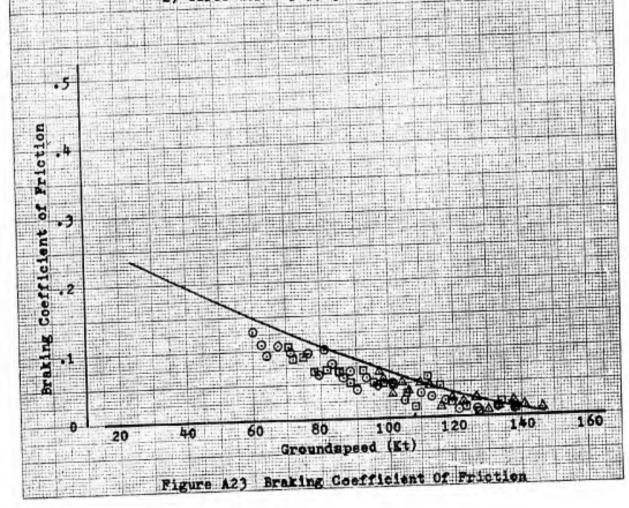
Mark II Antiskid, Standard Tires

Wet Concrete Runway

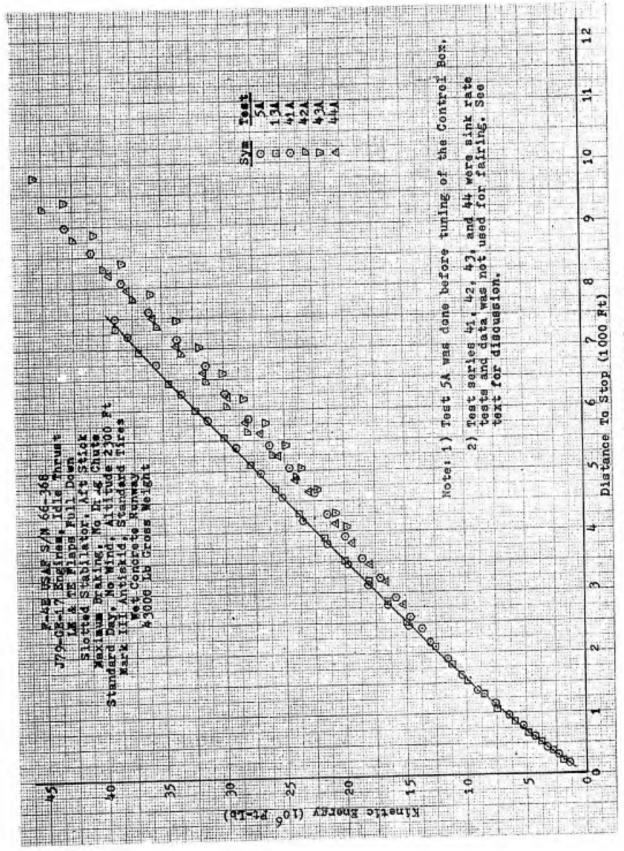
	Ores V	ind Amb Te	mp Press	Lt Brake	Lb x 10 6)
Sym Tes	t Wt(Lb) ((T) (Deg w	Control of the Contro	中央 电电子电话 化氯化物 化二氯化物 电电话 化二氯化物	4.73
A 51	43,200 -		Acces to a grant of the state o		6.73
0 511	Charles of the Control of the Contro	0.4 23.0 5.0 25.8			
0 510	34,475 =				

Note: 1) Curve is fairing from Figure A20.





		-	.179	AT 4 7	USAF S/N Engines,	Idle TREUS		
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+++	1		Max	demonstrate like	MAKINE. BO	-DI		
				Tes	t Day Cond	anderd Tir		
			max A	Wet	Concrete	Runway		
1.1					And Temp	Press Alt	Brake Energ (Pt-Lb x 1	y_
	0	Test	Wt(Lb)	Wind (Kt)		(Pt)		0
	Sym	67A	43.200	-5.6	14.4	2228	7.13 11.35	
	0	67B	38,600	-5.9	16.1 15.0	2227	11.37	
	0	67C	344500	-/->				
	- init							
	100			H. H.				
-	-		19.45					
		Note: 1) Curve	is fa	ring from	Pigure A20		
			2) Tires	were .	59-72 perc	ent worn fo	or those test	
	753							
1 15								
			434					
5	5							
		1 1 W.						
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Braking Coefficient of				(GEO)(D			2 4 4 A	



Pigure A25 Stopping Performance

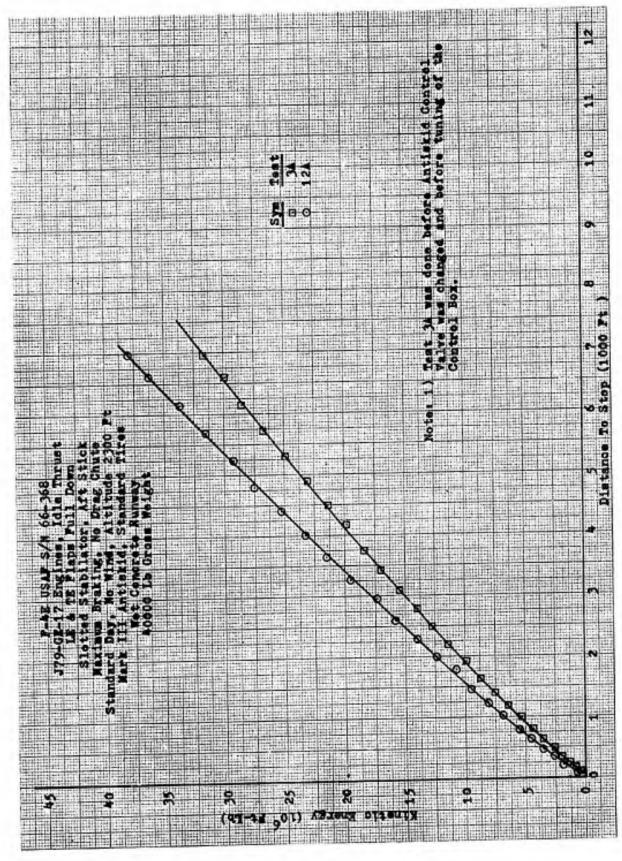


Figure A26 Stopping Performance

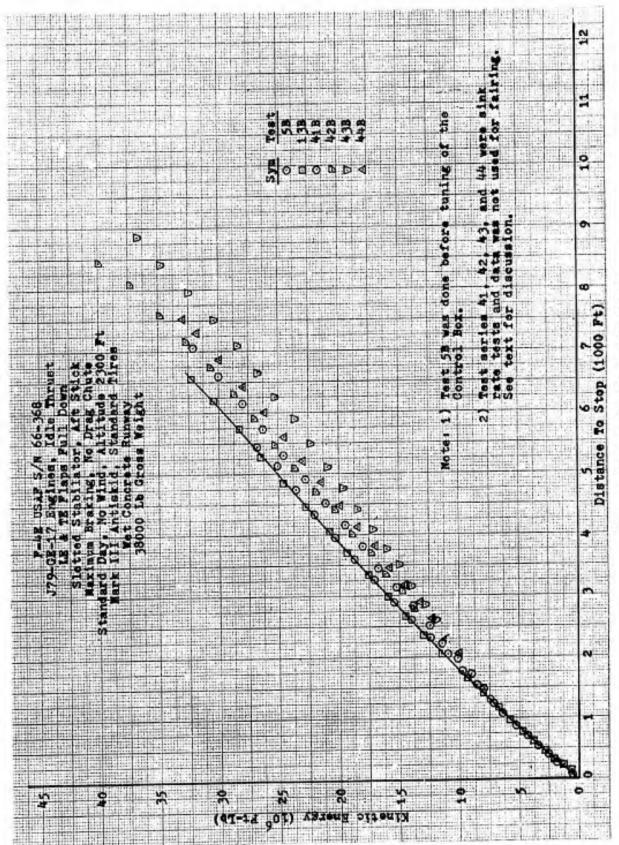
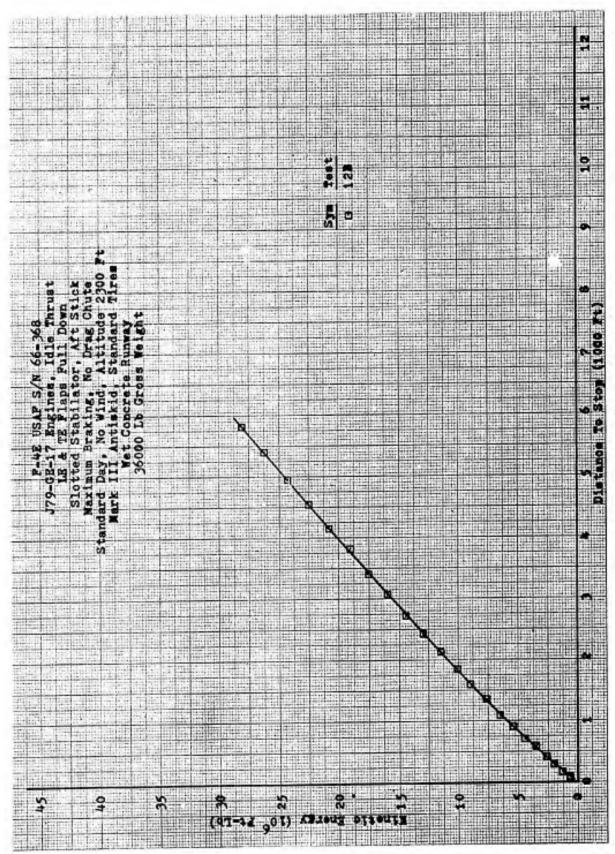
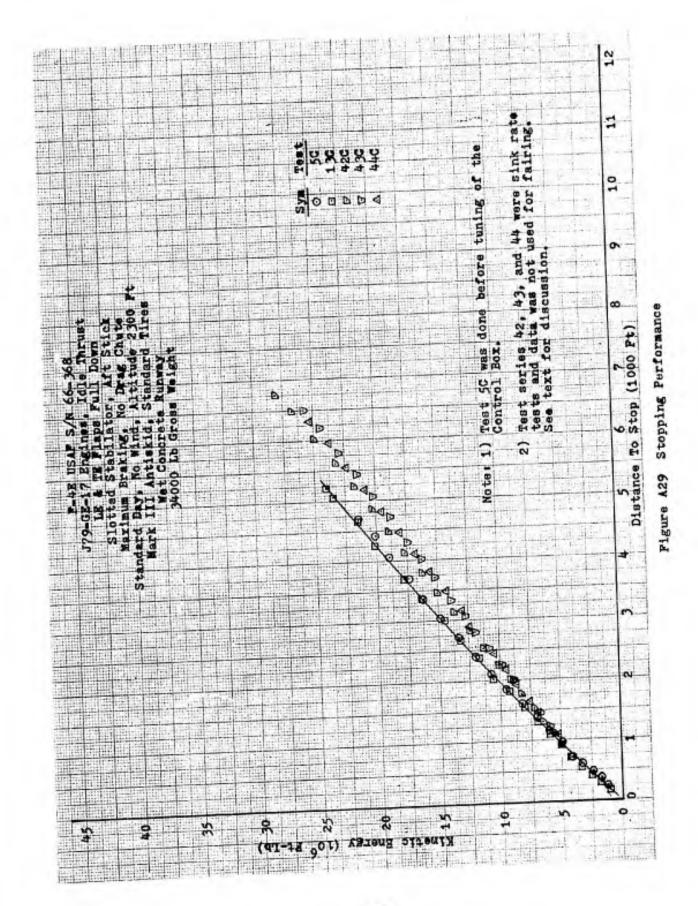


Figure A27 Stopping Performance



TOTAL PLANTS

Figure A28 Stopping Performance



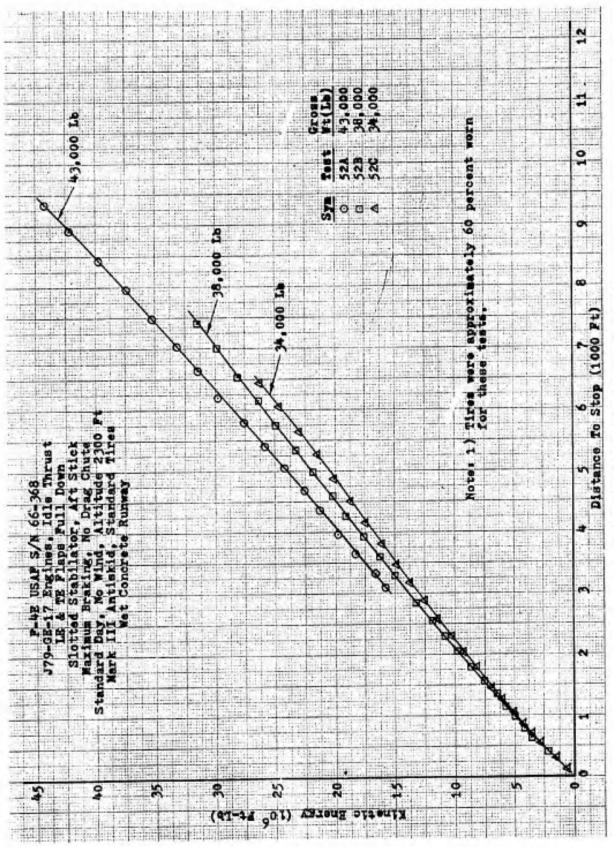


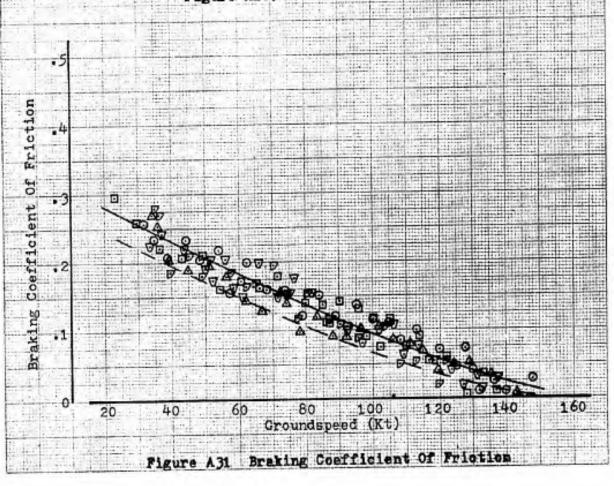
Figure A30 Stopping Performance

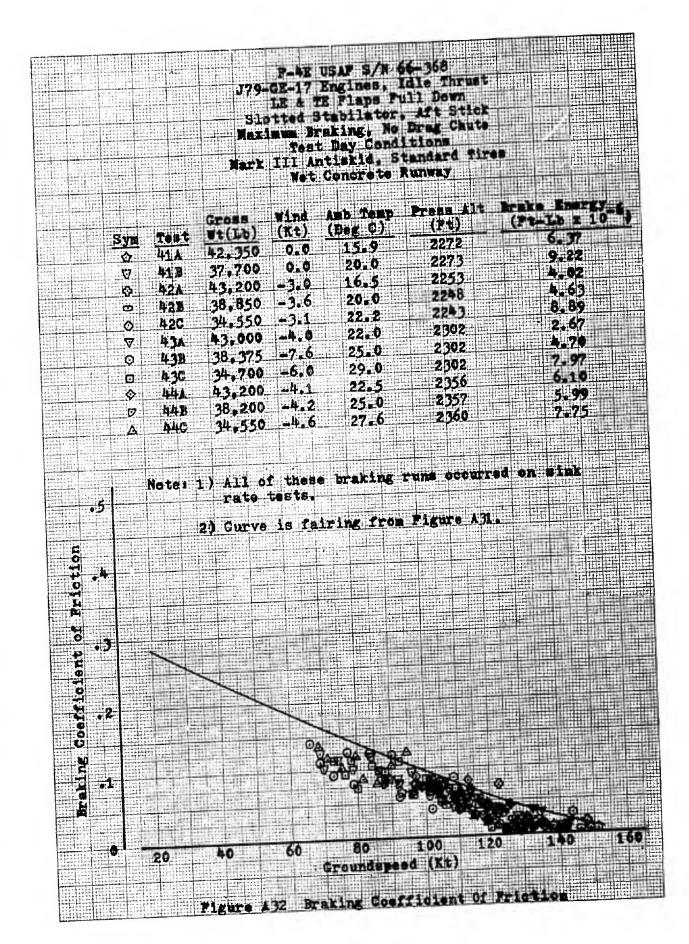
P-4E USAF S/N 66-368

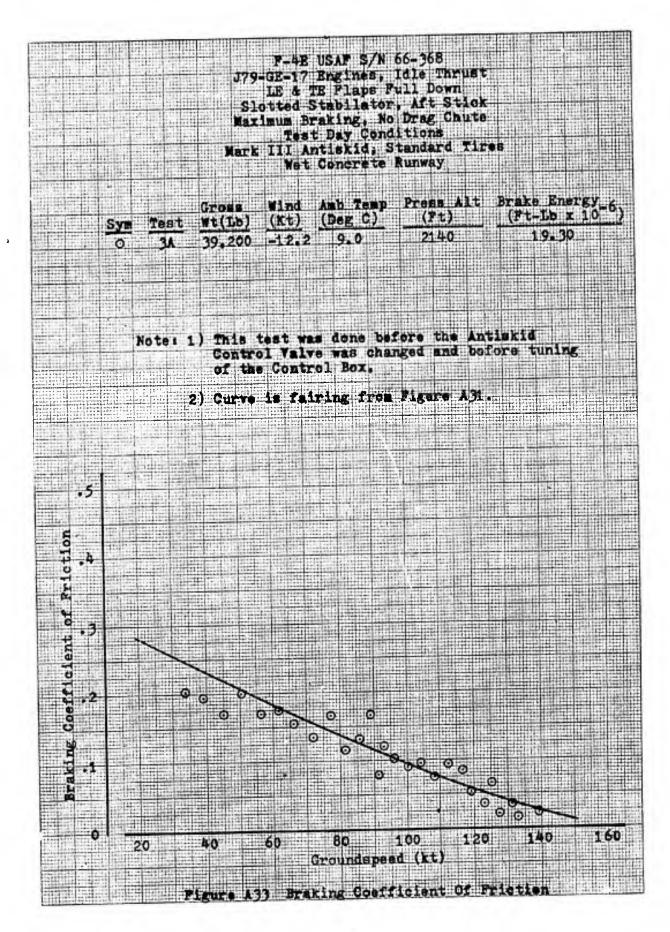
J79-GE-17 Engines, Idle Thrust
LE & TE Flaps Full Down
Slotted Stabilator, Aft Stick
Maximum Braking, No Drag Chute
Test Day Conditions
Mark III Antiskid, Standard Tires
Wet Concrete Runway

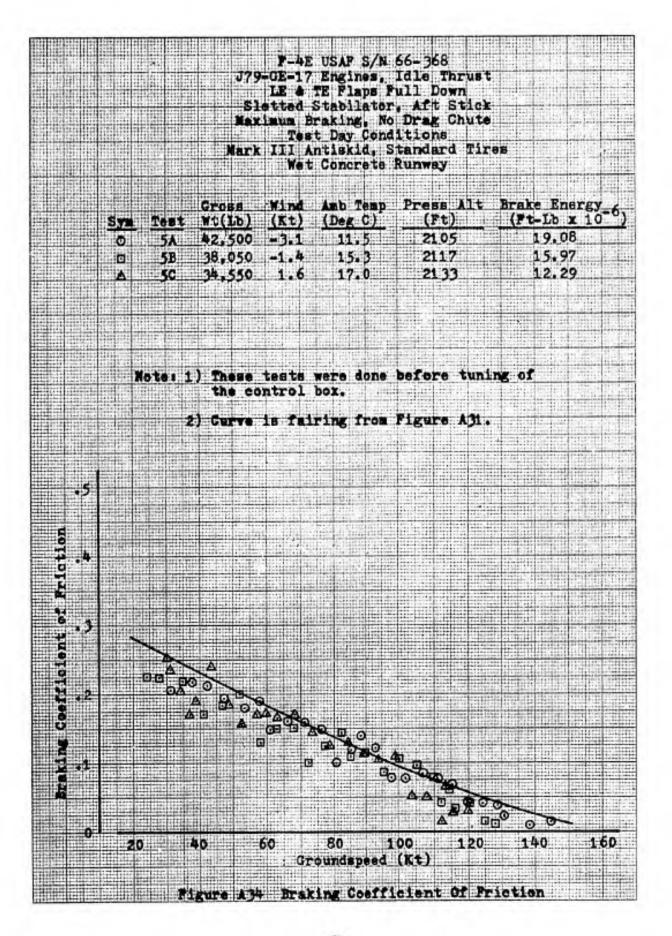
The state of	4-1-15	Gross	Wind	Amb Temp	Press	11+	Brake	Rherev	
200	1 -1 - 10	Contract of the Contract of th	many married breaks		the state of the s		Brake (Ft-L		10
Sym	Test	Wt(Lb)	(Kt)	(Deg C)	(Pt)	THE PROPERTY	17.1-1	OXIL	1
0	124	40,350	-6.5	3.7	226)	20	STREET, STREET, STREET,	
•	12B	36.050	-5.7	6.0	225	14012-06 242	100000000000000000000000000000000000000	35	
Δ	13A	42,200	-1.5	4.0	2119	TAX BARBOOK	at he collected in	.13	
₩ 🗸	1 3B	37,875	-3.0	7.0	2112	Checks to Both	1.6	4344 (47) (1422)	
D	1 3C	34,400	-1.8	9.0	210	3		3.21	
1	St. of 1911	Total de	49 11-1811-	The second second	The state of the s				1411111

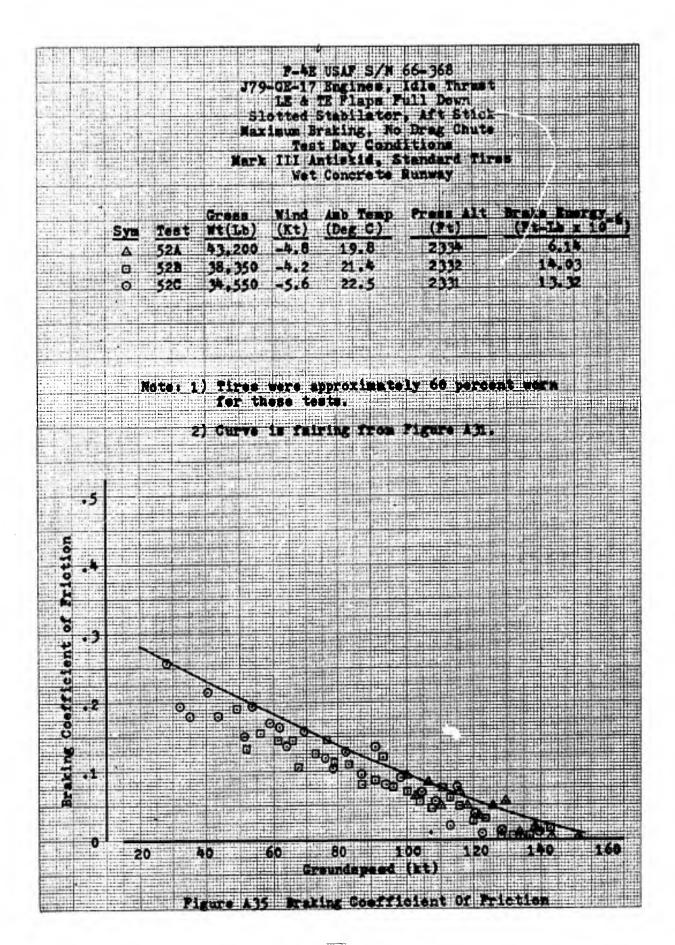
Note: 1) Dashed line is fairing of Mark II data from Figure A20.





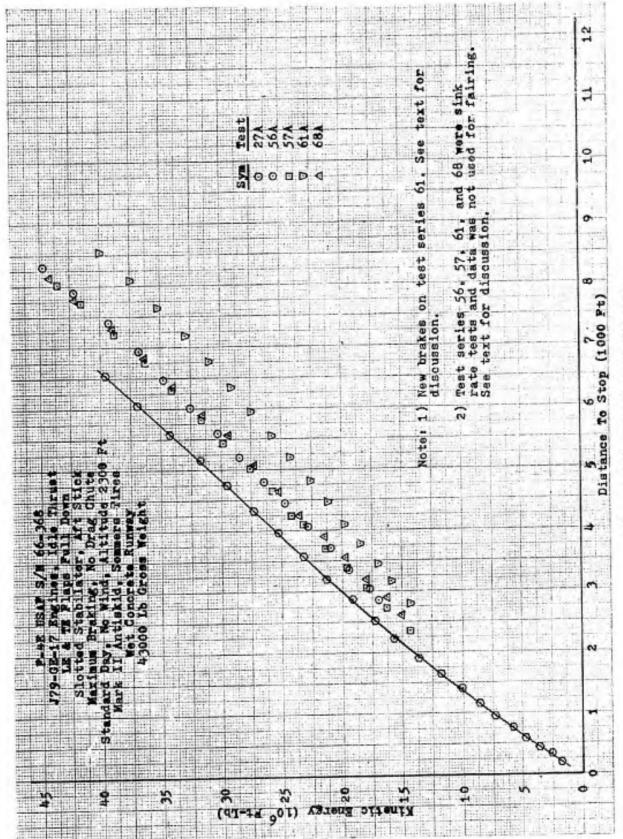






			TP P	79-	GE-17	USAF S Engine Down,	B. I	ile i	hrust Helf I	owa	
				Slo	tted	Stabila	tor,	Aft	Stick		
				laxi	rum B	raking, t Day (ondi	tions	CRUTE		
			Ma	rk	III A	ntiskio Concre	, St	andar	d fire		
					46.6	concre		UIVEC.			
			Gross		Wind	Amb Te	mp :	Press	Alt	brake E (Pt-L)	STET 4
	Sym	Test	Wt(L)		(Kt)	(Deg C					
	0	46A 46B	43,20			17.8		224	38	13.0	
	Δ	46C			-0.4	22.	The state of the s	22		13.	
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4. T											
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Braking Coefficient											
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0											
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r.								Δ		04° 04	00 B0 B0
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- 0									4 5.0	140	160
in land	2	9	40		60	80 rounds	11		120	140	Tot

			yark	TOS	Day Cond stickid, S Concrete	Drag Chut Itions Sandard Ti	30	
	0	5A	38,550	Wind (Et) 0.0	Amb Temp (Deg C)	Press 111t	Broke Sher (Pt-lb x) 4.60 5.62 6.69	¥-6
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Friotion								
8,,								
Paking Coefficient								
2.1						٨		e e



Pigure A38 Stopping Performance

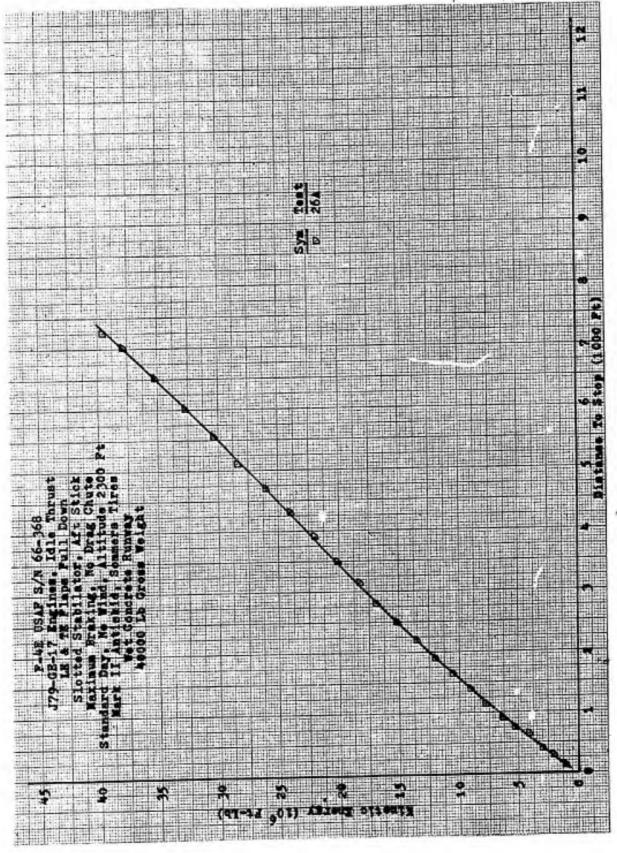


Figure A39 Stopping Performance

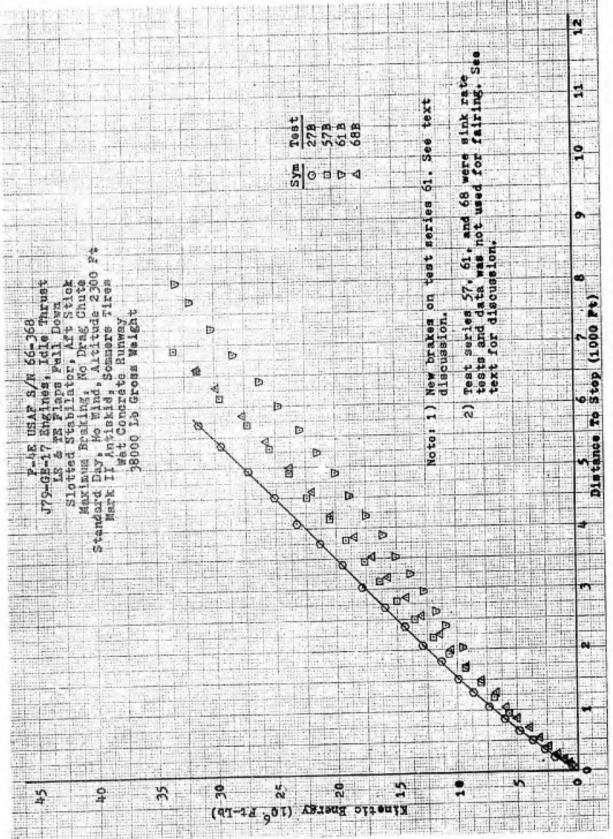


Figure A40 Stopping Performance

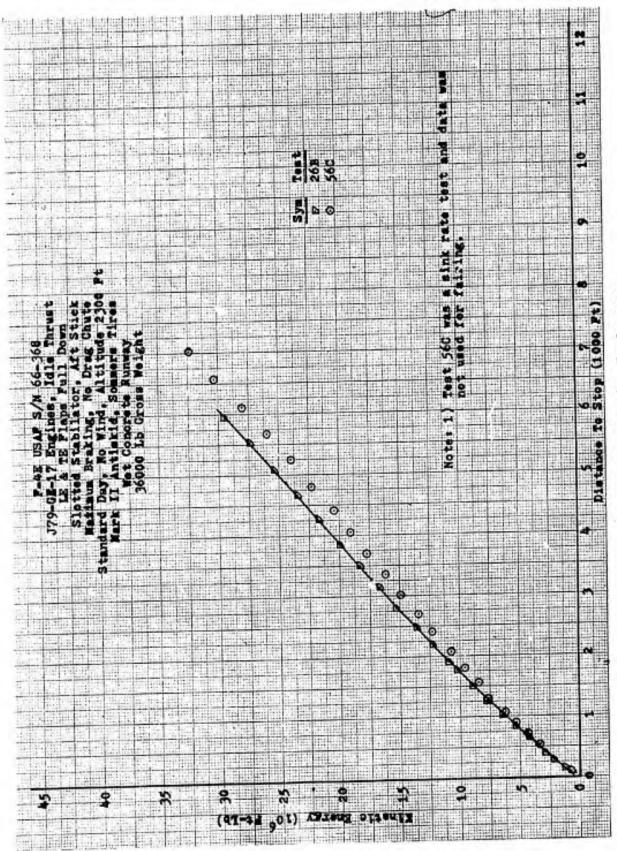


Figure A41 Stopping Performance

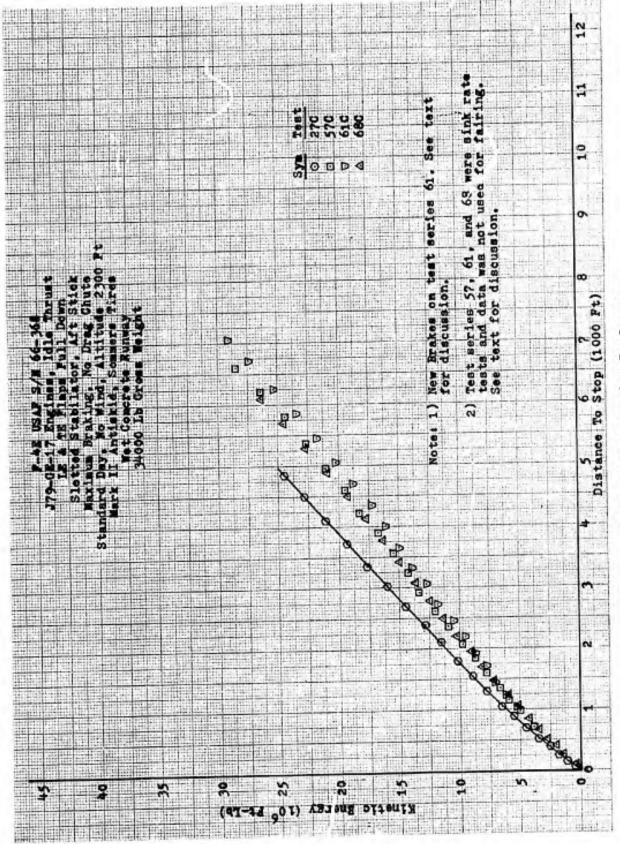


Figure A42 Stopping Performance

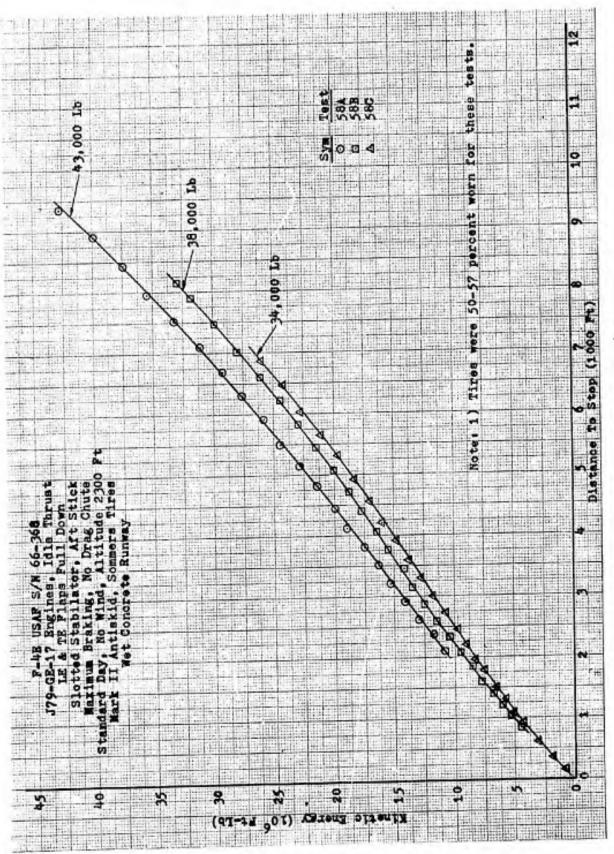


Figure A43 Stopping Performance

P-4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust

LE & TE Flaps Full Down

Slotted Stabilator, Aft Stick

Maximum Braking, No Drag Chute

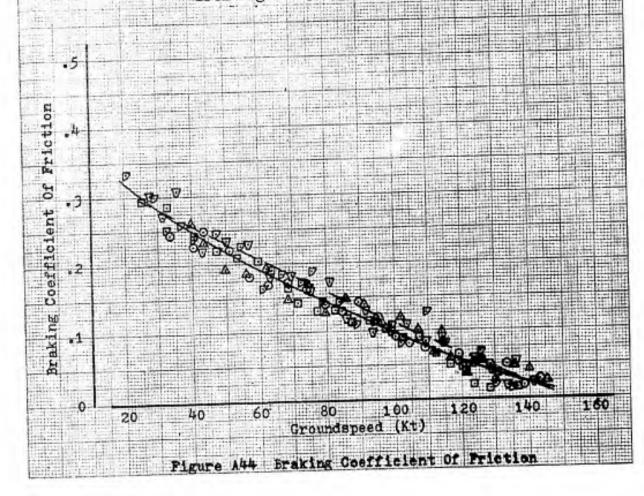
Test Day Conditions

Mark II Antiskid, Sommers Tires

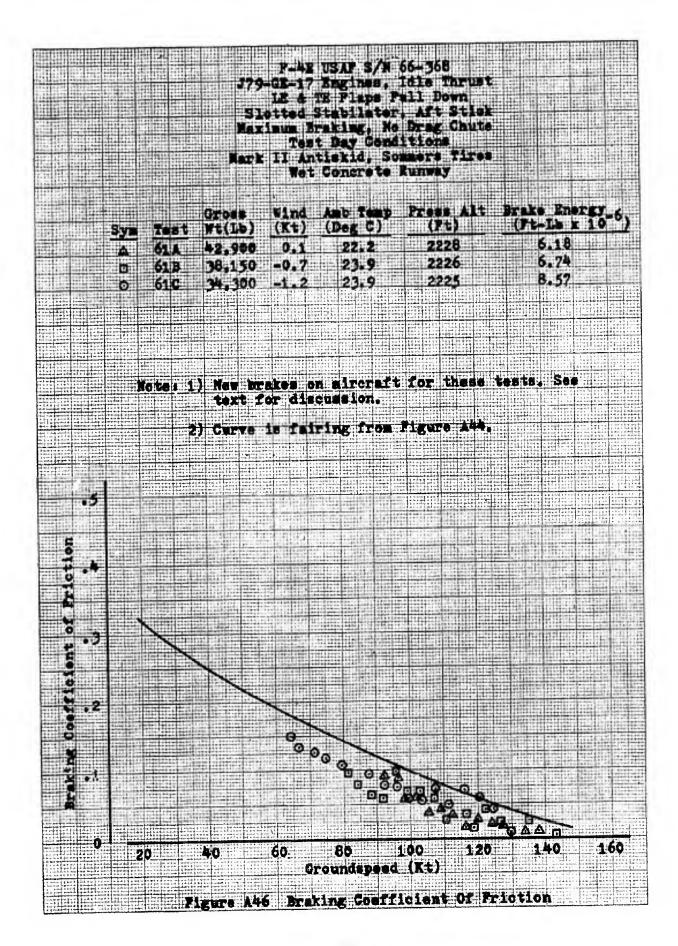
Wet Concrete Runway

		Gross	Wind	Amb Te	mp .	Press	Alt	Brake (Pt-	Ener	EV_6
Sym	Test	Wt(Lb)	(Kt)	(Deg C						
0.	26A	39,436	-2.3	15.8		100	12-10-14-04-Files	1		
O	26B	35,786	-1.0	19.0)	227	Control to be built	1		
۵	27A	43,200	-3.5	12.1	1111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	207	Time City was done	2	and a second and the second	
Ū	27B	38,350	-5.7	14.2		206			6 62	
D.	27C	34.550	-5.2	16.0		206	2			

Note: 1) Dashed line is fairing of Mark III data from Figure A54.



			S1 Mex	-GB-17 LE & otted imum B Tes	TE Plaps F Stabilator raking, No t Day Cond	Idle Thrust ull Down Aft Stick Drag Chute Itions mmers Tires		
			Gross	Wind	Amb femp	Press Alt	Brake Energ	у_6.
	Sym	Test	Wt(Lb)	(Kt)	(Deg C)	(Ft)	(Pt-Lb x 1	0)
	Ò	56A	43,250		17.5	2266	6.46	
	0	56C	35,200	-4.4	21.0	2253	13.26	
	0	57A	43,200		18.3	2229	7.67	
	v	57B	38,300	-4.9	18.3	2228	11.93	
	0		34,550	Company of the Compan		2225	10.65	
	A	68A	42,600			2190	7.87	
	0	68B	37.800		12.2	2185	15.36	
	0	68C	34,100		15.0	2183	13.75	
Chicken.	i cala di							
C AND DATE OF		to the second second			A RESTORATE OF A LABOUR SHOW AND A PROPERTY OF A PROPERTY			and the second second
							ed on	
		Note: 1) All of	these	braking)	runs occurr	ed on	
			sink I	ate to	88 68.			
			sink I	ate to	88 68.			
.5			sink I	ate to	88 68.	runs occurr Pigure A44		
			sink I	ate to	88 68.			
			sink I	ate to	88 68.			
			sink I	ate to	88 68.			
			sink I	ate to	88 68.			
			sink I	ate to	88 68.			
Frietion			sink I	ate to	88 68.			
of Friction			sink I	ate to	88 68.			
of Friction			sink) 2) Gurve		88 68.			
of Friction			sink) 2) Curve		88 68.			
of Frietion			sink) 2) Curve		88 68.			
of Friction			sink) 2) Curve		88 68.			
of Friction			sink) 2) Gurve		88 68.			
of Friction			sink) 2) Curve		88 68.			
of Friction			sink) 2) Curve		88 68.			
of Friction			sink) 2) Curve		88 68.			
of Friction			sink) 2) Curve		88 68.			
ng Coefficient of Friction			sink) 2) Curve		88 68.			
Braking Coefficient of Friction			sink) 2) Curve		88 68.			•
of Friction			sink) 2) Curve		iring from			& 160



F_4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust

LE & TE Plaps Full Down

Slotted Stabilator, Aft Stick

Maximum Braking, No Drag Chute

Test Day Conditions

Mark II Antiskid, Sommers Tires Wet Concrete Runway Gross Wind Amb Temp Press Alt Brake Emergy Sym Test Wt(Lb) (Kt) (Deg C) (Pt) (Pt-Lb x 10 6)

△ 58A 43.500 +3.7 17.8 2274 9.18

□ 58B 38.550 -2.4 20.0 2271 10.13

○ 58C 34.550 -2.8 22.8 2268 12.42 Note: 1) Tires were 50-57 percent worm for these to 2) Curve is fairing from Figure 144. 0 20 46 60 80 100 120 140 Groundspeed (Kt) Please A47 Braking Coats Clant Of Problem

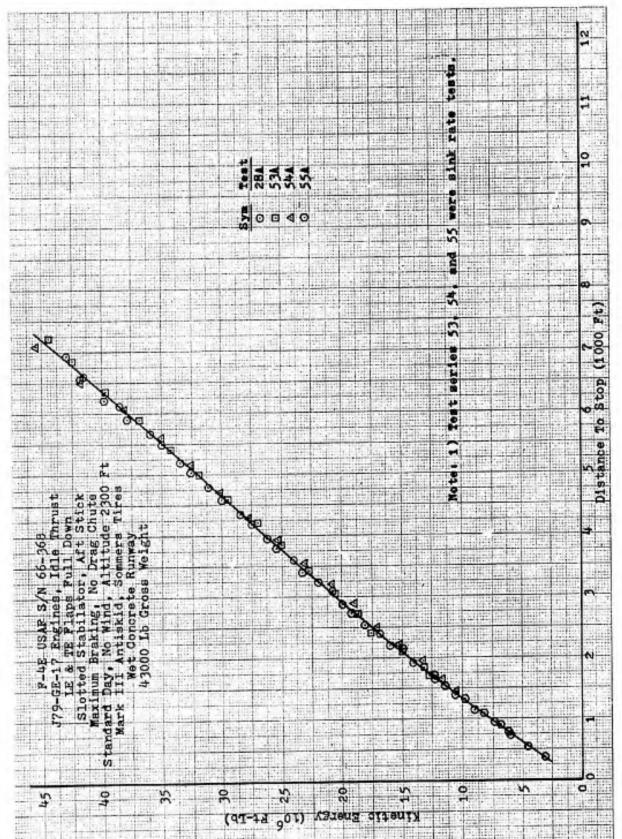


Figure A48 Stopping Performance

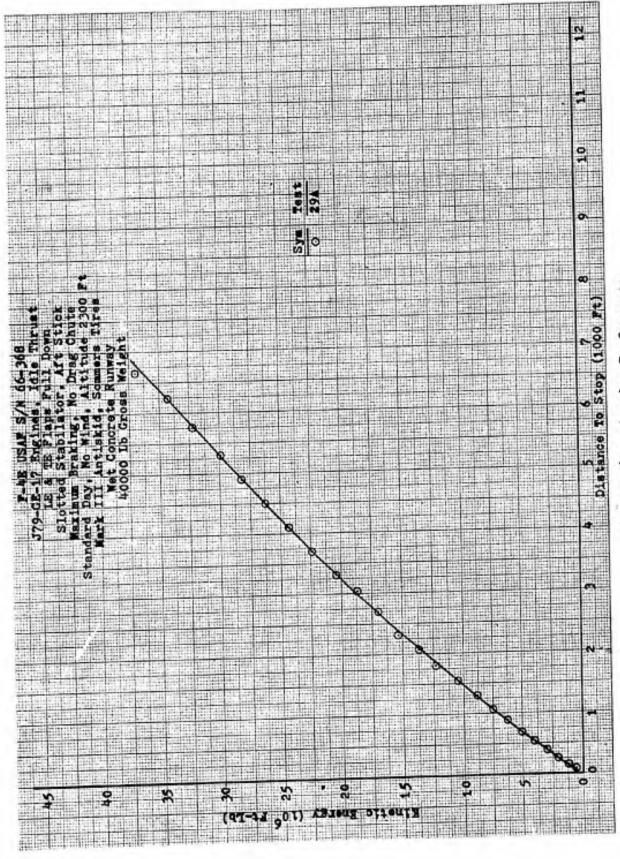


Figure A49 Stopping Performance

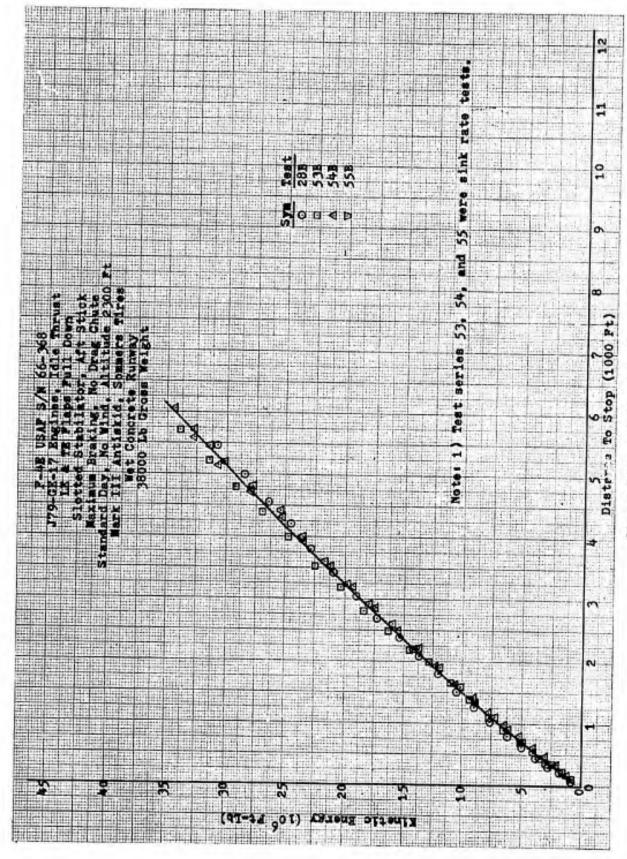
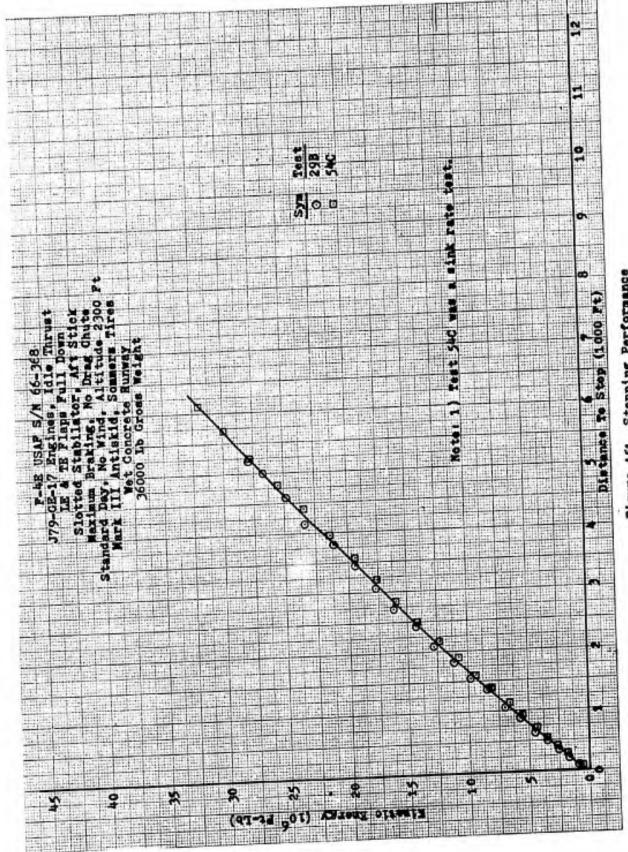
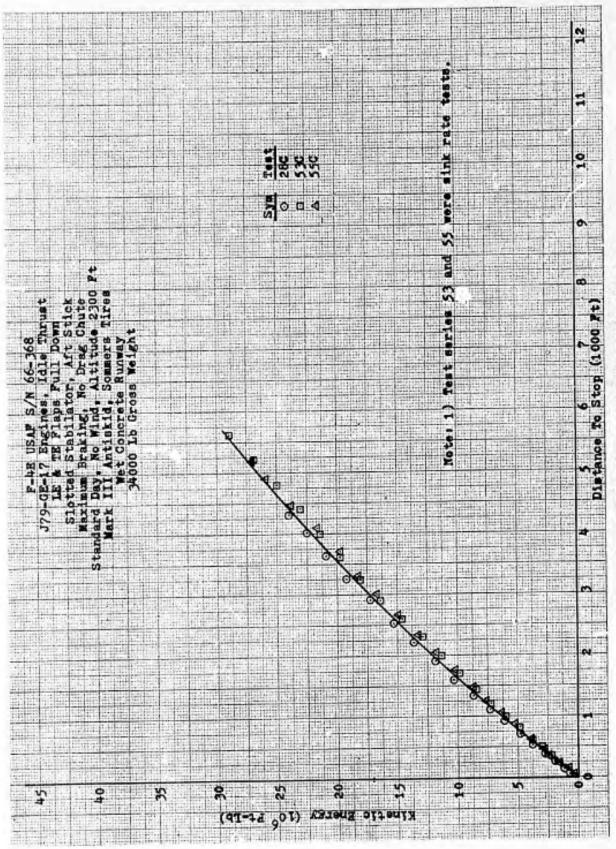


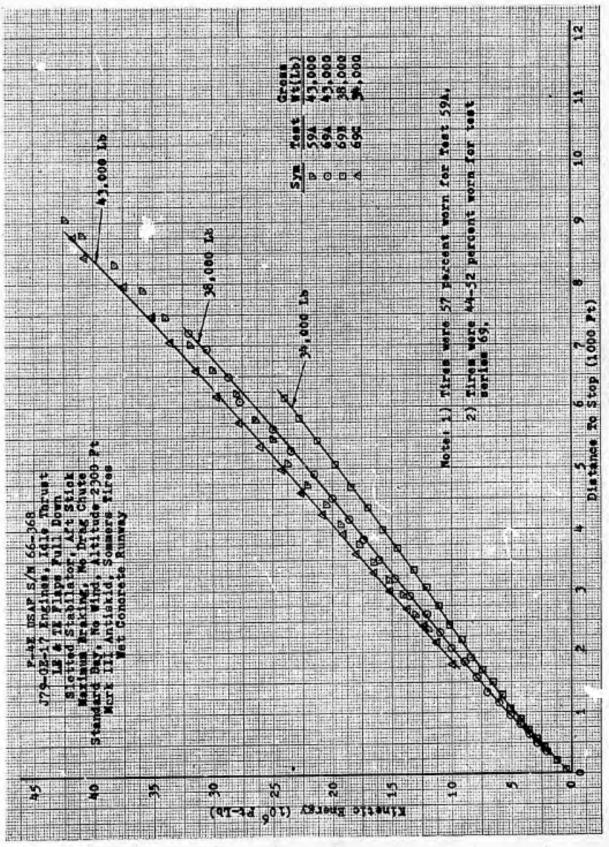
Figure A50 Stopping Performance



Pigure A51 Stopping Performance



Pigure A52 Stopping Performance



Pigure A53 Stopping Performance

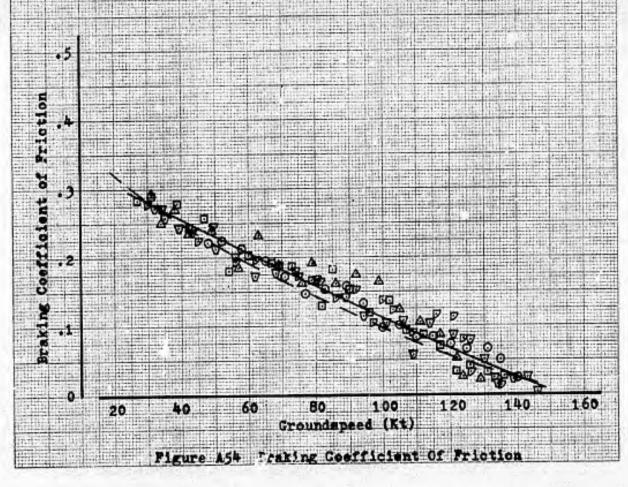
P-4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust
LE & TE Plaps Full Down
Slotted Stabilator, Aft Stick
Maximum Braking, No Drag Chute
Test Day Conditions

Mark III Antiskid, Sommers Tires
Wet Concrete Runway

	nd Amb Temp Pro	ess Alt Brake	Energy
Grees, Vi	Annual Control of the	Peet) (Ft-L	Energy_6 b x 10)
Sym Test Wt(Lb) (K		The state of the s	
O 28A 43.500 -2	.5 12.6	and constant or between second part of providing a	-59
m 283 38,500 -2		2055	. 37
A 28C 34,450 +2	The property of the party of th	2051 15	. 81
A CONTRACTOR OF THE PROPERTY O	CHEST GOOD CONTINUES OF THE STREET	Control Control Property and Party Control Control Control	.62
♥ 29A 40,500 -5		(1987年) 1987年 日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本	1.12(0.4 - 1.040 + 15) + 1) + 1
D 29B 36,375 -4	.1 18.7	2122 17	.80

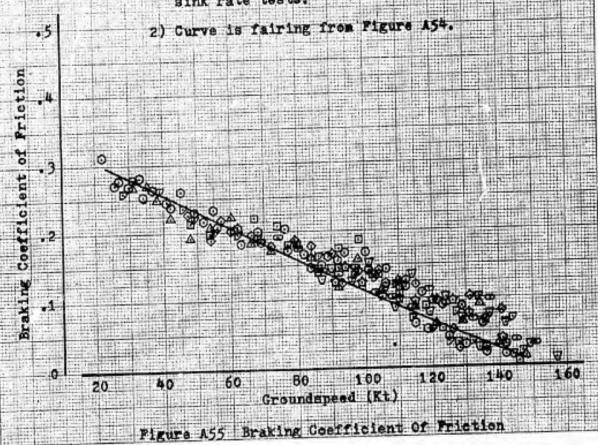
Note: 1) Dashed line is fairing of Mark II data from Pigure A44.



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Me.	conc	Lere	Maio			41121
	GE-17 LE & tted mum l Ter	GE-17 Engl IR & TR F1 Steed Stabi Imum Brakin Tent Day III Antisk	GE-17 Engines, IR & TR Flaps F Steed Stabilator Imum Braking, No Tent Day Cond III Antiskid, S	GE-17 Engines, Idle IR & TR Flaps Full Steed Stabilator, As Inum Braking, No Dr. Tent Day Condition III Antiskid, Somm	IE & TE Plaps Full Dow steed Stabilator, Aft S mum Braking, No Drag C Tent Day Conditions	GE-17 Engines, Idle Thrus IR & TE Flaps Full Down Steed Stabilator, Aft Stic Imum Braking, No Drag Chut Tent Day Conditions III Antiskid, Sommers Tir

			Gross	Wind	Amb Temp	Press Alt	Ft-Ib I 10
116	Sym	Test	At(TP)	(Kt)	(Deg C)	The second second second second second second second	
153	V	53A	43,200	-3.4		23331	12.67
	0	53B	38,200	-3.1	19.0	2332	20, 31
	в	53C	34,550	-6.1	21.0	2332	13.39
	· O	54A	43,200	-6.6	17.2	2291	14.05
	. •	54B	38,550	-6.3	18.5	2287	20.55
	Á	54C	35,050	-7.4		2286	18,63
	0	55A	43,200	-5.2	17.0	2289	18.98
	D	55B	38,350	-6.4	22.0	2287	21.28
	0	_55C_	34,400	-7.3	22.5	2285	18.39
1100	district.	SHE PROPERTY.					

Note: 1) All of these braking runs occurred on sink rate tests.

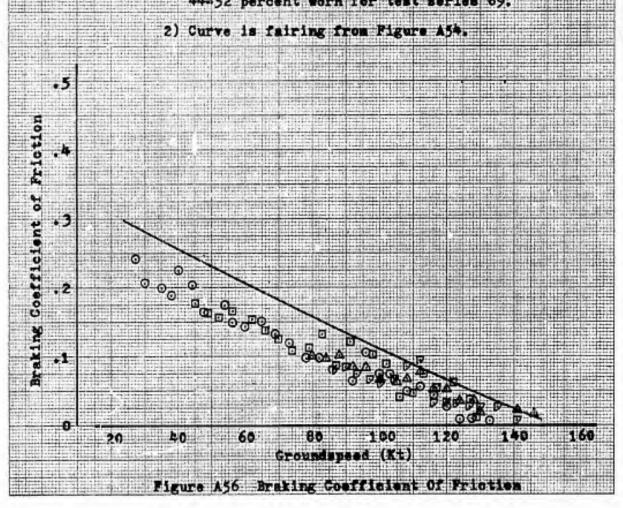


J79-GE-17 Engines, Idle Thrust LE & TE Plays Full Down Slotted Stabilator, Aft Stick Maximum Braking, No Drag Chute Test Day Gonditions Mark III Antiskid, Sommers Tires Wet Concrete Runway

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I	Sy	. !	l'e#	ŧ i							16			(ľt)			t-	Lb	erg z 1	o ')
Ē	D	uiiii)	59A	3H)	43.	350		3.	5	1515	35.	0	511	2	30					8, 5	9		50
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Note: 1) Tires were 57 percent worn for test 59A and 44-52 percent worn for test series 69.





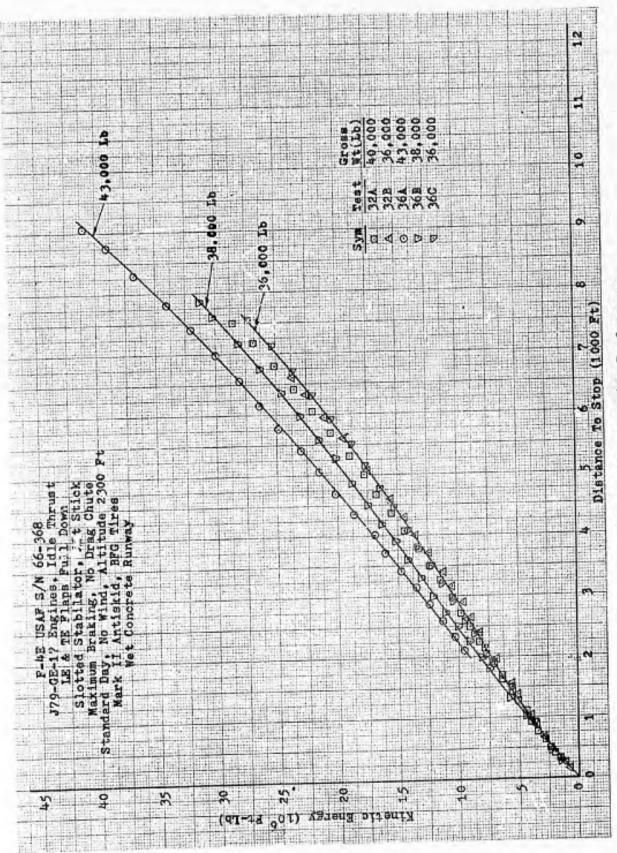


Figure A57 Stopping Performance

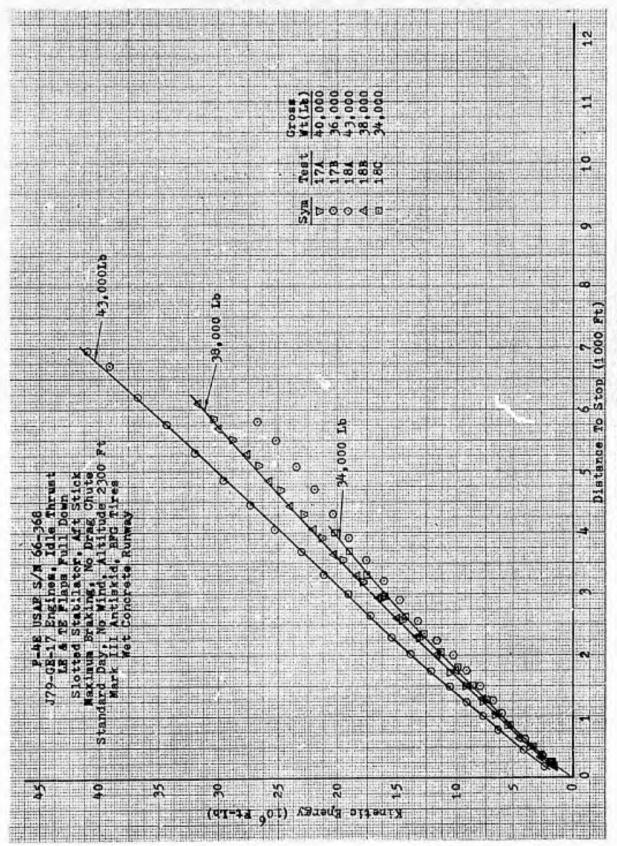


Figure A58 Stopping Performance

F-4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust

IE & TE Flaps Full Down

Slotted Stabilator, Aft Stick

Maximum Braking, No Drag Chute

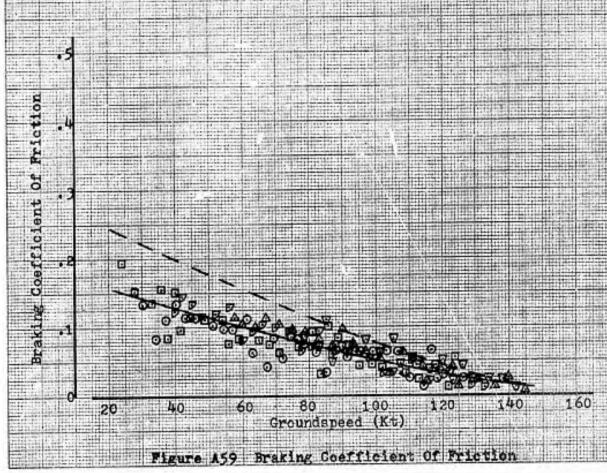
Test Day Conditions

Mark II Antiskid, BFG Tires

Wet Concrete Runway

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Note: 1) Dashed line is fairing of Mark III data from Pigure A60.



F-4E USAF S/N 66-368

J79-GE-17 Engines, Idle Thrust

IE & TE Flaps Full Down

Slotted Stabilator, Aft Stick

Maximum Braking, No Drag Chute

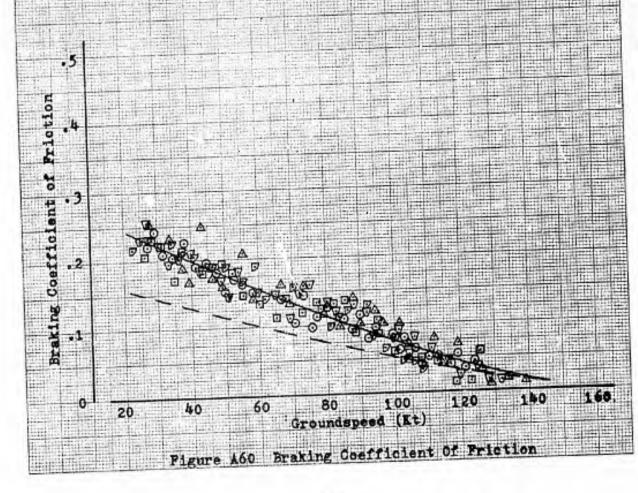
Test Day Conditions

Mark III Antiskid, BFG Tires

Wet Concrete Runway

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Note: 1) Dashed line is fairing of Mark II data from Figure A59.



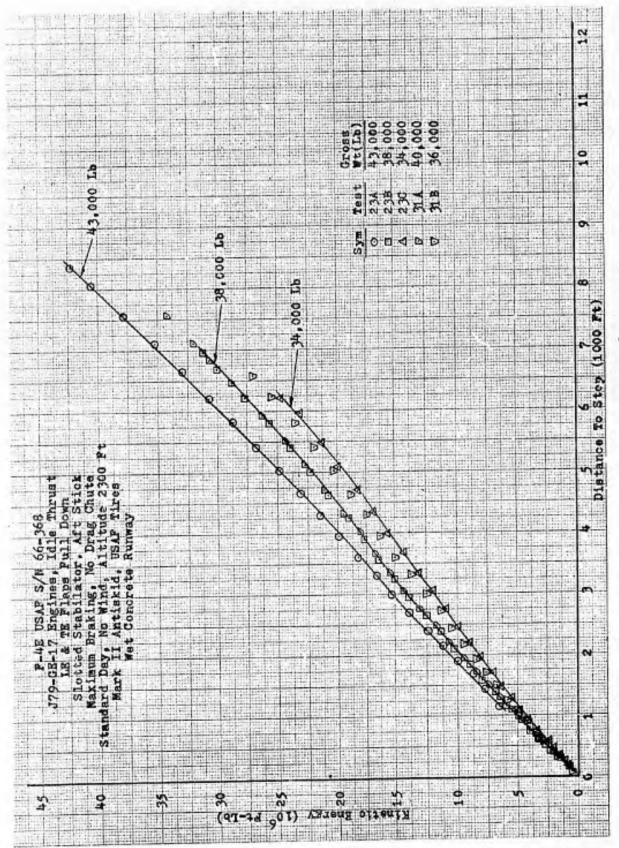


Figure A61 Stopping Performance

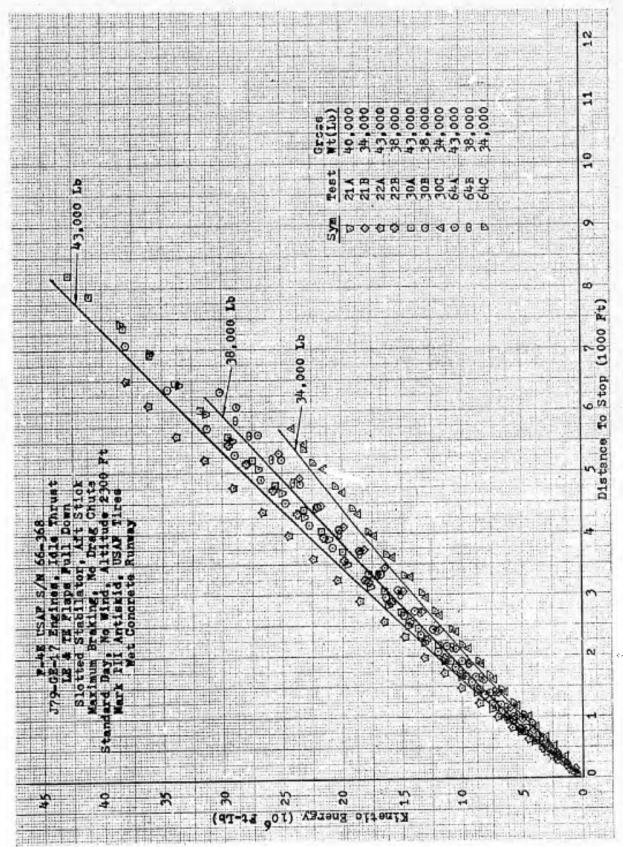
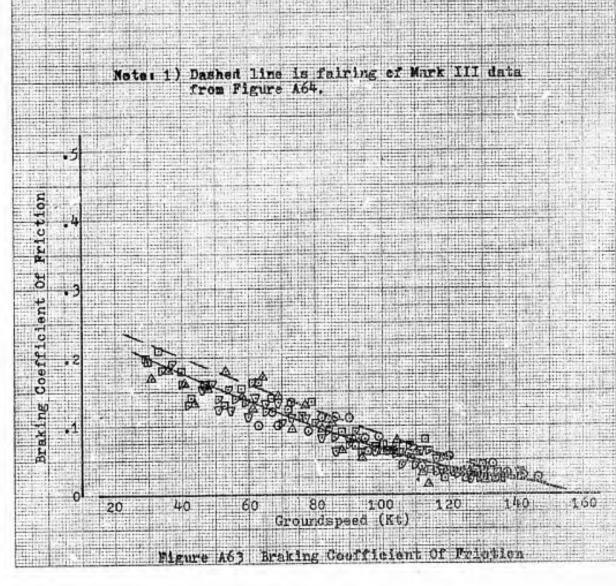


Figure A62 Stopping Performance

P-4E USAP S/N 66-368 J79-GE-17 Engines, Idle Thrust LE & TE Flaps Full Down Slotted Stabilator, Aft Stick Maximum Braking, No Drag Chute
Test Day Conditions
Mark II Antiskid, USAF Tires
Wet Concrete Runway

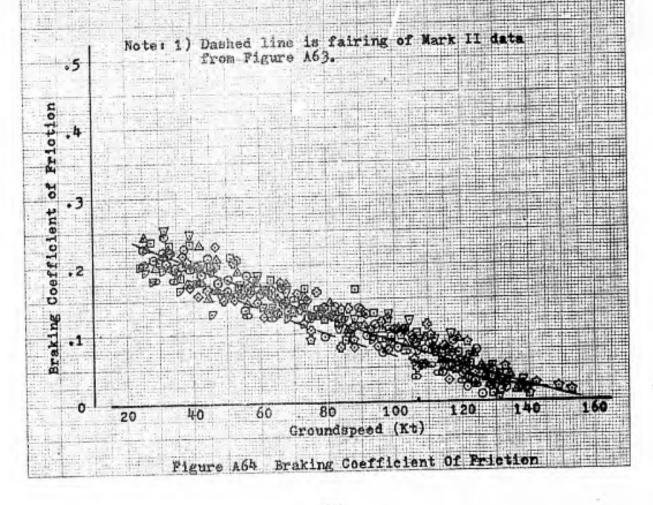
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	Gross	Wind	Amt Temp	Press Alt	Brake E	ner zv
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F-4E USAF S/N 66-368

J79-US-17 Engines, Idle Thrust
LE & TE Flaps Full Down
Slotted Stabilator, Aft Stick
Maximum Braking, No Drag Chute
Test Day Conditions
Mark III Antiskid, USAF Tires
Wet Concrete Runway

		Gross	Wind	Amb Temp	Press Alt	brake Energy 6,
Sym	Test	Wt(Lb)	(Kt)	(Deg C)	(Pt)	(Pt-Lb x 10 *)
0	21 A	39,800	0.0	6.6	2170	17.37
. 0	21 B	34,550	-1.7	9.8	21.57	14,42
Δ	22A	43,200	1.7	10.4	2042	20.41
Ø	22B	38,200	1.7	12.7	2037	16.35
Ø	30A	43,000	-7.4	17.5	2223	15.05
0	30B	38,200	-5.5	20.0	2226	17.45
0	30C	34,200	-4.6	22.2	2228	13,08
D	64A	43,250	0.0	11.6	2302	20,41
0	64B	38,150	0.0	16.7	2302	16,53
Ф	64C	34,350	0.0	19.4	2302	12,58



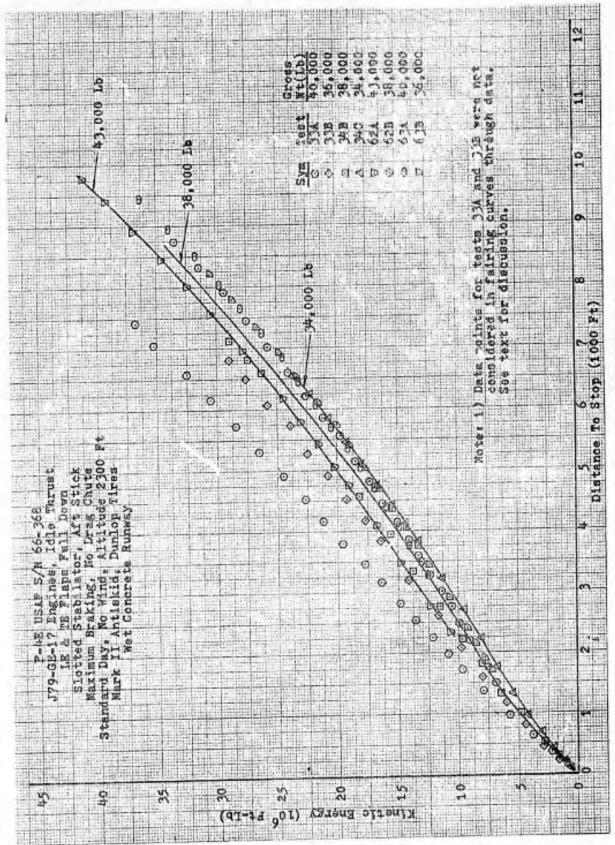


Figure A65 Stopping Performance

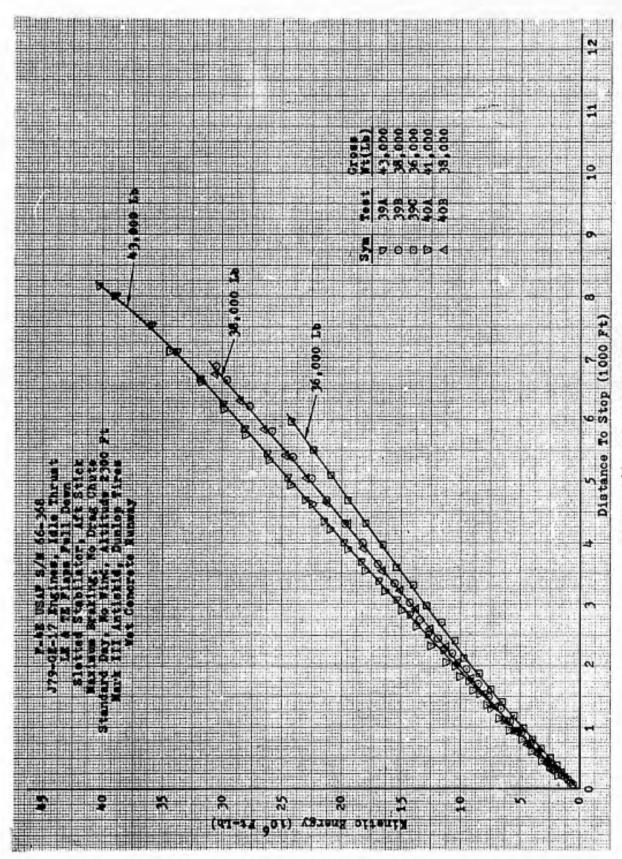
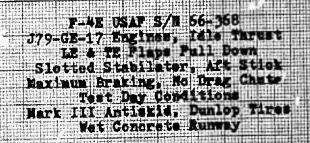


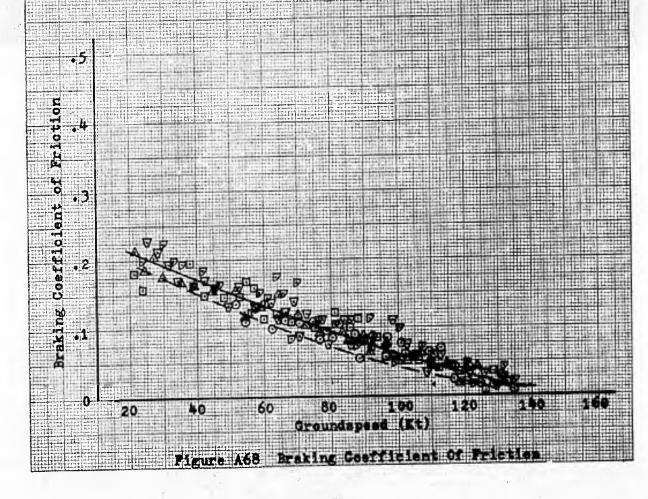
Figure A66 Stopping Performance

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	0	333	36.550		15.5	2233	13,64	
	Δ	148	38.700	0.3	24.6	2238	15.01	
	0	34C	34.700	0.5	24.7	2243	12.06	
	ש	62A	42,900	-4.4	16.1	2328	7.97 6.08	
	Ø	623	38,350			2332 2376	4,07	
	_0	63A	40,300		15.0 17.9	2376	5.94	
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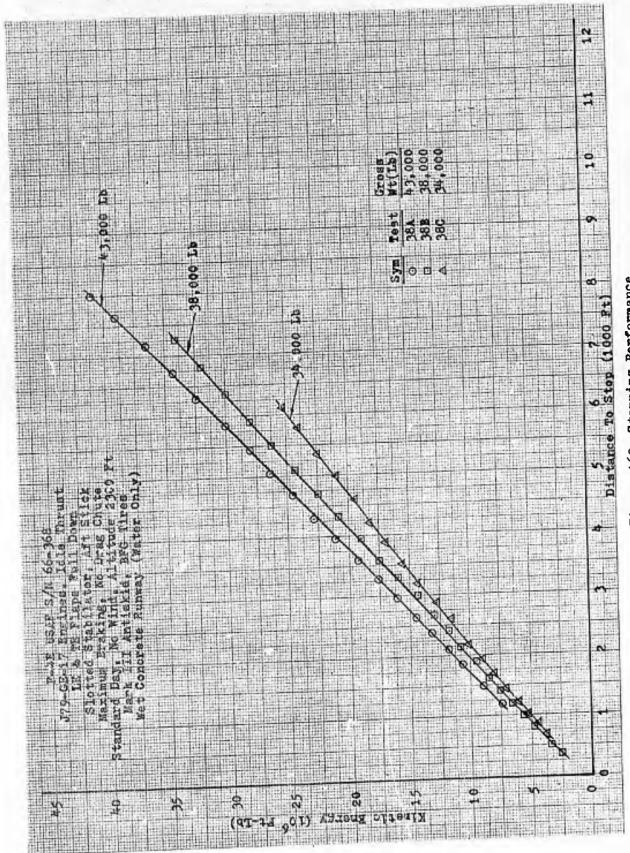


Figure A69 Stopping Performance

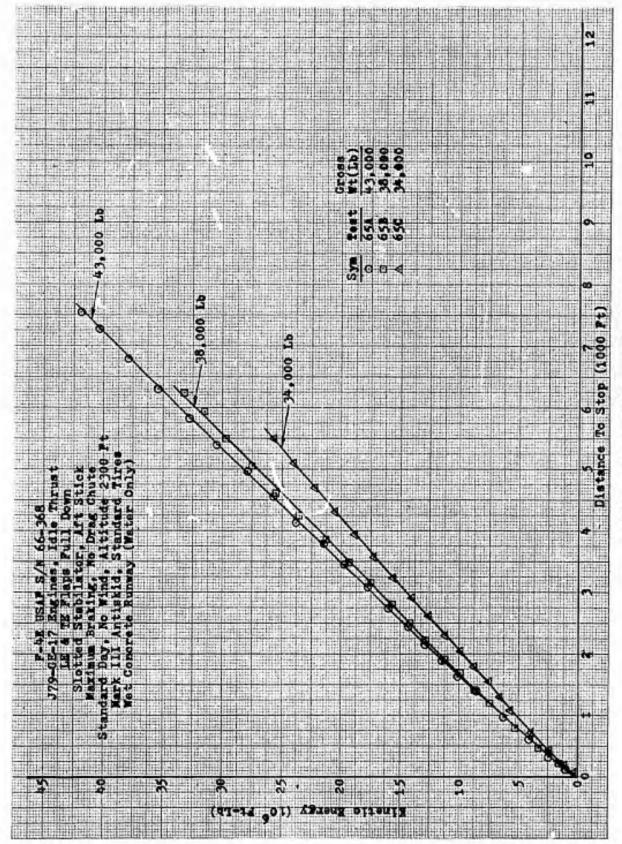
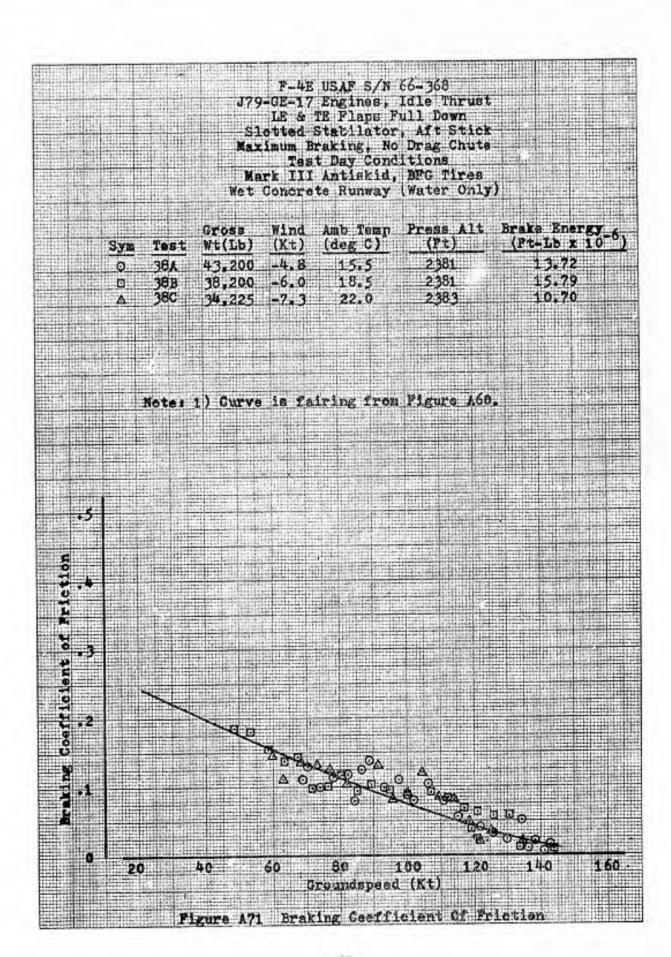
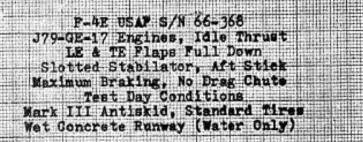


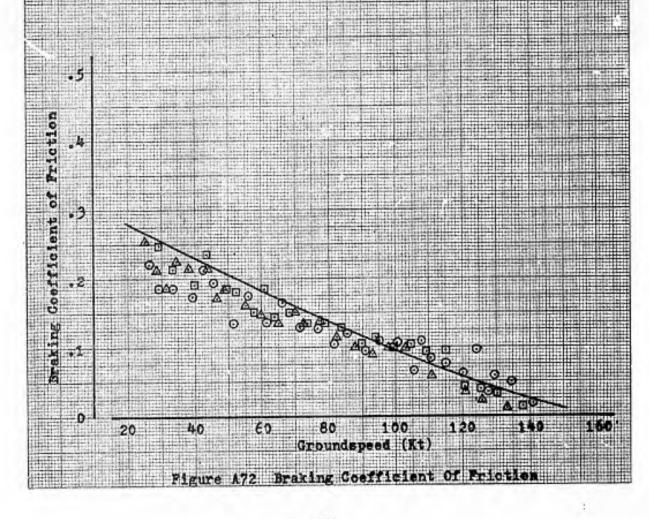
Figure A76 Stopping Performance

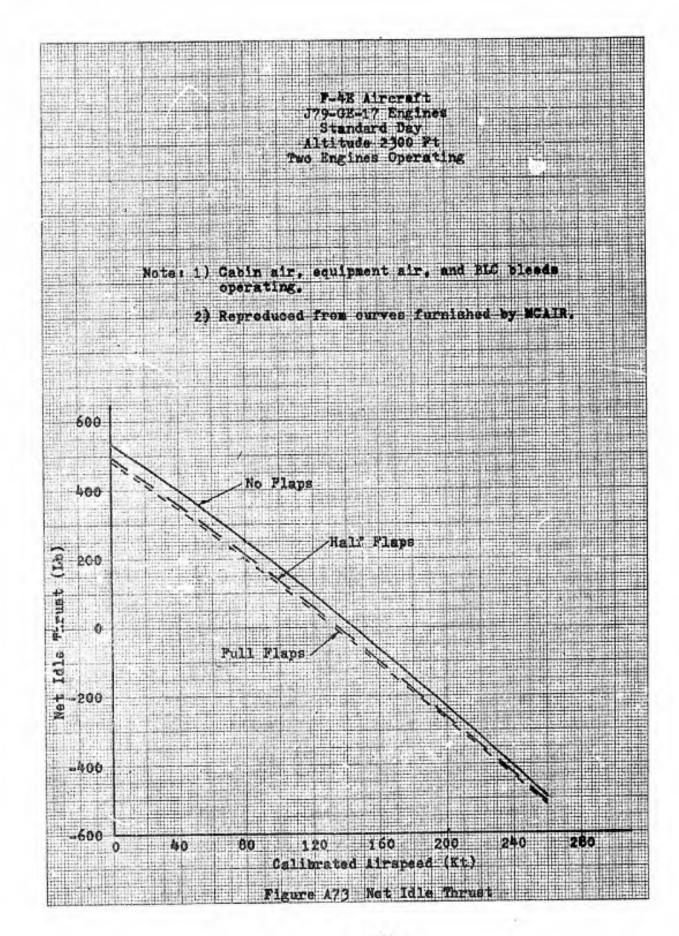


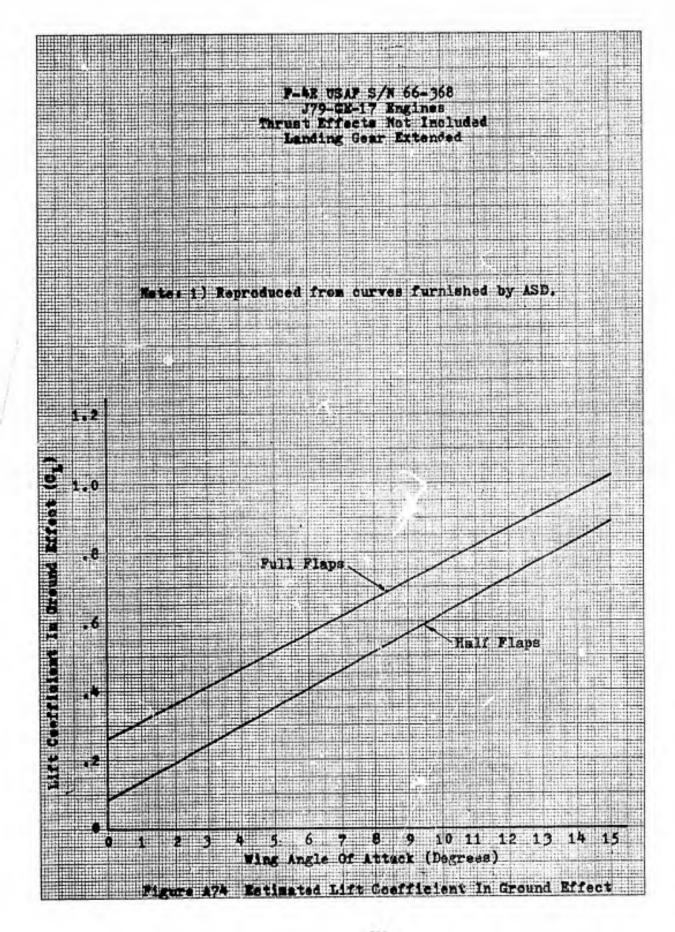


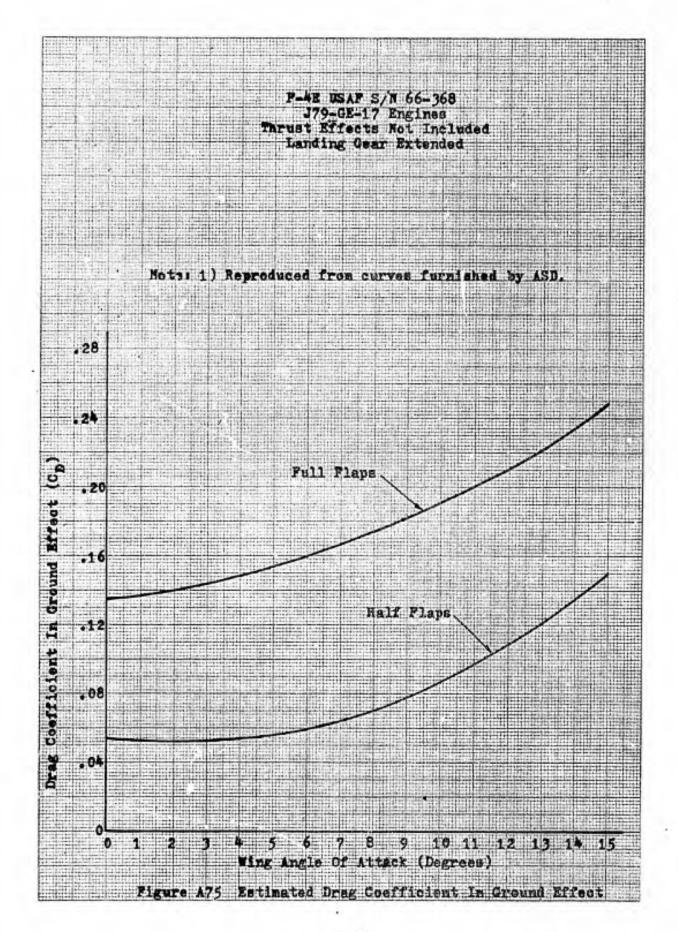
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Note: 1) Curve is Isiring from Figure A31.









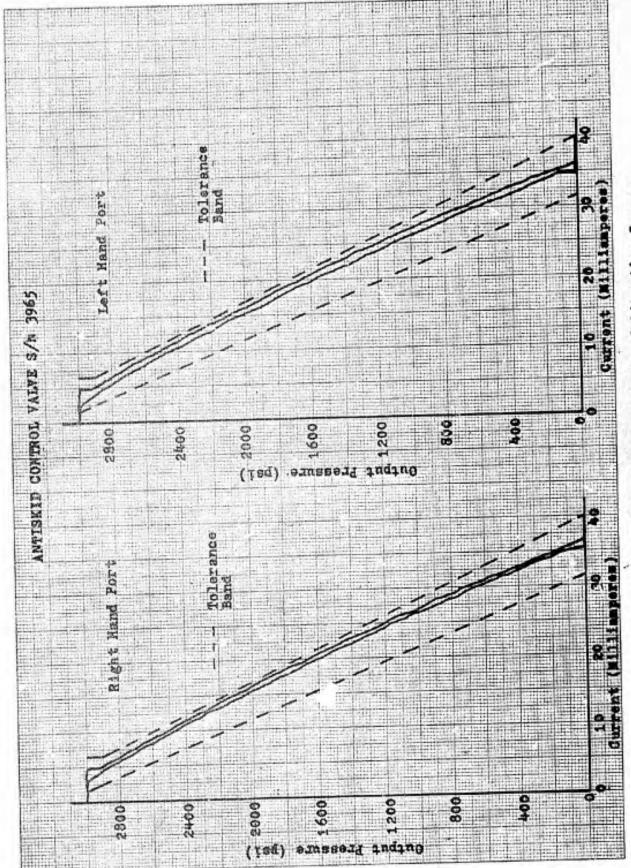
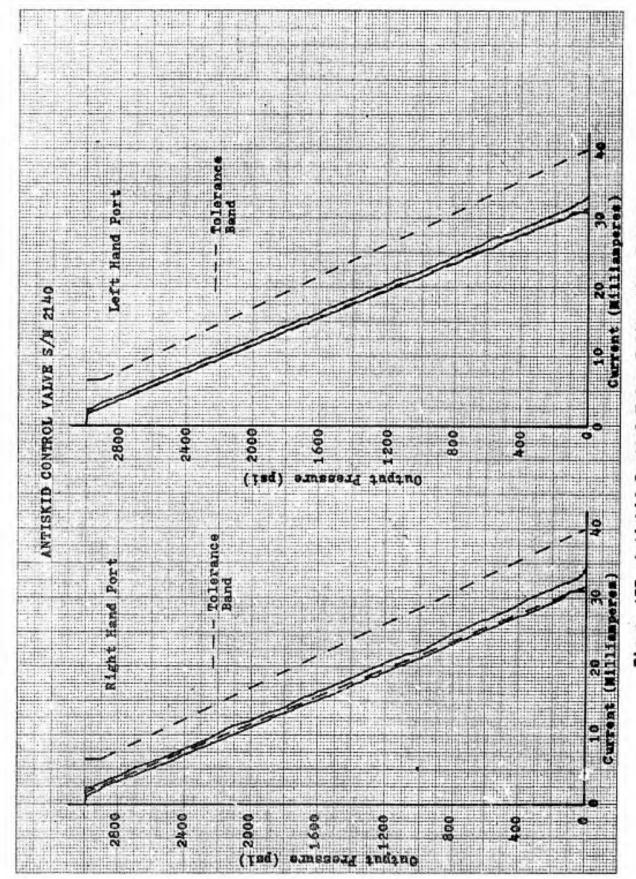


Figure A76 Antiskie Control Valve Calibration Curves



Pigure A77 Antiskie Control Valve Calibration Curves

APPENDIX B ANTISKID STRIPCHARTS

★ Figures B1 through B58 have been published separately due to their inconvenient size.

APPENDIX C TEST DATA SUMMARIES

EXPLANATION OF TEST DATA SUMMARIES

The first data point on each tabulation represents brake application. The last data point on each tabulation represents brake release.

TEST DAY

TOD - Time of day (seconds)

ACCEL - Acceleration from phototheodolite data (feet per second2)

GND-SPD - Groundspeed from phototheodolite data (knots)

DIST - Distance to stop extrapolated from phototheodolite data (feet)

KE - Kinetic energy calculated using test weight and test day groundspeed (106 ft-1b)

FBR - Total braking force (lb)

UBR - Braking coefficient of friction (dimensionless)

EBR - Summation of energy absorbed by the brakes (106 ft-1b)

STANDARD DAY - Standard day conditions, no wind, altitude 2,300 feet

KTAS - true airspeed (standard day, no-wind groundspeed) (knots)

DIST - Distance to stop (feet)

KE - Kinetic energy calculated using standard weight and standard day true airspeed (106 ft-lb)

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27200 25 -0	46 116.9	2067. 25.	33 9213.	.302	5.70	117.0	2081.	25.44
27704 25 -0	24 116.0	1874. 22.	83 9211.	.309	7.52	110.9	1884 .	22.88
27301427 -7	89 105.1	1691. 20.	86 9049.	.303	9.10	106.0	1698 •	20.87
27303.25 -96 27304.25 -86 27305.25 -96 27306.25 -9 27308.25 -9 27309.25 -9 27310.25 -9 27312.25 -10 27313.25 -9	24 108.3	1517. 18.	65 . 9807.	319	10.79	100.1	1519.	18.62
27304.25 -8	R9 95.3	1352. 16.	81 9589.	.309	12.33	94.9	1351.	16.74
27305.25 -9	78 89.6	1196. 14	87 10995.	.356	13.96	89.1	1192 •	14.78
27306-25 -9	66 83.9	1050. 13.	05 11076.	365	15.54	83.4	1043 •	12.92
27307.25 -9	92 77.9	913. 11.	24 11669.	.369	17.09	77.2	904 •	11.09
27308.25 -9	14 72.4	786. 9	71 10840.	.350	18.47	71.6	(/6 •	9.54
27309.25 -9	52 66 9	669. 8	30 11519.	-376	19.76	66.1	65/ •	0 = 1 1
27310-25 -9	76 61-1	561. 6	.92 12032.	.379	21.02	60.1	548 •	5.13
27311.25 +9	37 55.4	463. 5	.68 11687.	.371	22.16	54.3	449	0.40
27312.25 -10	10 49.6	373. 4	.56 12773.	•417.	23.23	40.4	359 •	7 77
27313.25 -9	. 43 43 . 8	295. 3.	56 12050.	.385	24.17	42.5	281 •	3.31
27314.25 -9	.47 38.2	225. 2	71 12221.	.391	24.98	36.8	212 •	4 96
27315.25 -9	79 32.16	166. 1	97 12737.	.413	25.70	31.1	173 .	1.00
27316.25 -10	.73 26.5	115. 1	.30 14063.	.451	26.35	24.9	103.	1-15
27317.25 -9	. 27 20 . 4	76.	.77 12238.	.398	26.82	18.6	C7 •	*69
27318.25 -6	. 42 15.6	46.	.45 8629.	.255	27.11	13.8	37 6	20
27311.25 -9 27312.25 -10 27313.25 -9 27314.25 -9 27315.25 -10 27317.25 -9 27318.25 -6 27318.58 -4	.78 14.4	38.	.38 6491.	.198	27.13	12.6	àu €	• 6 9
TEST NO. 18								OTDEC .
STAND WST 40000.LBS	TEST MG	T PRES	S ALT	TEMP	MINO	VEL VIC	238.0	DEG MAG
40000.L83	39850.LB	s 27.69	8 IN HG'	5.U C	2.00	N13		טבט וואט
		TEST	n AV			ST	ANDARD	DAY
700 40	CEL GND-SPD	DTOT K	F FRP	1100	E 120	K I A	11 1 31	. 70.7
TOD AC 28559.89 -4	CEL GNU-SPU	7070 X	.45 1263.	-044	.03	139.3	3080 .	34.38
2 A CC A TE . C	C 1. 4 77 H	2076- 33	. 15 3493.	-146	•56	136.7	2876 .	34.38 33.07 30.80
28560.75 -6 28561.75 -8 28562.75 -8	26 437 6	2648. 30	.91 5985	.232	1.76	131.9	2645 .	30.80
28561.75	1.7 127.4	2420. 28	.64 6655	クロク	₹.14	12F-8	2423 .	20.49
28563.75 -8	40 127 7	2218. 26	.40 7399	.254	4.53	. 121.7	. 2209 •	26.22
28564.75 -9	74 117 0	2016. 24	.14 8971	.321	6.30	116.3	2004 •	23.93
285644175 -7	.09 111.3	1823. 21	.65 8531	.294	7.98	110.5	1810 •	21.61
	.90 106.1		.85 8565		9.50	105.2	1624 .	19.59
			. 87 9352		11.07	99.7	1448 .	17.59
	0.32 100.7 0.29 95.2		.98 9571		12.51	- 94.1	1282 .	15.69
			.11 10709		14.19	88.3	1124 .	13.80
28569.75 -10	.55 83.5		.31 10382		15.71	82.3	977	11.99
		•	.69 18980		17-14	76.5	840.	
	3.85 77.8 3.64 72.11		.17 10920		18.50	70.7	714 .	
28572.75 -9 28573.75 -10			.77 11661		19.79	64.9	5 97.	
28574.75 -10	32 60.3		.42 12153	_	21.04	58.7	490 .	
	3.63 54.3		.20 11478		22.15	52.7	3 95 e	
	9.81 48.7		.19 11831		23.12	47.0	309	
			.20 13124			40.8	233	
28577.75 -10	3.39 36.2		.32 11585			34.3	168	2.09
	99 31.8		.78 6225			29.8	115	
	3.85 31.1		.71 48 65			29.2	1037	1.51

		0000		rev to	STA	DPACH	TIRES/	DRY RUNN	AY		
STAND WIT						T	ENP	MIND		MIND 01	EG HAG
43000.L85	-			200					STAN	DARD DA	Y
			TES	1 DAY		BR	INP	EBR	KTAS	DIST	KC.
TOD A	CCFI GI						.061	- 11 /		4-0-0	40.56
30073.69	5.15			38. RO		465.	.204	.74	143.3	7-52	39.08
30074.50	7.68		2030.	37.37	100		.393		137.2	3873.	35.83
30074.50	. 57	4 74 7	7766.	34.23	1	10124	.274	4.98	130.5	3646 .	32.42
30075.50 -1		127.7	3486.	TO . 04		8294.	.274	6.57	125.7	3427 .	30.08
	9.14	123.0	3273.	28.69	3	97034		8.39	120.2	3217 .	27.52
" O O O I ' I W W " "			3071.	26.22	2	9648.	.321		444.4	3019.	24.78
	9.72		2878.	23.58	1 1	0109.		10.33	108.8	2830 .	22.52
0001 2000			2694.		100	8905.	.283		103.5	2649 .	20.41
	The second		2520.	19.3		6777.	.213	15.56		2475 .	
30081.50 -		***	2752	48.41	9	6040.	.187	14.32	100.4	2307 .	
Z0082.58 -	6.21	97.9	2352.	16.6	3	60 82.	.182	15.37	96.0	2145 .	
30083.50	6.07				7	5861.	.181	16.22	93.0		15.26
30084.50	-5.82	90.6	2034.				.157	17.05	89.5		
70005.50	-5.22	87.2	1885.	14.4		6450.		17.88	86.3	1939 .	12.97
30.086.50	6.06	84.0	1740.	13.4		7299.	.226	18.84	82.5		12.91
200000000	-6.57	80.3	1602.	12.2				19.78	78.4	1557 .	11.71
	6.00	76.2	1469.	11.0		6711.		20.44	75.7	1425 .	10.92
		73.5	1343.	10.2	6		.161	21.23	72.3	1299 .	9.94
2000000	-4.10	70.1	1222.	9.3	3		.201	21.91	60.0	1179 .	9.08
30030-74		66.9	4487.	8.5	50	2 4 4 4 4	.166		CC E	1063 -	8.10
0007202	-4.81	60. 7	996.	7. 6	3	7925.		22.00	61.7	954 · 852 ·	7.25
		63.4	892.	6.7	76	/ 44 Ha	.225	23.47	59.4	852 .	6.49
30093.50	-6.12	59.7	995.	6.1	13	5833.	.172	24.09	40 CT 1	7 5 14 4	5.83
30094.50	-4.83	56.4	795.	6.	64	6548.	.196	24.66	51.8 47.8	662 .	5.11
**** FO	-5.31	53.4	102.	4.	72	8642.		25.33	51.0	000	4.34
30096.50	-6.82	49.9	614.		00	8174.	.252	26.00	47.8	578 .	3.68
	-6.30	45.9	500.		99	6356.	.199	26.55	44.0	499 .	
	- C 31	42.1	459.	3.		3388.	.094	26.62	42.8	467 .	3.40
30098-94	-2 67	P . 04	4690			14000					
300900074		MAR		HTTCH	TO/	STANDAR	O TIRE	SIDRY RI	YA KNL		
TEST NO. 2	2 B	MAR	K III A	MITON	Lur.	31 11 10 11					DIREC
16.01							TEMP	WT	ND VEL	MIND	DIKEU
STAND WET	T	TEST WO	T	PRESS	T.11	uc.	8.5 C	2	.3 KTS	76. 6	DEG MAG
38000-LBS		TEST WG 38200.L	35 2	7.661	IN	HG					
200004505				202		9.00			51	AND ARD	DAY
				EST D	AY-		1000	EBR	KTAS	DIST	KE
	ACCEL	CNIII	0 131	17.4		FBR	UBF	.06		2707 •	34.13
	_E 79	140.8	2633		12	1145	74		136.8	2417 .	31.41
32429.77 32431.00	- 0 46	134.3	2347	. 30.	.50	7728	.31		125.6	2192 .	20.50
32431.00	-10.10	127.2	2126		. 34	10347	.41			1980 .	25.30
32432.00	-11.90	120.4	1917	. 24	49	10495	42		115.6		22.48
32433.00	-11./5	147 2	1720		. 67	11031	43		108.5	1592	
32434.00	-11.68	113.2			. 04	10873	42	3 9.88		100000000000000000000000000000000000000	
32435.00	-11.41	100.1			.78	10791	41	7 11.72			
32436.00	-11.00	33.0			.68	10239	39	4 13.4	95.5		
32437.00	-10.33	93.6			. 75	11055	41	5 15.0	89.2		
32438.00	-10.79	9 00.0		. 12	07	10635			83.1		
32439.00	-10.2	5 00.0	905		. 03	11509			6 76.6		
32439600	-10.7	4 74.3	773		. 34					691	
32440.00	-10-1				.96	10 998				577	
32441.00	-10.5				. 51	11711			-		. 5.76
32442.00	-10.5	-		. 5	. 35	1104			The state of the s		. 4.63
32443.00	-9.8	4			. 27	1126	41				. 3.66
32444.00	-9.8				. 34	1199	843				
32445.00	-10.3	7 44.5			.44	1144	240				
32446.80	-9.7				. 88		530	7 24.8			
32447.00	-7.3				1.40		621	45 25.1			
32448.00	-6.1	1 28.		-	1.39			41 25.1	7 30.	0 103	
32448.02		3 28.	7 9	0.							

TEST NO. 3A	MĀRK	111 A	NTISKID/	STANDAR	DIRES	S/WET RUN	YAW		
STAND WGT 40000.LRS	TEST WGT	5	PRESS A	LT ·	TEMP	WINE 13.0	VEL .	WIND	DIREC DEG MAG

	EL GND-SPD							ANDARD I)AY
TOD ACC	30 144.0	DIST	KE 35.99	rnk - Andro-	AGO O	EBR	8133.8		KE -31471
40691.50 -4.			34.65	1647.	-066	.32	131.1	6723	30.42
40692.50 -1.0				.0.	0.000	37	129.4	6499	
40693.50 -3.	75 -138.8	7083.	33.44	590	-023	.40			
40694.50 -4.1	9 135.7		31.96		.046	.79	125.4		
40695.50 -2.5		6524.	31.19	0.	0.000	.83	123.7	5839.	27.10
40696.50 -3.8		6399.	30.31	0. 1133.	-044	.96	121.8	5625.	26.26
40697.50 -3.4		6178.	29.33	694.	.027	1.16	119.6	5414.	25.33
40698.50 -3.2	21 127.9	5960.	28.39	600.	.023		117.5		24.43
40699.50 -3.8		5745.		1430.			115.7		
40700.50 -3.4		5535		1126.	•041		113.2	4803.	22.69
40701.50 -3.4		5327	25.75	1260		2.04	111.3	4609.	
40702.50 -2.0	58 120.0	5124.	24.97	436.		2.19	109.4	4419.	
40703.50 -4.		4923.	24.11	2370.	.084	2.52	107.3 104.7	4229	20.37
40704.50 -3.4 40705.50 -3.6	115.4	4726. 4533.	23.10	1642.	.057	2.94 3.26	103.0	7042	19.42
40705.50 -3.6	63 113.6 33 110.9	4343.		2086.	.069	3.76	100.2	3681	17.78
40706.50 -3.8	66 109.6	4156.	20.84	1134.	037	3.96	98.9	3513.	17.30
40708.50 -4.2	23 107.4	3973.	20.00	3154	.102	4.42	96.6	3342.	16.52
40709.50 =3.3		3794	19.34	2171.		4.82	94.8	3179	15.90
40710.50 -3.9	7 102.9	3618.		3030.	.040	5.32	9921 5	3012-	15.02
40711.50 -3.8	32 100.9	3445.	17.68	293H	.094	- 5.81	90.1	2855.	14.37
40712.50 -3.6		3278.	16.89	2819.	.091	5.81 6.29	87.8	2700.	13.64
40713.50 -2.9	96.6	3113.	16.21	2117.	DAG	6 64	# BE 7	2550.	13.01
40714.50 -4.6	94.5	2951.	15.48			7.23	83.5	2402.	12.35
40715.50 -3.0		2795.		2375		7.74			11.59
40716.50 -4.0		2640.	14.13	3636.	.119	8.16		2122.	
40717.50 -5.3		2490.	13.16	5363.	.174		76.0	1980	10.23
40718.50 -3.6		2346	12.42	3317.	-108	9.49		1849.	9.56
40719.50 -3.9		2205	11.78 11.17	3795. 3381.	.121	9.99	69.1	1723. 1602.	8.98
40720.50 -3.5 40721.50 -3.5		2068.	10.57	3911.	128	10.47	~ / - ^	1485.	7.91
40721.50 -3.9 40722.50 -4.9	Z C F C F A	1805.	9.81	5299.	.171	11.60	63.9	1367.	7.24
40723.50 -3.5		1580.	9.19	3692	.120	12.12	61.5	1258	6.70
40724.50 -4.5	7.0 2.0 2.5	1 - 5 13	8.59	4940.	.158	12.65	59.0	1152.	6.17
40725.50 -4.3	67.6	1442.	7.93	4803.	- 156	-13.22-	56.2	1049.	5.60
40726.50 -4.4		1330.	7.36		.160	13.76	53.7	953.	5.11
40727:50 -4:2		1,223.	6.82	4808	.155	14.27	51.2	861.	4.65
40728.50 -4.5	59.8	1120.	6.21	5217.	.165	14.81		.: ·771 • ·	
40729.50 -3.8	57.4	1021.	5.73	4451.	.144	15.26	45.9	690.	3.73
40730.50 -5.1			5.22	6118.	-198	15.78	43.3		3.31
40731.50 -5.0		836.	4.62	6057	•195	16.32	40.0		2.83
40732.50 -4.9		751.	4.10	5947	192	16.83	36.9		2.42
40733.50 -4.2		571.	-3.67°	5155.	.167	17.25	34.3	399	2.08
40734.50 -4.2		596.	3.29	5231	167	17.64	31.8	341.	1.79
40735.50 -4.8		525.	2.87	5946	•190 •175	18.04	28.9	285.	1.48
40736.50 -4.3		458	2.49	5440	-172	18.42 18.73	26.0 23.7	F- 1 F	1.00
40737.50 -4.2 40738.50 -4.8		396	2.20 1.86	5272. 6056.		19.07	20.8		-77.
40739.50 -2.6		285	1.58	3446.		19.30	18.3		59
40739.66 -1.9		277.	1.56	2596	\$80.	19.30	18.0	" iii.	.57
	921	4-1		14 PA 10	191	1994		2 -12	

	100		HARK	*** AMT	TEVEN	STANDARD	TIRES/	DRY RUNA	IAY		
TEST NO	. 4A		MARK	III AN	138107	3141101110		urun	vei	HIND	DIREC
STAND	WET		TEST WGT	P	RESS A	LT	TEMP	3.6	VIC	253.0	DEG HAG
43000.1									713		
				W 11 22					STA	NDARD D	AY
100				TE	ST DAY-		HDD	EBR	PATAS	DIST	KE
TOD	A	CCEL	GNU-SPU	0.121				.01	143.2	3048 .	39.03
26309.	- 8	5.24	144.3	3099.	34.00	1906. 6203.	272	1.02	140.2	2003.	37.42
26310.	25 -	8.25	141.3	2913.	38.21	9874.	342	3.09	134.1	2628 .	34.21
26311.	25 -1	0.47	135.3	2679.	35.00	40040	.372	5.44	127.7	2404 .	31.02
26312.	25 -1	0.96	129.0		31.80	11355.	.384	7.76	121.2		27.96
26313.	25 -1	0.98	Martin Company of the	2244.	28.74	11355	383	10.15	114.1	1989 .	24.78
26 31 4.	25 -1	0.97	115.6	2043.	25.55	40486	.335	12.16	108.2	1799 .	22,30
26315.	25 -	9.78	109.8	1852.		10400	356	14.08	102.3	1619.	19.93
26316.	25 -1	0.03	104.0	1672.	20.68	12187.	740	14.08	95.9	1449 .	17.52
26317.	25 -1	0.61		1502.	18.29		708	18.01	89.6	1289 .	
26318.	25 -1	0.50	91.4	1342.	15.99	9464.		19.57	83.7	1141 .	13.34
26319.	25 -	8.16		1193.	14.03	94 64.		20.95	79.1	1002 .	11.92
26320.	25 -	9.32	81.1	1052.	12.59	11173.	740	22.36		872 .	10.26
26321.	25 -	8.52		920.			378	21.71	68-4	750 •	5.90
26322.	25 -	9.85		796.	9.51		337	A SHARE A LINE AND A		670	7.42
26323.	25 -	8.77	64.7	683.	8.00	11020.	145	26.16	57.1	535 .	6.20
26 324.	25 -	8.73	59.4	577.	6.75	11125.	774	27.24	57.1 52.2	442 .	5.20
26325.	25 -	9.38	54.6 48.4 43.6 38.5	481.	5./1	121 35.	71.4	28.26	45.9	358 .	4.02
26326.	25 -	8.57	48 - 4	396.	4.48	11213	766	29.11	41.1	282 .	3.21
26327.	25 -	9.05	43.6	316.	3.64	11904.	767	29.21	35.8	217 .	2.45
26328.	25 -	8.77	38.5	247.	2.83	11000.	221	30.46	31.0	160 .	1.83
26329.	25 -	5.42	33.7	187.	2.17	7290.	158	30-46	30.3	148 .	1.74
			38.5 33.7 32.9								
TEST	10. 45	11:10	HARK	III A	TISKID	/STANDAR	O TIRES	DRY RU	YA W		
			TEST MG1		PRESS	ALT	TEMP	WIN	VEL	WIND	DIREC
40000.	LBS	113.	TEST WGT 39200.LBS	2	7.714 I	N HG	6.0 C	3.	KTS		DEG HA
				T	CT DAY				ST	ANDARD	DAY
-			THE COL	DICT	V F	FRE	UDR	E CP	KTAS	DIST	KE.
									138.8	2689 .	34.12
28 55 0	31	0. 74	134.6	2420.	31.44	5918.	.245	1.32	134.2	24E3	31.88
28 55 1	25	0.31	120.0	2197.	28.89	9935.	.376		128.5	2230	29.22
28552	. 25 -	11.21	129.0	1985.		0705	770	5.23	121.6	2011 .	26.18
28553	25 -	10.71	122.3	1783.	23.23	11937.	.441	7.39	114.9	1801	23.36
28554	. 25 -	12.21	100.0	1595.		11278.	.420	9.54	107.0	1000	20.00
28555	. 25 -	11.37	108.8	1417.	18.05	11327.	.416	11.53	100.8	1421	18.01
28 556	. 25 -	11.13	102-0	1250.	15.78	11500.	.418	13.40	94.1	1248	
28557	.25 -	11.01	95.4	1094.	13.68		.439	15.66	87.4	1087	
28558	. 25 -	11.20	88.8	950.	11.75			16.87	80.7	939	
28559	. 25 -	10.34		-816.	10.03			18.46	74.3	801	
28560	. 25 -	11.40	THE RESIDENCE OF THE PERSON OF	693.		A CALL THE STATE OF THE STATE O		19.92	67.5	675	
28561	.25 -	10.01	69.4	581.				21.13	62.0	562	
28562	.25 -	10.01	63.9		120				55.2	457	
28563	. 25 -	10.24	57-3	387.			.396	23.37	49.6	365	
28564		-9.64		304.	-			24.33	43.4	282	
28565		10.10	45.8	232.					37.4	211	
28566		-9.B		169.				25.86	31.6	150	
28567	.25	-9.3		116.				26.49	25.7	98	
28568	.25 -	10.5	28.4	74.				26.91	19.8		
28569		-6.1		58.					18.7	45	67
28569	. 68	-3.3	2 57.0	200		3 3 3 3 5 5	100				

TEST NO.	5A	MARK	III	INTÍSKID	/STANDAR	D TIRES	SZWET RUN	WAY		
STAND . WG	т	TEST WGT		PRESS	ALT .	TEMP "	WIND	VEL	WIND	DIREC
43000 LBS		42500.LBS		7.715 I		11.5 C		KTS		DEG MAG
)	EST DAY		*****		51	ANDARD E)ΑΥ
TOD	ACCEL	GND-SPD		KE	FAR	UBR	EBR	KTAS	DIST	KE
35585.86	-4.38	145.1	7588.					143.0	7482.	38.93
35586.75	-3.09		7371.		0.	0.000	.05	141.4	7265.	38.07
35587,75	-3.93		7130.		400.	.016	.12	139.0	7023.	36.77
35588.75	-3.20		6894			0.000	.12	137.1	6786	35.78
35589.75	-3.94		6561	35.36	667.		.21		6552	34.66
35590.75	-3.11		6431.		0.	0.000	.23	132.9	6323.	33.65
35591.75	-3.70		6205.				•35	130.7	6095	32.50
35592.75			5982.			.009	.36	129.0	5874	31.70
35593.75	-3.81		5763.			.030	- 58	126.6	5653	30.50-
35594.75	-3.82		5547.			.043	· . 87	124.2		29.37
35595.75	-2.99		5336.			.009	.92	122.6	5227	28.63
35596.75			5127.		*4	.070	1.132	119.8	5017.	27.33
35597.75	-3.38		4923.			036	1.54	118.0	- 4813.	26.51
35598.75	-3.80		4722.			060	1.85	115.8	4613.	25.53
35599.75	-4.11		4525.			.080	2.32	113.1	4415.	24.36
35600.75	-3.03		4331.			.037	2.62	111.2	4223.	23.52
35601.75	-3.99		4141.			.079		109.1	· 4034 ·	22.67
35602.75	-3.09		3956.			. ()47	3.36	106.9	3848	21.75
35603.75	-4.11		3772.			.090	3.78	104.9	3666.	20.95
35604.75	-3.71		3594.			.079	4.25	102.7	3489.	20.07
35605.75	-3.82		3419.			.085	4.75	-100.2	3314.	-19.12
35606.75	-3.76		3247.			.087	5.23	98.1	.3144.	18.32
35607.75	-3.26		3079.	18.26	2300.	.069	5.64	96.1		17.57
35608.75	-4.19	96.1	2914.			.109	6,.16	93.6		16.68
35609.75	-4.65		2754.	16.45	4349.	.132	6.82			15.77
35610.75	-3.35		2599.	15.66	2754.	-085	7.32	8.88	2501.	14.99
35611.75	-4.72	88.9	2447.	14.88	4655.	.140	7.89	86.4		14.22-
35612.75	-4.30	86.1	2299.	13.96		.127	8.56	83.6		13.31
35613.75	-3.84	83.8	2156.			• 111	9.09	81.3	2063.	12.58
35614.75	-3.72	81.2	2017.			-111	9.64	78.7	1925.	11.78
35615.75	-3.44		1881.			-1,01	10.07-	76.7	- 1792.	
35616.75	-4.54		1748.			•146	10.63	74.5	1662.	10.58
35617.75	-3.94		1621.			.124	11.23	71.7	1537.	9.78
35618.75	-4.29		1497.			-142	11.75	69.5	1416.	9.19
35619.75	-4.82		1378.			•166	12.41	66.5	1298	8.42
35620.75	-4.24		1264.			.144	12.96	64.1	1187.	7.82
35621.75	-4.50		1154.			.156	13.58		1079	
35622.75	-3.74		1048.			•130	14.05	58.7	977.	6.56
35623.75	-5.32		946.			.192	14.62	-56.0		
35624.75	-3.83	55.7	850.			.137	15.16	53.0	784.	5.34
35625.75	-4.37	53.9	757.	5.47	5374	•161	15.58	51.2	696	4.98
35626.75	-4.73	50.8	569.		5928	•177	16.11	48.0	610.	4.38
35627.75	-5.03	48.1	585.	4.35	6389	•191	16.61 17.11	45.3	531. 456.	3.90
35628.75	-5.03	45.0	507.		6453.	•195		42.2	385.	2.87
35629.75	-5.44	41.7	433.	3.27	7072•	•212	17.62			
35630.75	-5.86	38.5	365.	2.78	7685	•233	18.11	35.6	320•	2.41
35631.75	-4.07	35.6	304		* 5378	•161	18,49	32.7	263.	1.63
35632.75	-5.88	32.2	245.		7831.	.233	18.90	29.3 27.2	208. 167.	1.41
35633.63	-1.78	30.2	. 200.	1.71	2441.	•073	19.08	5106	101.	1 0 14 1

TEST NO. 58 MARK	TIL ANTISKIDA	STANDARD TIRES	WET KUN	WAY		
-		LT TEMP	DAIW		WIND	DIREC
STAND WGT TEST WGT		-	1.4		228.0	DEG MAG
38000 LRS 38050 LBS	21.102.10	1300	_			
	TEST DAY-			STA)AY
TOD ACCEL GND-SPD	DIST KE	FBR UBR	EBR	KTAS	DIST	KE
	5554. 27.72	282012	.01	126.1	5467•	26.76
30027122	5455. 26.76	1166048	.20	123.9	5272	25.82
300000000000000000000000000000000000000	5244. 25.80	0. 0.000	- 31	121.6	5067	24.88
3002112	5036. 25.07	301012	. 34	119.9	4865	24.17
	4832. 24.22	1254050	.53	117.8	4666	23.35
30043443	4533. 23.36	34001	•66	115.7	4471 •	22.50
	4434. 22.61	1152044	.78	113.8	4278	21.78
	4241. 21.77	1620061	1.08	111.6	4090•	20.95
30000	4051. 20.94	977037	1.31	109.4	3905.	20.15
50521427	3864. 20.06	2132081	1.64	107.1	3723	19.29
30320023	3583. 19.30	994037	1.90	105.0	3546.	18.55
36323423	3503. 18.47	3040109	2.31	102.7	3372•	17.74
30331	3329. 17.60	2162075	2.76	100.2.	3202.	16.89
3030110	3158. 16.69	3155109	3.25	97.6	3036.	16.01
50052405	2992. 15.89	2834098	3.73	95.2	2874	15.23
30333143	2830. 15.18	2784095	4.16	93.0	2717•	14.55
3030 1003	2572. 14.34	3699128	4.70	90.3	2563	13.72
30333443	2518. 13.54	3325113	5.23	87.7	2414.	12.95
	2369. 12.76	3671126	5.77	85.1	2268	12.19
30351405	2224. 12.08	3403117	6.25	82.8	2128	11.53
30330123	2083. 11.27	4057140	6.82	79.9	1991	10.75
5055,425	1948. 10.70	3407115	7.27	77.8	1860.	10.19
20,21,000	1515. 9.91	4108138	7.82	74.9	1731 •	9.43
505.1745	1587. 9.33		8:30	72.6	1607•	8.86
505,202	1564. 8.79		- 8.71	70.4	1488.	8.34
30373023	1443. 8.21	4554153	9.19	68.0	1372.	7.78
303111111	1328. 7.62	4358 - 147	9.69	65.4	1261.	7.21
30373003	1217. 7.05		10.14	62.9	1154.	6.66
	1110. 6.52		10.60-	60.4	1050	6.14
20241952	1007. 5.98			57.8	951 •	5.63
30310123	908. 5.60		11.43	55.9	857.	5.26
	314. 4.99	6142208		52.7	765.	4.67
	724. 4.42	5425183		49.5	679•	4.13
2022115	540. 4.01	4565154		47.1	599•	3.74
30332443	560. 3.55			44.2	522•	
30333463	485. 3.14			41.5	451.	
30337823	415. 2.75	5119172		38.R	384 •	
38355.25 -4.42 40.4 38356.25 -5.97 37.3	349. 2.35	7008238		35.7	321.	
38357.25 -4.94 33.9	289. 1.93			32•3-		
38358.25 -5.77 31.3	233. 1.65			29.7	212.	
38359.25 -4.76 27.5	185. 1.28			26.0	166	
300011	140. 1.05			23.4	124	
38360.25 - 5.79 25.0 38361.25 - 2.84 21.3	10176	3569119		19.7	88	
38361.5987 21.3	9077		15.97	19.8	78.	•00

TEST NO. S	5C	MARK	[II AN	TISKIUZ	STANUARO	TIMES	WET RUN	чдү		
	_	TECT WCT	D	FESS AL	Ţ	TEMP	WIND	VEL.		DIREC
STAND MG		TEST WGT		.686 IN		7.0 C	1.6		55.0	DEG MAG
34000.LBS	3	455V•653	ε. 1	•110.52	107	., = =				
			TF	ST DAY-					ANDARD D)AY
TOD	ACCEL	GNU-SPD	DIST	KE	FAR	CHR	EBR	KTAS	DIST	KE '
40412.60	-3.87	119.6	4619.	21.87	632.	.028	•02	119.1	4699.	21.37
40413.50	-4.45	117.4	4539.	21.07	1384.	.061	.23	117.0	4525	20.59
40414.50	-2.91	115.1	4443.	20.27		0.000	•33	114.8	4336.	19.A2.
40415.50	-3.32	113.4	4250.	19.66	396.	•018	•36	113.1	4149.	19.24
40416.50	-3.41	111.5	4061.	19.01	591.	.054	.45	111.2		18.61
40417.50	-3.97	169.1	3374.	18.20	1343.	.057	•67	108.8	3786	17.92
40418.50	-3.40	106.9	3591.		81.7	• 036	. A7	106.7	3609.	17.13 16.58
40419.50	-3.48	165.1	.3513.	16.91	1040.	.044	1.00	104.9	3436	15.86
40420.50	-3.32	102.8	3337.	16.17	1014.	.041	1.21	102.7	3266	15.27
40421.50	-4.43	160.9	3165.	15.56	2293.		. 1.47	100.7	3099	14.44
40422.50	-4.19	98.0	2995.	14.70	2275.	.092	1.88	98.0	2938	
40423.50	-4.61	95.6	2834.	13.99	2875.	.111	5.58	95.6	2779.	13.75
40424.50	-3.92	93.1	2575.	13.25	2256.	.048	2.69	93.1	2626	
40425.50	-4.13	90.8	2520.	12.61.	2579.	.100	3.05	90.8	2476	12.42
40426.50	-4.17	88.2	2369.	11.89	2757.	.106	3.47	88.3		11.73
40427.50	-4.16	85.8	5555.	11.27	2859.	.109	3.88	86.0	2187.	11.12
40428.50	-4.91	83.0	2079.	10.53	3789.	.144	4.38	83.2	2049.	10.41
40429.50	-4.42	5.08	1942.	9.84	3365	.129	4.86	80.4	1915.	9.73
40430.50	-4.04	77.6	1309.	9.21	3063.	.116	5.29			9.13
40431.50	-4.85	75.2	1574.	8.54	4020.	1153	5.74	75.5		
40432.50		~ 72.4	1555.	8.03	3140.	.121	6.19	8.57	1540.	7.97
40433.50	-5.03	69.9	1435.	7.47	4411.	·165	6.63	70.3	1423	7.44
40434.50	-4.61	66.9	1319.	6.35	4060.	.152	7.13		1311.	- 6.83
40435.50	-4.58	64.3	.1208.	6.33	4108.	.156	7.56	64.8	1203.	
40436.50	-4.99		1102.	5.77	4642.	- 175	8.03	, 61.9	1099	5.77
40437.50	-4.93	5c.5		5.23	4722.	.178	8.50	59.0	1000.	
40438.50	-4.89	55.4	905.	4.69	4716:	.176	8.95	56.0	907.	4.72
40439.50	-3.82	52.8	513.	4.26	3642.	.135	9.30	53.5	817.	
40440.50	-5.53	50.4	725.	3.89	5537.	.206	9.70	51.1	730.	
40441.50	-4.77	47.4	543.	3.44	4789.	.154	10.10	48.2	650 •	
40442.50	-5.53	44.4	566.	3.02	5681.	.214	10.50	45.2	574.	3.08
40443.50	-6.02	40.8	493.	- 2.54	n296.	.235	10.95	41.6	503•	
40444.50	-3.79	30.0	428.	2.20	3972.	145	11.25	38.9	438.	
40445.50	-5.18	35.5	365.	1.92	5520.	.199	11.54	36.4	376.	
40446.50	-5.08	32.5	308.	1.61	5452.	.205	11.35	33.5	319.	
40447.50	-6.17		255.	1.28	6689•	.247	12.17	30.0	267.	
40448.28	-0.00	26.5	220.	1.08	,110.	.004	12.29	27.6	232•	1.15
-TU-T-TU-E-D										

TEST NO.	6 A	MARK	II AN	TISKID/	STAN DARD	TIRES/	DRY RUNH	AY	-	
STAND WS	_	TEST HGT	P	RESS A	ı T	TEHP	HIND	VEL	WIND	DIREC
43000.L95		43700 LBS			HG	8.5 C	3.0	KTS	270.0	DEG MAG
-				•				STA	NDAGA (7AV
							E BR	KTAS	DIST	KE
		GND-SPD	DIST	KE	EBR	UBR	FRA	149.2	3588 •	42.36
24846.41	-4.26	152.2	3791.	44.84	169. 1526.	.007	.00 .25	146.7	3384 •	40.98
24847.25	-5.11	149-8	3577.	43.41		-059	.85	143.7		39.30
24848.25	-6.28	146.7	3326.	41.64	3357.	.127	2.12	139.2	2912.	
24849.25	-8.00	142.2	3082.	39.12	5970.	.279	3.76	134.2	2687 .	
24850.25	-9.01		2846.	36.42	7739. 9580.	.321	5.78	128.5	2469.	
24851.25	-9.91	131.5	2619.	33.44 30.45	10757.	.350	7.99	122.6	2261 .	
24852.25		125.5	2402. 2196.	27.61	10679		10.15	116.6	2064 .	25.89
24853.25		119.5		24.76	11392		12.34	110.3	1876 .	23.17
24854.25		113.1	1999.	22.31	10387.		14.29	104.6	1699 .	20.84
24855.25	-9.50	107.4	1637.	19.97	11219.		16.18	98.9	1530 .	18.61
24856.25	-9.91	101.6	1470.	17.72	11447.		18.05	93.0	1371 .	.16.47
24857.25	- 9.86	95.7 89.9	1313.	15.64	12447.		19.88	87.3	1222 .	14.50
24858 . 25		83.7	1167.	1.3.56	11838.		21.63	81.1	1082 .	12.53
24859.25	-9.77	78.1	1030.	11.81	11131.		23.16		952 •	10.87
24860.25	-9.10 -8.63	73-1	983.	10.34	10701.		24.49	70.6	831 .	9.49
24 861. 25	-8.99	67.9	784.	8.91	11336.		25.79	65.4	719 •	0470
24862.25	-7.68	62.7	674.	7.61	9719		26.93	60.3	615 .	6.92
24 863 25	-9.14	E 0 /	571.	6.59	11830.		27.97	60.3 55.9	519	
24864.25 24865.25	-9.64	51.9	478.	5.22	12682.	.395	29.16	49.5	431 .	
	-8.81	47.1		4.30	11691.	.349	30.10	44.8	353 •	
24866.25 24867.25	-7.39	42.0	320.	3.41	9875	.297	39.89	39.7	283 .	
24868-25	-6.78	38-1	252.	3.41	9118.		31.49	35.8	221 •	
24869.25	-7.68		191.		10430.	.314	32.08	31.4	165 .	
24670.11	-3.54		146.	1.77	4910.	.135	32.34	28.1	124 •	1.50
TEST NO.		≅ H AR			STANDARI	D TIRES	DRY RUN	HAY	15	
CTAND ME	+ 3	TEST WGT		RESS A	LET	TEMP	WIND	. VEL	WIND	DIREC
40 00 0 . L 85		39200 L BS		.405 IN			3.2			DEG MAG
400000										
			TE	ST DAY-						0AY
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBK	EBK	KTAS	DIST	KE
27 095 . 25	-5.50	143.7	3368.	35.86	1692.	.079	.10	142.8	3404 •	
27096.25	-7.39		3129.	33.77	4375.	.186	.97	138.6	3158 •	
27097.25	-8.38	134.9	2896.	31.59	5934.	.240	2.19	133.9	2920 •	
		129.9	2673.	29.29	7323.	.274	3.67	128.8	2692 •	
27099.25			2459.	26.61	90 56.	.331	5.50	122.7	2471 •	
27100.25	-9.14	118.2	2254.	24.24	8103.	.291	7.19	117.0	2261 •	
27101.25			2059.	22.10	98 92•	.329	8.84	111.6	2062.	
27102.25	-9.74		1874.	19.85	9416.	.339	10.55	105.6	1871 •	
27103.25	-9.53		1698.	17.78	9438.	.341	12.19	99.8	1692 • 1522 •	
27104.25	-8.67		1532.	15.93	8653.	.301	13.65	94.3		
	9.47		1375.	14.21	9835.	.353	15.10	88.9	1361.	
27106.25	-8.74		1227.	12.52	9191.	.323	16.49	83.3 78.1	1069.	
	-9.39		1088.	11.05	10175	•363	17.81	72.4	937 •	
27.108.25			- 958.	9.54	9836.	-346	19.10	67.3	815	
27109.125	-8.15		837	8.30	9057.	•310 213	20.20 21.20	62.7	701	
27110.25	-8.20		724.	7.24	9269	.313	22.23	57.5	596	
27111.25			619.	6.12	10533.	.362 .347	23.19	52.0	499	
27112.25	-8.56		523.	5.05	9998. 9294.	.318	24.00	47.2	412	
		49.3	436	4.21	7606.	.251	24.64	42.8	335	
27114.25					8740.	.300	25.21	39.0	264	
27115.25	-7.28		285.	2.29	10724.	.369	25.85	34.1	200	
27116.25	-8.83		219.		11361.	•395	26.46		144	
27.117. 25			. 162.	1.66 1.16	6237.	.204	26.80	23.5	99	
27118.25	= 4.99		115.	1.16	6363.	.163		23.5	99	-
27118.25	-4.99	25.8	- 115.	1410	3 4 6 4 8	1100	20100			

TEST NO.					D/STANDAR					
STAND . WE	G T	TEST MGT 41350.LBS		PRESS	ALT	TEMP	WIND	VEL	WIND	QIREC
42000.LB3	S	41350.LBS	2	7.482	rn HG	2.0 C	4.5	KTS	205.0	DEG MAG
				COT DA	:	ej i ji				5.414
TOD	ACCEL	GND-SPD	DIST		FBR			VTIC		DAY
25568.58				41.09	3 1351.	0.54	Enk	KIAS,	0151	KE
25569.50	-7.28	149.8	1077	70 //	40 97.	477	•02 •72	14000	4163.	41.16 39.48 36.72
25570.50	-8.28		2000	76 76	5736.		2.05	1450 5	3 9 9 2 •	39.48
25571.50	-7.86	137.4		30 0 7 0	2130	.223	3.30	170.0	3699.	36.72
25572.50	-8.31	132.4	3997	72 44	6561.	•247	0 • 0 U	136.0	3471	34.41 31.91
	-8.85		3007.	32.1	7774	9647	4.7.2			
25574.50	-7.25			27.36	7771. 6034.	207	7 74	125.4	2995.	29.24
25575.5D		117.9	2594.	25 61	7109.	, • < U 4	7+74	120.0	2//9•	27.04 25.08
25576.50	-8.84				.8606.		9.08	11601	25/1.	25.08
25577.50	-9.61	107.2			9901.		10.50	111.3	23/1.	23.03
25578.50	-7.64	102.5	2016	19.22		•333	12.41	105.2	2117 .	20.57
	-8.66	97.6	2036.	17460	9159.	•256	13.84	100.4	199/ •	18.73
25580.50	-9.75	20.00	T 00	4/87	7177	•290 767	15.27	95.4	1824.	16.93
:25581.50	-7.20	96.1	1706.	17 70	10799.	257	10.09	89.8	1658	14.98
25582.50		86.7 82.9	1556.	13470	7751. 7425.	•253	18.27 19.27	84.2	1504	13.20
25583.50	-6.83 -8.70	76 6	1412.	16.5		.238	19.27	80.4	1359.	12.02
			1410	11.31		.320	20.49 21.57 22.88	7 to U	1221.	10.75
25584.50 25585.50	-7.85	10.1	1149.	9.94	9075	•297	21.57	70.9	1091.	9.36
	-0.03	68.2	1029.	8 • 53	10276.	.327	22.88	65.4	369 •	7.95
25586.50		63.2	91/.	7.32 6.50	9056.	.291	23.94 24.64 25.19	60.2	855 .	6.75
25587.50	-4.52			6.50	5293.	.157	24.64	5 E • 5	752 .	5.94
25588.50	-4.49	57.5	715.	6.05	5288.	•164	25.09	54.4	657 •	5.50
25589.50	-6.52	54.1	620.	5.36	7982	•250	25.76	51.0	565	4.83
25590.50	4.35	50.5	532.	4 • 67	5292	•165	26.33	47.3	480 .	4.16
25591.18	2.77	57.5 54.1 50.5 49.2	475.	4.44	3312.	.098	26.48	46.0	425 •	3.93
TEST NO.	78	MAR	(II A	NTISKIO	/ STANDARI	D.TIRES	DRY RUNK	AY		
STAND WE	т	TEST HGT		PRESS	ALT.	TEMP	WIND	VFI	WIND	BIREC
36000.LBS		TEST WGT 35700.LBS	2	7.490 I	N HG	6.8 C	5.4	KTS	206.0	DEG MAG
										*
500	4000		[EST DAY					AND ARD	
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBR	E 8R		DIST	KE
		141.1		31.49	269.	.014	•02	137.5	3458.	30.14
29133.50		138.5				.025	•09		3225.	
29134.50		135.2	3124. 2898.	28.90	2 2 45.	•114	•48		. 2998 .	
29135.50	-5.45	132.1	2898	27.59	1957.	•096	•91		2777.	
29136.50	-6.37	128.7 124.6	2679.	26.18	3230.	.147	1.48	124.9	2561.	24.88
29137.50	-6.70	124.6	2465.	24.54	3844.	•174	2.27 3.28	120.8	2351.	23.25 21.71
29138.50		120.6		22.97	6130.	•263	3.28	116.7	2147 .	21.71
29139.50			2059.	20.90		.311	4.70	111.1	1950 .	19.66
29140.50	-9.21		1869.	18.96		.313	6.13	105.6	1763.	17.76
29141.50	-9.19		1689.	17.09		.319	7.54	100.0	1585.	15.92
29142.50	-9.11		1518.	15.38	8148.	.329	8.90	94.5	1417.	14.25
29143.50	-9.23	93.3	1356.	13.75	8518.	.343	10.23	89.1	-1259.	12.66
29144.50	-9.81	87.8	1203.	12.18	9405.	.367	11.57	83.5	1110 .	11.12
29145.50	-18.39	81.3	1060.	10.45	10297.	.398	13.02	77.0	968 .	9.45
29146.50	-9.28	76.0	928.	9.13		.348	14.23	71.7	840 .	8.18
	-10.08	69.9	804.	7.72		.408	15.46	65.5	720 •	6.83
29148.50	-9.21	64.5	691.	6.57		.371	16.53	60.0	611 .	5.73
29149.50	-9.81	58.8	586.	5.45		.381	17.55	54.2	510 .	4.68
29150.50	-8.41	53.3	492.	4.49		.344	18.43	48.7	420 .	3.78
29151.50	-6.94	43.2	407.	3.83		.260	19.08	44.6	342.	3.17
29152.50	-7.73	44.7	328.	3.16		.311	19.70	40.6	269.	2.55
29153.50	-9.26	39.7	256.	2.49		.384	20.37	35.0	204 .	1.95
29154.50	-5.08	34.7	194.	1.90		.212	20.79	29.9	149.	1.42
29154.55	-4.79	34.6	191.	1.89		.200	20.79	29.7	146.	1.41
		•								_ ,

TEST MODE PRESS ALT TEMP NINO WEL NINO DIFEC	TEST NO. 88	MARK	II AN	TISKID/	STANDARD	TIRES	DRY RUNW	IAY		
Too		TEST MOT	p	pF55 Δ 1	T .	TEMP	WIND	VEL		DIPEC
TOD ACCEL (NNO-SPO DIST KE FBR USA EXAMPLE AND ACCEL (NNO-SPO DIST K	STANU WELL	7550 1 BS	27	.565 IN	HG 1	0.0 C	12.2	KTS	237.0	DEG MAG
TOD								0.54	N 5 4 5 5	14V
TOO ACCEL SWOSPO USIS 36.49 48.20 320. 36.40 320. 36.49 48.20 320. 36.49 4										
30526.50 -7.12 143.9 3291. 34.41 40.99. 1.75 1.31 133.0 2673. 29.76 30526.50 -7.12 143.9 3051. 34.41 40.99. 1.75 1.31 133.0 2673. 29.76 30520.50 -6.95 1391.7 2812. 32.44 40.99. 1.72 2.26 128.8 2472. 21.91 30520.50 -7.99 135.5 2579. 30.52 79.70 2.73 1.24.6 2237. 26.11 30530.50 -9.95 139.1 2355. 28.11 7927. 23.76 19.10.10 11	TOD ACCEL									
30528.50 -7.12 143.9 3031. 32.44 1099, 1172 2.26 128.8 2452. 27.91 30530.50 -6.95 139.07 2612. 32.44 1099, 1172 2.26 128.8 2452. 27.91 30530.50 -7.99 135.5 2579. 30.52 5593. 23.4 3.37 124.6 2237. 26.11 30530.50 -9.56 130.1 2355. 28.11 7927. 237 4.98 115.1 2027. 23.65 30532.50 -9.91 124.3 2140. 25.68 86.66. 32.7 6.76 113.3 1827. 21.59 30532.50 -9.91 124.3 2140. 25.68 86.66. 32.7 6.76 113.3 1827. 21.59 30533.50 10.73 118.3 1935. 21.66 9973. 3659 8.67 10.7.2 1635. 19.35 30334.50 -10.62 105.5 1556. 18.49 104.61. 338 12.52 94.3 1264. 11.97 30536.50 -10.62 99.3 1365. 16.49 104.61. 338 12.52 94.3 1264. 14.97 30536.50 -10.62 99.3 31.55 16.38 103.55 16.39 103.51 10.62 10.65 10.6								_	2673	
30599,50 -6.95 139,7 2612. 30.52 3. 24.4 3.37 124.6 2237. 26.11 30530.50.7.99 135,5 2579. 30.52 3. 24.4 3.37 124.6 2237. 25.64 30531.50 -9.56 130.1 2355. 28.11 7927. 27.4 98 119.1 2027. 23.68 30531.50 -9.91 124.3 2140. 25.68 866. 327 6.76 113.3 1827. 21.59 30533.50 -10.73 118.3 1935. 23.26 9973. 359 8.67 107.2 1636. 19.55 30533.50 -10.73 118.3 1935. 23.26 9973. 359 8.67 107.2 1636. 19.55 30533.50 -10.73 118.3 1935. 23.26 9973. 359 8.67 107.2 1636. 19.55 30533.50 -10.62 105.5 1556. 18.49 104.61 .388 125.2 94.3 1228. 14.97 30535.50 10.29 99.3 1365. 16.38 11351. 351 14.30 81.122. 11.25 30537.50 -10.29 99.3 1365. 16.38 11351. 351 14.30 81.122. 11.25 30537.50 -10.62 105.5 1556. 16.38 11351. 351 14.30 81.122. 11.25 30537.50 -9.33 68.9 107.1 12.56 97.99 346 17.57 6 839 9.63 30538.50 -9.33 68.9 107.1 12.56 97.99 346 17.57 70.5 71.8 8.37 30539.50 -9.35 81.9 328.1 114.9 9928. 355 18.20 70.5 71.8 8.37 30539.50 -9.35 81.9 328.9 928. 11.14 9928. 355 18.23 64.5 597. 6.99 30541.50 -10.02 63.7 561. 6.74 11257. 409 22.49 52.2 359. 459 30541.50 -10.02 63.7 561. 6.74 11257. 409 22.49 52.2 359. 459 30543.50 -10.14 57.5 453. 54.9 11554. 407 24.09 46.0 307 3.55 30545.50 -10.06 44.8 284. 333 12421. 4553 26.18 33.2 166. 13.0 16.6 14.8 284. 333 12421. 4553 26.18 33.2 166. 307 3.55 30545.50 -10.06 44.8 284. 333 12421. 4553 26.18 33.2 166. 307 3.55 30545.50 -10.06 44.8 284. 333 12421. 4553 26.18 33.2 166. 307 3.55 30545.50 -10.06 44.8 284. 333 12421. 4553 26.18 33.2 166. 307 3.55 30546.50 -9.78 36.6 24.5 50.1 10.0 3356. 124 28.40 12.7 12.2 30547.50 -10.11 33.2 153. 183 11970. 425 27.67 21.5 770 -78 30547.50 -10.11 33.2 153. 183 11970. 425 27.67 21.5 770 -78 30547.50 -10.11 33.2 153. 183 11970. 425 27.67 21.5 770 -78 30547.50 -10.11 33.2 153. 183 11970. 425 27.67 21.5 770 -78 30590.50 -26 26 134.6 2743. 32.25 38.00 .288 6.47 119.3 2200. 25.2 2591.50 -9.92 119.50 -10.20 113.2 1901. 22.81 3819. 166 .99 119.3 2205. 30.30 25910.50 -8.68 130.6 2511. 30.34 6598. 20.4 24.4 11.7 9. 22.3 32.5 30.00 2591.50 -9.93 101.7 12.50 8.2 30.0 30.3 3.12 10.0										
30531.50 -9.56 130.1 2355. 28.11 7927297 4.98 115.1 2027. 22.86 30531.50 -9.56 130.1 2355. 28.11 7927297 4.98 115.1 2027. 22.86 30531.50 -9.56 130.1 2355. 21.66 9973359 4.67 107.2 1636. 19.35 30531.50 -10.73 118.3 1935. 21.66 9973359 4.67 107.2 1636. 19.35 30531.50 -10.62 105.5 1556. 18.49 104.61 .388 12.52 94.3 1284. 17.91 30534.50 -10.62 105.5 1556. 18.49 104.61 .388 12.52 94.3 1224. 14.97 30536.50 -10.62 99.3 1385. 16.38 10351381 1.30 88.1 1125. 13.05 30537.50 -10.63 93.1 1223. 14.42 10.14399 16.01 81.1 125. 13.05 30537.50 -9.35 81.9 926. 11.14 9928358 16.90 77.5 6 839 .9.63 30536.50 -9.35 81.9 926. 11.14 9928358 16.90 77.5 6 839 .9.63 30536.50 -10.29 69.7 673. 8.77 114.99. 325 10.65 10.29 69.7 673. 8.07 114.99. 325 10.50 10.99 69.7 673. 8.07 114.99. 325 10.50 10.99 69.7 673. 8.07 114.99. 325 10.50 10.14 57.5 458 5.94 115.54 92.2 94 52.2 359 4.57 30546.50 -10.10 6 51.5 366. 4.41 126.35467 25.16 40.0 23.2 2.94 57.3 10543.50 -10.14 57.5 458 5.94 115.54 312.57 .408 22.94 52.2 359 4.57 30546.50 -10.96 51.5 366. 4.41 126.35467 25.16 40.0 232. 23.5 30544.50 -10.66 44.8 284. 3.33 124.21453 26.18 33.2 166. 1.85 10545.50 -10.61 33.2 153. 1.85 11970425 27.67 21.5 7070 30545.50 -10.61 33.2 153. 1.85 11970425 27.60 11.1 3.2 27.80 1 N HG 4.22 27.4 11.7 923 30546.50 -9.78 38.6 214. 2.47 115.05412 26.99 26.9 112. 122 30545.50 -5.98 12.1 22 30545.50 -5.98 12.1 22 30545.50 -5.98 12.1 22 30595.18 -9.94 12.1 22 30.5 35.0 -6.62 13.46 2743. 3452. 37.63 393022 .02 14.2 2.45 10.1 3.2 25.6 30.38 25.910.50 -5.88 12.1 2.1 2.1 2.2 30.5 3.5 3.3 .92 13.98047 28.44 11.7 923 30595.18 -9.94 11.1 2.99 2.2 3.5 3392 13.98047 28.44 11.7 923 30595.18 -9.94 11.1 2.99 2.2 3.99 3.3 4.6 5.99 3.3 4.75 2.5 3.6 3.0 3.8 25.910.50 -5.88 13.2 2.1 2.1 2.2 3.3 3.4 2.2 3.3 3.3 3.2 3.2 3.2 3.3 3.3 3.3 3.3										
30531.50 -9.91 124.3 2140. 25.68 8686. 327 5.76 113.3 1827. 21.59 30533.50 -10.73 118.3 1935. 21.26 9973. 3.59 8.67 107.2 1636. 19.35 30533.50 -10.73 118.3 1935. 21.26 9973. 3.59 8.67 10.76 10.65 10.9.5 10.00 111.7 1741. 20.72 10.280. 3.75 10.66 100.6 1454. 17.01 30535.50 -10.62 105.5 1558. 18.49 10461. 3.88 12.52 94.3 1224. 14.97 30535.50 -10.29 99.3 1385. 16.38 10351. 3.81 14.30 88.1 1125. 13.05 30537.50 -10.29 99.3 1385. 16.38 10351. 3.81 14.30 88.1 1125. 13.05 30537.50 -10.29 99.3 1385. 16.38 10351. 3.81 14.30 88.1 1125. 13.05 30537.50 -9.33 86.9 1071. 12.56 9799. 346 17.57 75.6 839. 9.63 30538.50 -9.33 86.9 1071. 12.56 9799. 346 17.57 75.6 839. 9.63 30538.50 -10.23 75.8 796. 9.55 11152. 400 20.32 64.5 597. 8.99 30540.50 -10.22 65.7 561. 6.74 11.257. 400 20.32 64.5 597. 8.99 30541.50 -10.22 65.7 561. 6.74 11257. 400 20.32 64.5 597. 8.99 30541.50 -10.02 65.7 561. 6.74 11257. 4.08 22.94 52.2 394. 4.59 30543.50 -10.02 65.7 561. 6.74 11257. 4.08 22.94 52.2 394. 4.59 30543.50 -10.02 65.7 561. 6.74 11257. 4.08 22.94 52.2 394. 4.59 30543.50 -10.96 64.8 294. 3.33 12421. 4.53 26.18 33.2 166. 334. 4.59 30545.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 334. 4.59 30545.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 30547.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 30547.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 30547.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 30547.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 166. 30547.50 -10.66 44.8 294. 3.33 12421. 4.53 26.18 33.2 26.9 26.9 26.9 112. 1.22 30547.50 -10.13 33.2 35. 36.0 36.4 36.9 37.7 36.9 36.9 36.9 36.9 37.7 36.9 36.9 36.9 36.9 36.9 36.9 36.9 36.9								119.1	2027 •	23.86
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TEST NO. 9A MARK II ANTISKID/STANDARD TIRES/DRY RUNWAY STAND WGT TEST WGT PRESS ALT TEMP WIND VEL 265.0 DEG MAG MACCEL GND-SPD DIST KE FBR UBR EBR KTAS DIST KE 25906.56 -4.95 145.4 3452. 37.63 393. 022 .02 146.0 3469. 37.76 25908.50 -6.95 138.8 2973. 34.26 3819. 164. 99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25911.50 -10.14 124.7 2303. 27.66 9039. 333 4.75 1250. 2307. 27.68 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25912.50 -9.31 107.2 1716. 20.45 9039. 312 10.02 107.3 1714. 20.37 25913.50 -9.83 101.7 1539. 18.42 9961. 345 11.66 101.8 1535. 18.34 25917.50 -9.83 101.7 1539. 18.42 9961. 345 11.66 101.8 1535. 18.34 25917.50 -9.91 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.55 25917.50 -9.91 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.55 25917.50 -9.97 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.55 25917.50 -9.97 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.55 25917.50 -9.97 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.56 25919.00 -11.55 81.4 1001. 11.78 13003. 455 17.25 81.1 992. 11.65 25919.00 -10.20 74.2 870. 9.79 11596. 406 18.89 73.8 860. 9.65 25921.00 -9.06 68.8 749.8 84.2 1068. 71.6 10773. 338 22.39 52.3 431. 4.84 25925.00 -9.24 63.4 638. 71.6 10773. 338 32.9 52.3 431. 4.84 25925.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 71.6 10773. 368 21.29 62.9 627. 7.02 25922.00 -8.88 52.9 442. 4.98 10013. 338 23.29 52.3 431. 4.84 25925.00 -8.88 52.9 442. 4.98 10013. 338 23.29 52.3 431. 4.84 25925.00 -8.82 47.9 356. 4.08 10068. 363 24.14 47.2 346. 3.94 25925.00						.124	28.40	12.7	18 .	
TEST NO. 9A MARK II ANTISKID/STANDARD TIRES/DRY RUNWAY STAND WGT 40200.LBS TEST WGT 40200.LBS TEMP 4.2 C TEMP 1.8 KTS TEMP 1.8 KTS TEMP 265.0 DEG M*G TEST WAS TEMP 1.8 KTS TEMP 1.8 EBR KTAS DIST KE 1.8 KTS 1.8 KTS TEMP 1.8 LE 1.8						.047	28-44	11.7	9.	.23
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TOD ACCEL GND-SPD DIST KE FBR UBR EBR KTAS DIST KE S900.56 -4.95 145.4 3452. 37.63 393. 0.22 .02 146.0 3469. 37.76 25907.50 -5.38 142.1 3211. 35.94 1577. 0.71 .33 142.7 3225. 36.06 25908.50 -6.95 138.8 2973. 34.26 3819. 164 .99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25910.50 -8.68 130.6 2518. 30.34 6598264 2.94 131.0 2526. 30.38 25911.50 -10.14 124.7 2303. 27.66 9039333 4.75 125.0 2307. 27.68 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25912.50 -9.31 107.2 1716. 20.45 9039312 10.02 107.3 1714. 20.39 25915.50 -9.83 101.7 1539. 18.42 9961345 11.66 101.8 1535. 18.34 25916.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25916.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25918.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25919.00 -11.55 81.4 1001. 11.78 13003452 17.25 81.1 992. 11.65 25922.00 -9.24 63.4 638. 7.16 10773368 21.29 62.9 627. 7.02 25923.00 -8.98 57.7 535. 5.92 10628358 22.38 57.1 524. 5.77 25923.00 -8.98 57.7 535. 5.92 10628358 22.38 57.1 524. 5.77 25923.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 25.8 35.1 205. 218 25921.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1								WAY		
TOD ACCEL GND-SPD DIST KE FBR UBR EBR KTAS DIST KE 5906.56 -4.95 145.4 3452. 37.63 393. 022 .02 146.0 3469. 37.76 25907.50 -5.38 142.1 3211. 35.94 1577. 071 .33 142.7 3225. 36.06 25908.50 -6.95 138.8 2973. 34.26 3819164 .99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25910.50 -8.68 130.6 2518. 30.34 6598. 264 2.94 131.0 2526. 30.38 25911.50 -10.14 124.7 2303. 27.66 9039333 4.75 125.0 2307. 27.68 25912.50 -9.24 119.1 2098. 25.23 8300288 64.7 119.3 2100. 25.22 25912.50 -9.24 119.1 2098. 25.23 8300288 64.7 119.3 2100. 25.22 25912.50 -9.31 107.2 1716. 20.45 9039. 312 10.02 107.3 1714. 20.39 25915.50 -9.83 101.7 1539. 18.42 9961345 11.66 101.8 1535. 18.34 25915.50 -9.81 107.2 1716. 20.45 9039. 312 10.02 107.3 1714. 20.39 25915.50 -9.81 107.2 1716. 20.45 9039. 348 13.33 95.7 1367. 16.23 25916.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25916.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25919.00 -11.55 81.4 1001. 11.78 13003452 17.25 81.1 992. 11.65 25920.00 -9.00 68.8 749. 8.42 10292352 20.12 68.4 739. 8.28 25922.00 -9.24 63.4 638. 7.16 10773368 21.29 62.9 627. 7.02 25922.00 -9.24 63.4 638. 7.16 10773368 21.29 62.9 627. 7.02 25923.00 -8.82 47.9 356. 4.08 10689353 22.38 57.1 524. 5.77 25923.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 22.38 55.1 205. 218 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149.	TEST NO. 9A	MARI	K II AN	IT1SKID/	STANDARD	TIRES	/DRY RUN		WIND	DIREC
TOD ACCEL GND-SPD DIST KE FBR UBR EBR KTAS DIST KE 25906.56	TEST NO. 9A	MARH TEST WGT	K II AN	TISKID/	STANDARD LT	TIRES	/DRY RUN	VEL	WIND 265.0	DIREC DEG MAG
TOD ACCEL GND-SPD DIST KE 393 .022 .02 146.0 3469. 37.76 393. 022 .02 146.0 3469. 37.76 36.06 25907.50 -5.38 142.1 3211. 35.94 1577. 071 .33 142.7 3225. 36.06 25908.50 -6.95 138.8 2973. 34.26 3819. 164 .99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25910.50 -8.68 130.6 2518. 30.34 6598264 2.94 131.0 2526. 30.38 25910.50 -8.68 130.6 2518. 30.34 6598264 2.94 131.0 2526. 30.38 25912.50 -9.24 119.1 2098. 25.23 8300288 6.47 119.3 2100. 25.22 25912.50 -9.24 119.1 2098. 25.23 8300288 6.47 119.3 2100. 25.22 25912.50 -9.31 107.2 1716. 20.45 90.39312 10.02 107.3 1714. 20.35 25914.50 -9.31 107.2 1716. 20.45 90.39312 10.02 107.3 1714. 20.35 25915.50 -9.83 101.7 1539. 18.42 9961345 11.66 101.8 1535. 18.34 25915.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25916.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25917.50 -9.91 90.1 1215. 14.46 10595370 14.91 90.0 1209. 14.34 25917.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25919.00 -11.55 81.4 1001. 11.78 13003455 17.25 81.1 992. 11.65 25920.00 -10.20 74.2 870. 9.79 11596406 18.89 73.8 860. 9.65 25920.00 -9.24 63.4 638. 749. 8.42 10292352 20.12 68.4 739. 8.28 25922.00 -9.24 63.4 638. 749. 8.42 10292352 20.12 68.4 739. 8.28 25922.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25922.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25922.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25922.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25927.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25928.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 137.14. 14.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 137.14. 14.86 6767208 26.25 29.6	TEST NO. 9A	MARH TEST WGT	K II AN	TISKID/	STANDARD LT	TIRES	/DRY RUN	VEL KTS	265.0	DEG MAG
25906.56 -4.95 145.4 3452. 37.63 393. 022 02 142.7 3225. 36.06 25907.50 -5.38 142.1 3211. 35.94 1577. 071 .33 142.7 3225. 36.06 25908.50 -6.95 138.8 2973. 34.26 3819. 164 .99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 3230. 136 1.84 135.1 2753. 32.32 25910.50 -8.68 130.6 2518. 30.34 6598. 264 2.94 131.0 2526. 30.38 25911.50 -10.14 124.7 2303. 27.66 9039. 333 4.75 125.0 2307. 27.68 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25913.50 -10.20 113.2 1901. 22.81 9815. 349 8.28 113.4 1902. 22.77 25913.50 -9.83 101.7 1539. 18.42 9961. 345 11.66 101.8 1535. 18.34 25915.50 -9.83 101.7 1372. 16.32 9950. 348 13.33 95.7 1367. 16.23 </td <td>TEST NO. 9A STAND WGT 40000.LBS</td> <td>MARH TEST WGT 40200.LBS</td> <td>(II AN P 27</td> <td>RESS A</td> <td>STANDARD LT HG</td> <td>TIRES TEMP 4.2 C</td> <td>/DRY RUN WIND 1.8</td> <td>VEL- KTS</td> <td>265.0 ANDARD</td> <td>DEG MAG</td>	TEST NO. 9A STAND WGT 40000.LBS	MARH TEST WGT 40200.LBS	(II AN P 27	RESS A	STANDARD LT HG	TIRES TEMP 4.2 C	/DRY RUN WIND 1.8	VEL- KTS	265.0 ANDARD	DEG MAG
25907.50 -5.38 142.1 3211. 35.94 1577. 071 .33 142.7 3225. 38.36. 25908.50 -6.95 138.8 2973. 34.26 3819. 1164 .99 139.3 2985. 34.36 25909.50 -6.26 134.6 2743. 32.25 32.32 25909.50 -8.68 130.6 2518. 30.34 6598. 264 2.94 131.0 2526. 30.38 25910.50 -8.68 130.6 2518. 30.34 6598. 264 2.94 131.0 2526. 30.38 25910.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25912.50 -9.24 119.1 2098. 25.23 8300. 288 6.47 119.3 2100. 25.22 25913.50 -10.20 113.2 1901. 22.81 9815. 349 8.28 113.4 1902. 22.77 25913.50 -9.81 107.2 1716. 20.45 9039. 312 10.02 107.3 1714. 20.39 25914.50 -9.81 107.2 1716. 20.45 9039. 348 13.33 95.7 1367. 16.23 25915.50 -9.81 107.2 1716. 20.45 9050. 348 13.33 95.7 1367. 16.23 25916.50 -9.61 95.8 1372. 16.32 9950. 348 13.33 95.7 1367. 16.23 25916.50 -9.87 84.2 1068. 12.62 10784. 378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784. 378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784. 378 16.09 84.0 1060. 12.50 25919.00 -10.20 74.2 870. 9.79 11596. 406 18.89 73.8 860. 9.65 25920.00 -9.24 63.4 638. 7.16 10773. 368 21.29 62.9 62.7 7.02 25922.00 -9.24 63.4 638. 7.16 10773. 368 21.29 62.9 62.7 7.02 25922.00 -8.88 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25926.00 -11.31 41.9 280. 313 13940. 469 25.08 41.2 269. 3.00 25928.00 -7.45 35.9 215. 2.30 9236. 315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 2	TEST NO. 9A STAND WGT 40000.LBS	MARM TEST WGT 40200.LBS	< II AN P 27	RESS A	STANDARD LT HG	TIRES TEMP 4.2 C	/DRY RUN WIND 1.8	VEL- KTS	265.0 ANDARD (DIST	DEG MAG
25908.50	TEST NO. 9A STAND WGT 40000.LBS	MARH TEST WGT 40200.LBS GND-SPD	VII AN 27 TE DIST	RESS A .801 IN ST DAY-	STANDARD LT HG FBR	TIRES TEMP 4.2 C UBR .022	VDRY RUN WIND 1.8 EBR .02	VEL- KTSST/ KTAS 146.0	265.0 ANDARD (DIST 3469.	DEG MAG DAY KE 37.76
25909.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95	MARK TEST WGT 40200.LBS GND-SPD 145.4	F 27	RESS A 801 IN ST DAY- KE 37.63 35.94	STANDARD LT HG FBR 393. 1577.	TIRES TEMP 4.2 C UBR .022 .071	VDRY RUN 1.8 EBR .02 .33	VEL- KTSST/ KTAS 146.0 142.7	265.0 ANDARD (DIST 3469. 3225.	DEG MAG DAY KE 37.76 36.06
25910.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1	F 27TE DIST 3452. 3211.	RESS A 801 IN ST DAY- KE 37.63 35.94	STANDARD LT HG 	TIRES TEMP 4.2 C UBR .022 .071 .164	VDRY RUN 1.8 EBR .02 .33 .99	VEL- KTS ST/ KTAS 146.0 142.7 139.3	265.0 ANDARD (DIST 3469. 3225. 2985.	DEG MAG DAY KE 37.76 36.06 34.36
25911.50 -10.14 124.7 2303. 27.66 9039333 4.75 125.0 25.22 25912.50 -9.24 119.1 2098. 25.23 8300288 6.47 119.3 2100. 25.22 25913.50 -10.20 113.2 1901. 22.81 9815349 8.28 113.4 1902. 22.77 25913.50 -9.31 107.2 1716. 20.45 90.39312 10.02 107.3 1714. 20.39 25914.50 -9.81 101.7 1539. 18.42 9961345 11.66 101.8 1535. 18.34 25915.50 -9.83 101.7 1539. 18.42 9961345 11.66 101.8 1535. 18.34 25917.50 -9.61 95.8 1372. 16.32 9950348 13.33 95.7 1367. 16.23 25917.50 -9.91 90.1 1215. 14.46 10595370 14.91 90.0 1209. 14.34 25918.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784378 16.09 84.0 1060. 12.50 25919.00 -11.55 81.4 1001. 11.78 13003452 17.25 81.1 992. 11.65 25920.00 -10.20 74.2 870. 9.79 11596406 18.89 73.8 860. 9.65 25921.00 -9.00 68.8 749. 8.42 10292352 20.12 68.4 739. 8.28 25922.00 -9.24 63.4 638. 7.16 10773368 21.29 62.9 62.7 7.02 25923.00 -8.98 57.7 535. 5.92 10628358 22.38 57.1 524. 5.77 25923.00 -8.98 57.7 535. 5.92 10628358 22.38 57.1 524. 5.77 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25925.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25927.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8	F 27TE DIST 3452. 3211. 2973.	RESS A 801 IN ST DAY- KE 37.63 35.94 34.26 32.25	STANDARD LT HG FBR 393. 1577. 3819. 3230.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136	VDRY RUN 1.8 EBR .02 .33 .99 1.84	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1	265.0 ANDARD (DIST 3469. 3225. 2985. 2753.	DEG MAG DAY KE 37.76 36.06 34.36 32.32
25912.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6	F 27TE DIST 3452. 3211. 2973. 2743.	RESS A .801 IN .ST DAY- KE 37.63 35.94 34.26 32.25 30.34	STANDARD LT HG FBR 393. 1577. 3819. 3230. 6598.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .204	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0	265.0 ANDARD DIST 3469. 3225. 2985. 2753. 2526.	DEG MAG DAY KE 37.76 36.06 34.36 32.32 30.38
25913.50 -10.20 113.2 1901. 22.81 9615. 334 10.02 107.3 1714. 20.39 25914.50 -9.31 107.2 1716. 20.45 9039. 312 10.02 107.3 1714. 20.39 25915.50 -9.83 101.7 1539. 18.42 9961. 345 11.66 101.8 1535. 18.34 25915.50 -9.61 95.8 1372. 16.32 9950. 348 13.33 95.7 1367. 16.23 25917.50 -9.91 90.1 1215. 14.46 10595. 370 14.91 90.0 1209. 14.34 25917.50 -9.87 84.2 1068. 12.62 10784. 378 16.09 84.0 1060. 12.50 25918.50 -9.87 84.2 1068. 12.62 10784. 378 16.09 84.0 1060. 12.50 25919.00 -11.55 81.4 1001. 11.78 13003. 452 17.25 81.1 992. 11.65 25920.00 -10.20 74.2 870. 9.79 11596. 406 18.89 73.8 860. 9.65 25921.00 -9.00 68.8 749. 8.42 10292. 352 20.12 68.4 739. 8.28 25922.00 -9.24 63.4 638. 7.16 10773. 368 21.29 62.9 627. 7.02 25923.00 -8.98 57.7 535. 5.92 10628. 358 22.38 57.1 524. 5.77 25923.00 -8.88 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25925.00 -8.82 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25927.00 -7.45 35.9 215. 2.30 9236. 315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6	F 27 TE DIST 3452. 3211. 2973. 2743. 2518. 2303.	RESS A 801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66	FBR 393. 1577. 3819. 3230. 6598. 9039.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .204 .333	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94 4.75	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0	265.0 ANDARD (DIST 3469. 3225. 2985. 2753. 2526. 2307.	DEG MAG XE 37.76 36.06 34.36 32.32 30.38 27.68
25914.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68 25911.50 -10.14	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7	VII AN 27 27 27 27 27 3452. 3211. 2973. 2743. 2518. 2303. 2098.	RESS A 801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3	265.0 ANDARD (DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22
25915.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2	F 27 TE DIST 3452. 3211. 2973. 2743. 2518. 2303. 2098. 1901.	RESS A -801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .204 .333 .288 .349	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4	265.0 ANDARD DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100. 1902.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 22.77
25916.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2	VII AN 27 27 27 27 27 27 27 34 52 32 11 29 73 25 18 23 03 20 98 19 01 17 16	RESS A 801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3	265.0 ANDARD DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100. 1902. 1714.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 22.77 20.39
25917.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31	MARM TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7	VII AN 27 27 27 27 27 27 3452. 3211. 2973. 2743. 2518. 2303. 2098. 1901. 1716. 1539.	RESS A -801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 9961.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .204 .333 .288 .349 .312 .345	VDRY RUN 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8	265.0 ANDARD DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100. 1902. 1714. 1535.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 22.77 20.36 18.34
25918.50	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25909.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.61	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8	F 27 TE DIST 3452. 3211. 2973. 2743. 2518. 2303. 2098. 1901. 1716. 1539.	RESS A -801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 9950.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7	265.0 ANDARD (DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.39 18.34 16.23
25919.00 -10.20 74.2 870. 9.79 11596. 406 18.89 73.8 860. 9.65 25921.00 -9.00 66.8 749. 8.42 10292. 352 20.12 68.4 739. 8.28 25922.00 -9.24 63.4 638. 7.16 10773. 368 21.29 62.9 627. 7.02 25923.00 -8.98 57.7 535. 5.92 10628. 358 22.38 57.1 524. 5.77 25923.00 -8.38 52.9 442. 4.98 10013. 338 23.29 52.3 431. 4.84 25924.00 -8.38 52.9 442. 4.98 10013. 338 23.29 52.3 431. 4.84 25925.00 -8.82 47.9 356. 4.08 10689. 363 24.14 47.2 346. 3.94 25925.00 -11.31 41.9 280. 3.13 13940. 469 25.08 41.2 269. 3.00 25926.00 -11.31 41.9 280. 3.13 13940. 469 25.08 41.2 269. 3.00 25927.00 -7.45 35.9 215. 2.30 9236. 315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 6767. 208 26.21 31.4 149. 1.75	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.61 25917.50 -9.91	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1	OIST 3452. 3211. 2973. 2518. 2303. 2518. 2303. 1901. 1716. 1716. 1372. 1215.	RESS A 2.801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 14.46	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 10595.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.39 18.34 16.23 14.34
25920.00 -10.20	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25914.50 -9.31 25916.50 -9.83 25916.50 -9.61 25917.50 -9.91 25918.50 -9.87	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2	OIST 3452. 3211. 2973. 2518. 2303. 2518. 2303. 1901. 1716. 1716. 1372. 1215. 1068.	RESS A 2.801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 14.46 12.62	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 10595. 10784.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .204 .333 .288 .349 .312 .345 .348 .370 .378	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0	265.0 ANDARD (DIST 3469. 3225. 2985. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.39 18.34 16.23 14.34 12.50
25921.00	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.83 25916.50 -9.83 25917.50 -9.83	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4	VII AN 27 27 27 27 27 27 27 27 27 27 27 27 27	RESS A 2.801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.32 14.46 12.62 11.78	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 10595. 10784. 13003.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1714. 1535. 1367. 1209. 1060. 992.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.39 18.34 16.23 14.34 12.50 11.65 9.65
25923.00	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.95 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.83 25916.50 -9.83 25917.50 -9.83 25918.50 -9.83 25918.50 -9.81 25918.50 -9.81 25918.50 -9.87 25919.00 -11.55	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2	VII AN 27 27 27 27 27 27 27 27 27 27 27 27 27	RESS A '801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 14.46 11.78 9.79	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9059. 10595. 10784. 13003. 11596.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452 .406	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 68.4	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060. 992. 860. 739.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.39 18.34 16.23 14.34 12.50 11.65 9.65 8.28
25923.00	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.87 25917.50 -9.91 25918.50 -9.87 25919.00 -11.55 25920.00 -10.20 25921.00 -9.00	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 66.8	OII AN 27 27 27 27 27 27 27 27 27 27 27 27 27	RESS A 2.801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 14.46 11.78 9.79 8.42	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9059. 10595. 10784. 13003. 11596. 10292.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452 .406 .352	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12	VEL- KTS 146.0 142.7 139.3 135.1 135.1 135.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 68.4 62.9	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060. 992. 860. 739. 627.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 22.77 20.36 18.34 16.23 14.34 11.65 9.65 8.28 7.02
25925.00 -8.82 47.9 356. 4.08 10689363 24.14 47.2 346. 3.94 25926.00 -11.31 41.9 280. 3.13 13940469 25.08 41.2 269. 3.00 25927.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 2474074 26.35 29.6 107. 1.56	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.87 25916.50 -9.87 25919.00 -11.55 25920.00 -10.20 25922.00 -9.24	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 68.8 63.4	P 27TE DIST 3452. 3211. 2973. 2743. 2518. 2303. 2098. 1901. 1716. 15372. 1068. 1001. 870. 749. 638.	RESS A 2.801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.32 14.46 11.78 9.79 8.42 7.16	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9950. 10595. 10784. 13003. 11596. 10292. 10773.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452 .406 .352 .368	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 81.1 73.8 68.4 62.9 57.1	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1714. 1535. 1367. 1209. 1060. 992. 860. 739. 627. 524.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.22 20.36 18.34 16.23 14.34 12.50 11.65 9.65 8.28 7.02 5.77
25926.00 -11.31 41.9 280. 3.13 13940469 25.08 41.2 269. 3.00 25927.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.18 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 2474074 26.35 29.6 107. 1.56	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.61 25917.50 -9.87 25918.50 -9.87 25919.00 -11.55 25920.00 -10.20 25921.00 -9.00 25922.00 -9.24 25923.00 -8.98	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 68.8 63.4 57.7	VII AN P 27 27 27 27 27 27 27 27 27 27 27 27 27	RESS A '801 IN ST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 11.78 9.79 8.42 7.16 5.92	FBR 393. 1577. 3819. 3230. 6598. 9039. 9815. 9039. 10595. 10784. 13003. 11596. 10292. 10773. 10628.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452 .406 .352 .368 .358	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29 22.38 23.29	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 81.1 73.8 68.4 62.9 57.1 52.3	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1914. 1535. 1367. 1209. 1060. 992. 860. 739. 627. 524. 431.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.27 20.36 18.34 16.23 14.34 12.50 11.65 9.65 8.28 7.02 5.77 4.84
25927.00 -7.45 35.9 215. 2.30 9236315 25.80 35.1 205. 2.16 25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 2474074 26.35 29.6 107. 1.56	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.81 25917.50 -9.91 25918.50 -9.87 25919.00 -11.55 25920.00 -10.20 25921.00 -9.00 25922.00 -9.24 25923.00 -8.98 25924.00 -8.38	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 66.8 63.4 57.7 52.9	VII AN 27 27 27 27 27 27 27 27 27 27 27 27 27	RESS A '801 IN '87.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 14.46 12.62 11.78 9.79 8.42 7.16 5.92 4.98	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9950. 10595. 10784. 13003. 11596. 10292. 10773. 10628. 10013.	TIRES TEMP 4.2 C UBR .022 .071 .164 .136 .264 .333 .288 .349 .312 .345 .348 .370 .378 .452 .406 .352 .368 .358	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29 22.38 23.29 24.14	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 68.4 62.9 57.1 52.3 47.2	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060. 992. 860. 739. 627. 524. 431. 346.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.27 20.36 18.34 16.23 14.34 12.50 11.65 9.65 8.28 7.02 5.77 4.84 3.94
25928.00 -5.38 32.3 157. 1.86 6767208 26.21 31.4 149. 1.75 25928.00 -5.38 32.3 157. 1.86 2474074 26.35 29.6 107. 1.56	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25915.50 -9.81 25923.00 -10.20 25922.00 -10.20 25922.00 -9.24 25923.00 -8.88 25925.00 -8.88	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 68.8 63.4 57.7 52.9 47.9	VII AN P 27 P 2	RESS A -801 IN -801	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9950. 10595. 10784. 13003. 11596. 10292. 10773. 10628. 10013. 10689.	TIRES TEMP 4.2 C	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29 22.38 23.29 24.14 25.08	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 68.9 57.1 52.3 47.2 41.2	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060. 992. 860. 739. 627. 524. 431. 346. 269.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.27 20.36 18.34 16.23 14.34 12.50 11.65 9.65 8.28 7.02 5.77 4.84 3.94 3.00
25725000 114 1 66 2474 1074 76.35 69.6 1010 1050	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.81 25917.50 -9.91 25918.50 -9.87 25919.00 -11.55 25920.00 -10.20 25921.00 -9.00 25922.00 -9.24 25923.00 -8.88 25925.00 -8.88 25926.00 -11.31	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 68.8 63.4 57.7 52.9 47.9 41.9	VII AN P 27 TE DIST 3452. 3211. 2973. 2743. 2518. 2303. 2098. 1901. 1716. 1539. 1372. 1215. 1068. 1001. 870. 749. 638. 535. 442. 356. 280.	RESS A 2.801 IN EST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 14.46 12.62 11.78 9.79 8.42 7.16 5.92 4.98 4.08 3.13	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 90595. 10595. 107984. 13003. 11596. 10292. 10773. 10628. 10013. 10689. 13940. 9236.	TIRES TEMP 4.2 C	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29 22.38 23.29 24.14 25.08 25.80	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 682.9 57.1 52.3 47.2 41.2 35.1	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1269. 1060. 992. 860. 739. 627. 524. 431. 346. 269. 205.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.27 20.36 18.34 16.23 14.36 11.65 9.65 8.28 7.02 5.77 4.84 3.94 3.00 2.18
	TEST NO. 9A STAND WGT 40000.LBS TOD ACCEL 25906.56 -4.95 25907.50 -5.38 25908.50 -6.26 25910.50 -8.68 25911.50 -10.14 25912.50 -9.24 25913.50 -10.20 25914.50 -9.31 25915.50 -9.83 25916.50 -9.83 25916.50 -9.81 25917.50 -9.91 25918.50 -9.87 25919.00 -11.55 25920.00 -10.20 25922.00 -9.24 25923.00 -8.88 25925.00 -8.88 25925.00 -8.88 25925.00 -11.31 25927.00 -7.45	MARK TEST WGT 40200.LBS GND-SPD 145.4 142.1 138.8 134.6 130.6 124.7 119.1 113.2 107.2 101.7 95.8 90.1 84.2 81.4 74.2 68.8 63.4 57.7 52.9 47.9 41.9 35.9	VII AN P 27 P 2	RESS A 2.801 IN EST DAY- KE 37.63 35.94 34.26 32.25 30.34 27.66 25.23 22.81 20.45 18.42 16.32 11.78 9.79 8.42 7.16 5.92 4.98 4.08 3.13 2.30 1.86	FBR 393. 1577. 3819. 3230. 6598. 9039. 8300. 9815. 9039. 10595. 10784. 13003. 11596. 10292. 10773. 10628. 10013. 10689. 13940. 9236. 6767.	TIRES TEMP 4.2 C	VDRY RUN WIND 1.8 EBR .02 .33 .99 1.84 2.94 4.75 6.47 8.28 10.02 11.66 13.33 14.91 16.09 17.25 18.89 20.12 21.29 22.38 23.29 24.14 25.08 25.80 26.21	VEL- KTSST/ KTAS 146.0 142.7 139.3 135.1 131.0 125.0 119.3 113.4 107.3 101.8 95.7 90.0 84.0 81.1 73.8 68.4 62.9 57.1 52.3 47.2 41.2 35.1 31.4	265.0 ANDARD (DIST 3469. 3225. 2753. 2526. 2307. 2100. 1902. 1714. 1535. 1367. 1209. 1060. 992. 860. 739. 627. 524. 431. 346. 269. 205. 149.	DEG MAG KE 37.76 36.06 34.36 32.32 30.38 27.68 25.27 20.36 18.34 16.23 14.36 11.65 9.65 8.28 7.02 5.77 4.84 3.94 3.00 2.18 1.75

TEST NO.	104	F-41	eK II as	TISKI	VST4NOAR		WET HUN	*AY	1	k pedi
STAND 40		TEST #6	1 +	7.520	ALT	TEAP	MINO De4		MIND	DIREC DEG MAG
40000000		1				28		1 1 0	19793	60.15
					(ANDARD	The second second second
C. C. 257 E	0.000	GMB-SPD	6157	KF	FHR	UHS	FEY	KTAS	DIST	KE
27748.65	-3.93		touns.	44.3			0.00	150.2	9072.	
27749.50	-3.45		4904.	43.3		0.000	0.00	148.5	8884 .	
27750.50	-4.95		9545.	41.9.		*0.31	-00	145.9	H635.	T. 0 T. C. 2
27751.50	-4.07		9292.	40.50	· · · · · · · · · · · · · · · · · · ·	0.000	.09	143.3	8392.	36.36
27752.50	-4.14		9039.	39.1		0.000	.09	140.8	8154.	35.12
27753.50	-3.84		4791.	34 . 15		0.000	.09	138.7	7920 •	34.05
27754.50	-4.18		4567.	36.77		1200	•18	136.2	7689.	32.86
27755.50	-3.81		4307.	35.00		*00H	.51	134.0	7463.	31.82
27756.50	-4.40	136.6	8072.	34.3		.05]	.44	131.4	7239.	30.58
27757.50	-3.65	136.3	7534.	33.1		.017	.59	129.1	7020.	29.50
27758.50	-4.09		7511.	32.13		.044	.76	126.9	6806.	28.53
27759.50	-4.42	131.5	7350.	30.45	1715.	. Gn5	1.12	124.3	6594.	27.38
27760.50	-3.46	120.9	7107.	24.00	654.	.025	1.40	121.8	6386.	26.26
27761.50	-3.47		6950.	29.03	637.	.009	1.42	120.3	6187.	25.64
27762.50	-4.06		n737.	27.91	1091.	· unl	1.72	117.9	5985	24.60
27763.50	-3.53	122.9	4524 .	26.98	1145.	+1141	1.97	115.8	5790.	23.74
27764.50	-3.52		2327.	20.00	137/.	050	2.23	113.7	5598.	22.89
27765.50	-3.52		5120 ·	75.11	land.	.004	2.58	111.5	5409.	55.00
27766.50	-3.44		9922.	24.14	1505.	+051	2.40	109.3	5224.	21.16
27767.50	-3.63		5727.	- 83.32	1885.	. 464	3.24	107.2	5042.	20.36
27768.50	-3.19		5535.	22.53		- uep	3.53	105.3	4865.	19.63
27770.00	-3.70		5256.	21.35		.074	4.01	102.3	4604.	18.54
27771.00	-4.05		5073.	20.44		.092	4.40	100.1	4434.	17.74
27772.00	-3.34		4994.	19.61		066	4.91	97.8	4267.	16.94
27773.00	-3.10		4719.	18.99		.059	5.21	96.1	4106.	16.37
27774.25	-3.11		4504.	18.04		.062	5.64	93.6	3908.	15.52
27775.25	-3.53		433h.	17.41		.083	6.03	91.8	3753.	14.93
27776.25	-3.33		4171.	16.56		.077	6.44	89.7	3601.	14.26
27777.25	-2.58		40100	16.01		·uh?	6.79	47.8	3452.	13.64
27778.25	-3.72		3851.	15.54		.098	7.15	86.4	3309.	13.21
	-3.71		3597.	14.01	The second	.1149	7.71	83.6	3163.	12.37
27779.25				13.94	44.2	.055	8.13	81.5	2991.	11.76
27780.50	-2.73		35000	13.46	ALC: NO.	.005	8.40	79.9	2858.	11.29
27781.50	-3.55		3300.					17.6	2725.	10.68
27782.53	-3.35		3214.	17.75		.043	8.92		2597.	10.20
27783.50	-3.16		3674.	15.00		*UH7	9.29	75.9		9.39
27785.00	-3.10		depar.	11.30		•090	9.90	72.8	2409.	
27736.00	-3.06		273=+	10.04		.047	10.56	71.1	2289.	8.95
2,7787.00	-3.06		2500.	10.35	and the second second	.09]	10.62	69.3	2173.	8.51
27788.00	-3.13		2474.	9.4.		.095	11.01	67.4	2059.	8.05
27789.00	-5.95		53500	9 3		*OHA	11.35	65.8	1947.	7.66
27790.00	-2.69		55330	0.90		. UM2	11.69	64.0	1839.	7.24
27790.10	-2.59	70.7	2206.	3.97	2472.	.077	11.69	63.9	1815.	7.24

TEST NO.	114	MARK	III AN	TISKID/	STANDARD	TIRES/	DRY RUN	AY		
1531 401						TEHP	H IND		WIND	DIREC
STAND WE	T	TEST WGT		RESS A			10.4	VIS	218.0	CEG MAG
40000.LB3		40050.LBS	27	.535 IN	H3	5.5 C	10.4			
		-		2012.0.				STA	NDARD D	AY
			TE				EBR	KTAS	DIST	KE
TOD	ACCEL	GND-SPD	DIST	KE.	FBR	UBR	.00	137.8	2761 .	33.64
25147.10			3113.	38.35	87.	.004	.90	134.4	2555 .	31.99
25148.00			2891.	3€.59			2.89	128.2	2331 .	29.09
25149.00			2653.	33.52	8963.	.427		121.8	2117 .	26.28
25150.00	-11.94		2427.	30.52	100 22.		5.03	114.8	1911.	
25151.100	-11.31		2212.	27.36	11056.	.410	7.36	108.3	1718 .	
25152.00	-11.29	Company of the second s	2007.	24.57	11334.		9.50		1536 .	18.16
25153.00	-11.04	and the second s	1814.	21.76	11417.		11.82	101.3	1367 .	
25154.00	-10.11		1632.	19.46	10539.		13.73	95.2	1208 .	
25155.00	-10.60		1461.	17.26	11545.		15.62	89.0	1059 .	
25156.00	-10.0	5277	1300.	15.13	10985.		17.41	82.7	921 .	
25157.00	-10.2		1149.	13.26	11479.		19.08	76.7	792 .	
25157.00	-10.3	The state of the s	1008.	11.43	11819.		20.71	70.5	201,212	
25158.00	-10.0		877.	9.78	11651.		22.21	64.4	675 .	
25159.00		12 12 12 12	757.	8.32	11015.	.385	23.53	58.6	568 •	- 1000
25160.00			646.	7.03	10887.	.379	24.73	53.0	470 .	4.09
25161.00		7 2 2 2 4	544.	5.97	10374.	.346	25.76	48.0	364 .	2.00
25162.00			451.	4.91	10697.	.362	26.74	42.6	305 •	The second second
25163.00			366.	3.97	11427.		27.56	37.3	235 .	E
25164.00	-9.2		291.	3.11			28.47	31.8	175 .	
25165.00				2.42			29.14	26.8	124 .	
25166.00			224.			7.7	29.68	22.0	82 .	
25167.00	-7.3		166.					20.9	75 .	.78
25167.20	-6.5	1 31.1	155.	1.72	95 000		1000			

TEST NO.	124	MARK	III AN	TISK IDA	STANDARI) TIRES	ZWET RUNI	WAY		
STAND WG		TES1 WGT +0350.LBS		RESS A		TEMP 3.7 C	WIND 6.5			DIREC DEG MAG
	,		TE	CT DAY-				51	ANDARD [)ΔΥ
TOD		GND-520	DIST	, KE	FBR	HBR	EBR	KTAS	DISI	KE
24739.55	-3.38	151.8		41.15		0.000	0.00	146.5	6979	38.00
24740.50	-3.95		/267	39.98		0.000	0.00	144.3	6746.	
24741.50	-4.56	147.4	7017.	38.31			.04	142.1	6505.	
24742.50	-4.41	144.3	5771.	37.21	641.	.028	.28	139.0	6266.	
24743.50	-3.50	142.2	6529	36.12		0.000	.29	136.8	6034.	33.15
24744.50	-3.92		6290.	35.07	289.	010	2.1	134.7	5806.	32.14
24745.50	-4.12	137.7	6056.	33.85	776.	.032	. 45	132.3	5581 •	
24746.50	-3.93	135.3	5826.	32.68	706.	.028	.61	129.8	5360.	
24747.50	-3.33	133.2	5599.	31.70	46.	.005	•67			- 28.90
24748.50	-3.63	131.2	5370.	30.76	507.	.021	.74	125.8	4932	
24749.50	-4.18	128.8	5157.	29.65	1421.	.055	•98	123.4	4722	
24750.50	-4.24	126.1	4941.	28.42	1691.	.064	1.37	120.6	4516.	25.77
24751.50	-3.74	124.0	4730.	27.45	1192.	.044	1.63	118.4	4315 4118	24.84
24752.50	-4.10	121.7	4523.	26.45	1789.	■ 065	1.94	116.1	4118.	23.88
24753.50	-3.77	119.1	4320.	25.35	1539.	• 056	2.31		3925	
24754.50	-3.75	117.2	4121.	24.52	1631.	059	2.58	111.6	3737.	
24755.50	-4.45	114.6	3925.	23:47	2673.	. 1195	3.05		3551	
24756.50		112.0	3734.	22.39	3421.	•116	3.63	106.3	3369.	20.03
24757.50		104.0	3547.	21.20	3143.		4.27			.18.90
24758.50	-4.06	106.7	3365.	20.35	2780.	•091	4.13	101.1		18.08
	-4.97		3187.	19.33	4035	•133	5.38		2851	
,	4.41	101.1	3014.	18.28	3482.	.115	6.03	95.4	2687	16.13
24761.50	-4.39	98.5	2845.	17.33	3592	117	6.62	92.8		15.24
	-4.44	96.2	2581.	16.52	3753.	124	7.18	90.4 87.5	2374	14.48
24763.50	-4.83	93.3		15.55	4383.		7.85 8.50	0/ 0	2078	-13.57- 12.71
24764.50	-4.56	90.5	2365	14.63	4162.			84.7 82.2	2078.	
24765.51	-4.07	88.1	2215.	13.85	3636	118	9.06 9.71	79.5	1901.	
24766.50	-5.17	85.4	2059.	13.02	5135.	.164 .102	10.31	76.5	1669	10.37
24767.50	-3.57	82.4	1928	11.62	3260. 4728.	.154	10.51	74.8	1544	9.90
24768.50	-4.70	H().7	1790. 1657.	10.71	4857.	•15A	11.48	71.5	1420.	9.06
24769.50	-4.71 -4.39	77.4 74.8	1529.	10.00	4554.	145	12.05	68.9	1302.	8.40
24770.50 24771.50	-4.68	72.2	1404	9.30	5018.	.157	12.65	66.2	1189.	7.77
24772.50	-4.38	69.5		8.62	4719.	149	13.22	63.5	1080.	7.14
24773.50	-4.89	6h.8	1170.	7.96	5442	.176	13.80	60.8	975.	6.54
24774.50	-4.85	64.0	1059.	7.32	5484.	.174	14.38	58.0	876.	5.96
24775.50	-5.33		954	6.61	6170.	199	15.02	54.8	780 .	
24776.50	-3.33	56.4	554.	6.08	3745.	.116	15.47	52.3	692.	4.84
	-5.22	55.9	757.					49.8		4.39
24778.50	-5.41	56.6	566.	4.94	6488.	.208	16.55	46.5	526.	3.82
24779.50	-5.18	49.5	580.	4.37	6280.	0.05	17.09	43.3	450.	3.33
24780.50	-5.48	46.3	400.	3.83	6726.	.212	17.61	40.2	380•	2.86
24781.50	-5.92	42.8	423.	3.28	7352.	.231	18.14	36.7	315•	2.38
24782.50	-4.83	39.8	354.	2.83	6031.	•195	18.58	33.6	257.	2.00
24783.50	-5.55	36.7	289.	2.40	7008.	•21B	19.00	30.4	203.	1.64
24784.50	-5.97	33.3	230.	1.99	7573.	.245	19.42	27.1	155.	1.30
24785.50	-5.23	29.5	176.	1.56	6725.	808.	19.A0	23.3	112.	•96
24786.50	-3.36	27.5	150.	1.35	4395.	• 1.30	20.03	21.2	79.	•79
24787.50	-2.16	25.5	84.	1.16	2920.	.092	20.18	19.2	49.	•65
24787.60	-2.05	25.4	80.	1.16	2781.	•04R	20.18	19.1	47.	•65

TEST NO.	128	MARK	111 AN	TISKIDZS	STANDARD	TIRES	WET RUNI	MAY		
STAND WG		TEST WGT	р	KESS AL	Т	TEMP	WIND		WIND	DIREC
36000.L95		6050.LBS		565 TN		6.0 C	5.7	KIS	224.0	DEG MAG
			***	ST DAY				ST	ANDARD ()AY
					FAR	UBR	EBR	KTAS "		KE
TOD		GMD-SPD	DIST	KE 17		0.000	0.00	132.8	5817.	28.12
27277.10	-3.68	137.5	4202.	30.17	540:	- 025	.06	130.5	5615.	27.16
27278.00	-4.22	135.2	5994	29.18	725.		.20	128.2	5395.	26.19
27279.00	-4.25	132.9	5768	28.18	342.	.016	.32	125.7	5179.	25.17
27280.00	-3.78	130.4	5546	27.13	103.	.005	36	123.5	4968	24.31
27281.00	-3.47	128.2	5328		991.	.044	.49	121.4	4761	23.49
27282.00	4.13	126.2	5113.	25.40		0.000	.62	118.9	4558	22.53
27283.00	-3.12	123.7	4903.	24.41	1348.	.059	.76	117.0	4358.	21.80
27284.00	-4.21	121.7	4595.	23.65	1537.	.065	1.08	114.4	4161.	20.85
27285.00	-4.23	119.2	4492.	22.67		•055	1.34	112.0	3970.	19.99
27286.00	-3.91	11c.8	4293.	21.78	1308	-080	1.71	109.4	3781.	19.06
27287.00	-4.50	114.2	4097.	20.82	2129	.031		107.2	3598	18.32
27288.00	-3.15	112.1	3907.	20.05	753.	.076	2.21	105.0	3419	17.57
27289.00	-4.00	109.9	3720.	19.27	1833.	.081		102.6	3243.	16.78
27290.00	-4.04	167.5	3536.	18.45	2044 <u>.</u> 2929 •	•H5	3.03	100.0	3070 •	
27291.00	-4.68	104.9	3357•	17.56	1933.	.073	3.45		: 2903.	
27292.00	-3.63	102.3	3182.	16.71		.115	3.87	95.2	2740 .	14.44
27293.00	-4.55	100.2	3011.	16.01	3075 • 2331 •	.089	4.35	92.3	2581.	13.58
27294.00	-3.77	97.3	-2845	15.11	3497.	.130		90.1	2426.	12.95
27295.00	-4.71	95.1	2582	14.45	_	105	5.33	87.2	2276.	
27296.00	-3.97	92.3	2524•	13.59	2796		5.83	84.8	2129	
27297.00	-4.75	89.9	2370.	12.89	3779. 2984.	.142 .110	6.34	82.0	1988.	
27298.00	-3.94	87.1	2221.	12.10	3769	.137	6.81	79.7	1851.	
27299.00	-4.55	84.8	2075	11.48	3024	.112	7.30	76.9	1718.	9.43
27300.00	-3.80	82.0	1935.	10.74	3781.	- 139	7.75	74.8	1591.	. 8.92
27301.00	-4.41	79.9	1798	10.20 9.44	3738	.137	8.29	71.8	1466.	
27302.00	-4.27	76.9	1566.		4125.	152	8.76	69.4	1347.	7.68
27303.00	-4.54	74.6	1538.	8.88	4789.	.178	9.34	66.4	1230.	7.04
27304.00	-5.04	71.6	1414.	8.19	4549	.167	9.88	63.6	1120.	
27305.00	-4.74	68.8	1296•	7.55	4335.	.161	10.38	60.8	1014.	
27306.00	-4.48	66.0	1152.	6.95	4744.		10.87	58.1	914.	5.38
27307.00	-4.77	63.3	1072.	6.40	4666		11.37	55.1	817.	4.84
27308.00	-4.63	60.4	968.	5.82	4879.		11.82	52.7	727.	4.42
27309.00	-4.76	55.0	568.	5.36	5110.		12.32	49.4	640.	3.89
27310.00	-4.88	54.7	773.	4.78	5031.	.185	12.75	46.7	559.	3.47
27311.00	-4.75	52.0	583.	4.31	5714.		13.21	43.8	482.	3.05
27312.00	-5. 30	49.1	597 •	3.85 3.37	5296		13.65	40.6	411.	2.62
27313.00	-4.85	46.0	517•	2.97	5789		14.05	37.8	345.	2.27
27314.00	-5.24	43.2	442.	2.54	6367		14.47	34.5	284.	1.90
27315.00	-5.71	39.9	372.	2.12	5934		14.87	31.0	228.	1.53
27316.00	-5.27	36.4	307.	-	6797		15.23	28.1	178.	1:26
27317.00	-6.00	33.6	248.	1.80	7134		15.61	23.9	133.	
27318.00	-6.23	29.4	195.	1.38 1.10	6745	246	15.90	20.7		•68
27319.00	-5.85	26.2	148	.79	7720		16.21	16.5	63.	
27320.00	-6.68	22.2	107.	59	2649		16.35	13.7	39	30
27321.00	-2.12	19.3	73.	• 59	<u>.</u> ∪+7•	• • • • •				

TEST NO. 1	ЗА	MARK	III ANT	ISKID/S	TANDARD	TIRES	MET KON	μAΥ		
•			nt.	mee Ai	τ	TEMP	MIND	VEL.	MIND 0	1REÇ
STAND WGT		TEST WGT	27	ESS AL	•	4.0 C	1.6		240.0 [DEG MAG
43000.LBS	42	2800.LBS	21.	1 E E E	.1/1					
			TES	Y40 T				STA	NDARD DA	/Y
	ACCEL (GND-SPD	DIST	KE .	FBR	UHR -	EDW		0101	KE
		143.1	7200.	38.23	184.			145.0	7545•	40.00
24546.61	-4.04	139.1	6808.	36.15	268.		17 -	.140.∙9	7130	31.19
24548 • 25	-3.98	137.1	5575	35.13		0.000			6884	35.71
24549 - 25	-3.64		1914	33.87	762.	.031	•33	136.3	6641	
24550.25	-4.09	134.6	6120.	32.83	0.	0.000	.36	134.2	6403.	34.28
24551.25	-3.06	130.7		31.91	739.	.028	.42	132.3	6169.	,33 • 32
24552.25	-3.85	128.0	5580.	30.62	1349.	.050	.71,	4	5938	31.96
24553.25	-4.15	125.9	5465.	29.61	. 1127.	.041	•93	127.4	5711.	30.89
24554.25	-3.87	123.5	5255	28.51	1286.	.046	1.20	125.0	5489	
24555.25	-3.88	121.3	5048		1397.	.050	1.47	122.7	5271.	28.64
24556.25	-3.87		4845.		1045.	.037	1.71	120.4	5057	
24557.25	-3.49	119.1	4647.	25.55	1782.	.061	1.99	118.2	4847.	
24558 • 25	-3.92		4451.	24.46	1954.	.067	2.39	115.6	4641.	
24559 25	-3.93	114.4	4260.	23.59	1712.	.056	2.70	T. T. C. T.	4440.	
24560.25	-3.57	112.4	4072	22.58	2704.	.086	3.15		4241.	
_ ,	-4.19	-	3588	21.64	2725.	.088	3.63	108.7	4048.	
24562.25	-4.12	107.6	3709.	20.69	2236	.073	4.09	106.2		-21.47
24563.25		-105.2	3533.	19.97	1731.	.054	4.39	104.3	3674.	20.72
2456425	-3.17	103.4	3360.	19.05	3433	-109	4.90	101.9	3491.	19.75
C 10000	-4.38	101.0	3192.	18.19	3274.	.102	5.44	99.5	3315.	18.85
24566.25	-4.15	98.7		17.21	2791 •		5.96	96.8 -		17.82
24567.25	-3.6B	96.0	3028.	16.49	3073.	.094	6.40	94.7	2973.	17.06
C 122012	3.82	94.0	2367	15.70	3161.	.095	6.88	92.3	2808.	16.23
24569 • 25	-3.80	91.7	2710. 2558.	14.94	3012.		7.35	90.0	2648	15.43°
24570.25	-3.63	89,4	2409	14.28	3529.		7.80	0.88	2492•	14.74
24571.25	-3.95	87.4		13.44	3956.		8.37	95.3	2339.	13.86
24572.25	-4.19	84.8	2263•	12.73	4044.		8.91	83.0	5191.	13.10
24573.25	-4.18	(/ 4 -	5155.	11.99	3953.		9.44	80.5	2047.	12.33
24574.25	-3.95	80.1	1984.	11.36	3229		9.49	78.3	1908.	11.67
24575.25	-3.41	78.0	1851	10.68	4422.		10.41	75.9	1772.	10.96
24576.25	-4.26	75.6	1721.	10.13	2981		10.83	73.9		. 10.38
24577.25	-3.11	73.6	1596	9.40	5275		11.40	71.1	1513.	9.62
24578.25	-4.78	70.9	1473.	9.76	3642		11.91	68.6	1390•	8.95
24579.25	-3.47	68.5	1356	55.8	4720.		12.38	66.4	1271.	8.38
24580.25	-4.24	66.3	1242	7.59	4641.		12.90	63.7	1157.	7.73
24581.25	-4.11	63.8	1132.	7.06	5011.		13.39	61.4	1047.	7.17
24582.25	-4.34	61.5	1026		6356		13.99	58.4	941.	6.50
24583.25	-5. 31	58.6	925.	6.41 5.77	5416		14.55	55.3	841.	5.83
24584.25	-4.53		929•	5.27	5513		15.02	52.8	747.	5.32
24585.25	-4.54	53.1	738		6057		15.56	49.4	656.	4.65
24586.25	-4.89	49.8	550	4.63	6288		16.06	46.6	57l•	4.13
24587.25	-5.00	47.0	568	4.12	6355		16.54	43.5	491.	3.61
24588.25	-5.01	44.0	491.	3.62	6418		16.98	40.6	418.	3.14
24589.25	-5.01	41.2	419.	3.17	6838		17.41	37.7	349.	2.70
24590.25	-5.28		352•	2.74	8603		17.89	34.1	285•	
24591.25			290.	2.25 1.88	7789		18.13	30.9	242.	1.82
24592.00	-5.91	31.7	248•	I • O.O.	1100	# 14				

TEST NO. 1	38	MARK	III AN	TISKI	D/STANDARI	D TIRES	FT RUN	IWAY		
STAND WGT		TEST WGT	p	RESS	ALT	TEMP	WIND	VEL	WIND	DIREC
38000.L3S		37875.LBS				7.0 C		KTS	217.0	DEG MAG
			T	CT D.				CT	ANDARD (1AV
TOD	ACCEL	GND-SPD	OIST	SI DA	Y Fвк	UBR	EBR		ANDARO (DIST	KE
			6655.	32.8		0.000		138.4	6558	32.22
	-3.62	139.9				0.000		136.6	6340	31.39
	-3.97	138.1	6437	31.9			.18	133.7	6107.	30.05
	-4.32		6206	30.6		0.000	.19	131.7	5881	29.16
	-3.62	133.2	5980.	29.7 28.6		-024	•32	129.1	5657	
	-3.99	130.7	5757.	27.7		0.000	•34		" 5438 •	27.15
	-3.27	128.6	5539.	26.8		.018	.40	124.8	5222	26.22
	-3.64	1,57,13,9,5	5323.			.027	• 48	122.9	5011.	25.40
	-3.72	124.5	5111.	26.0		- 4	, , , ,	120.5		24.41
		122.1	4903.	25.0		.037	- •66 - •87	118.3	4599	23.52
	-4.03	120.0	4699	24.1		•053		115.7	4399	22.52
	-3.74	117.4	4498	23.1		•045				21.72
		115.4	4302.	22.3		.059	1.37	113.6	4202	20.74
	-4.20	112.8	4109.	21.3		.076		111.0	4010	19.90
	-3.38	110.6	3921.	20.4		.044	1.99	108.8	3822. 3638.	19.20
	-4.29	108.6	3735.	19.7		089	2.28			
	-4.23	105.7	3555.	18.7		.093	2.77	103.8	3457	18.14
	-3.35	103.8	3378.	18.0			3.04	99.4		16.62
	-4.53	101.3	3205.	17.2		•111 •òà	3.49 3.97.		2941.	15.76
	-3.99		3036.		2560	.094	4.35		2778	15.08
	-3.75	96.6	2571.	15.6		•086		92.1	2618	14.28
	-4.13	94.1	2710.	14.8		•106	4.81		2463.	13.56
	-4.04	91.8	2553.	14.1		•106	5.26 5.79	89.8 87.2	2311.	12.80
	-4.58	89.3	2400.	13.3		.131	6.29	84.6	2165	12.05
	-3.92	86.7	2252.	12.6		-106	6.77	82.2	2022.	11.37
	-4.35	84.3	2108.	11.9		•131	7.36	79.3	1883.	10.58
	-4.71	81.4	1967.	11.1		.147			1750.	.9.99
	-4.02	79.2	1833.	10.5		.123	7.83	77.1	1620.	9.21
	-5.07	76.2	1701.	9.7		.170	8.42			8.54
	-4.38	73.5	1575.	9.0		•144	8.97	71.3	1496	7.88
	-4.15	70.7	1453.	8.3		•136	9.48	68.5	1376	
	-4.26	66.8	1335.	7.9		» 145	9.90	66.6	1262.	7-46
	-5.17	65.5	1555.	7.1		.186	10.50	63.2	1150.	6.71 6.19
	-4.16	63.0	1114.	6.6		•148	10.97	60.7	1044.	
	-4.65	60.4	1010.	6.1		.167	11.44	58.1	943.	5.67
	-4.24	57.6	910.	5.5		.154	11.90	55.2	846.	5.13
	-5.69	55.0	815.	5.0			12.42	52.5	754.	
	-3.89	51.8	726.	4.5		.146	12.98	49.3	667•	4.10
	-5.21	49.2	640.	4.0		.200	13.31	46.8	585	3.68
-	-5.60	45.8	560.	3.5		-221	13.82	43.3	507.	3.16
	-5.44	42.5	486.	3.0		•216 •216	14.29	40.0	436.	2.69
	-4.95	39.3	417.	2.5		.201	14.69	36.7	369.	2.26
	-6.26	36.2	352.	2.2		.250	15.11	33.6	308.	1.90
	-5.12	32.6	295.	1.7		- •209	15.49	30.0	253.	1.51
-	-5.68	29.5	242.	1.4		.236	15.82	26.8	204.	1.21
_	-3.46	26.7	195.	1.1		.146	16.06	24.0	161.	•97
27046.87	-3.07	25.5	168.	1.0	9 3802.	•123	16.13	22.8	137.	∗ 87

TEST NO.	13C	MARK	de ha	TISKID/S					HITME	DIREC
STAND WG	The second second	TEST WGT	p	KESS AL	T HG	TEMP	1.8	VEL KTS	SS0'0 MIMD	DEG MAC
34000.LBS	3	4400,Las			14.5	NA .	E /- 1 - 1 /	4673 - 64		
			TE	ST DAY				STA	DIST	KE
TOD	ACCEL	GND-SPD	DIST	KE	FHR	UHR	EBR	126.5	5191.	24.08
28983.39	-3.58	128.3	5391 .	25.06		0.000	0.00		4959.	23.13
28984.50	-3.95	125.8	5153.	24.09	315.	.016	.04	124.0	4754.	22.19
28985.50	-4.64	123.2	4943.	23.13	1216.	.061	.24	121.4	4554.	21.24
28986.50	-3.85	120.6	4734.	22.14	. 551.	.027	.44	118.8	4358.	20.48
28987.50	-3.24	118.5	4536.	21.37		0.000	.49	116.7	4165.	19.82
28988.50	-3.81	116.6	4337.	20.69	778.	.037	.56	114.8	3976.	18.98
28989.50	-3.83	114.1	4143.	19.03	966.	.045	.77	112.3	3790.	18.20
28990.50	-4.13	111.8	3952.	19.02	1402.	.064	1.00	109.9	3609.	17.38
28991.50	-3.81	109.3	3766.	18.18	1217.	.054	1.27	107.5		16.70
28992.50	-3.90	107.1	3583.	17.48	1409.	.004	1.49	105.3	3432.	15.88
28993.50	-4.43	104.5	3404.	16.63	2105.	.117	1.64	102.7		15.07
28994.50	-4.96	101.9	3230.	15.80	2954 .	.125	2.29	100.1	3089.	14.18
	-4.13	98.9	3061.	14.89	2246.	.093	2.75	97.1	2924.	13.56
28995.50 28996.50	-3.99	96.7	2596.	14.24	5553.	.009	3.08	94.9	2754.	12.88
	-3.75	94.3	2735.	13.55	2083.	-082	3.43	92.5	2608.	
28997.50	-5.06	91.9	2577.	12.97	3596.	.141	3.89	90.1	2455.	
28998.50	-3.09	89.3	2425.	12.13	1510.	.003	4.27	87.4	2308.	
28999.50	-4.17	87.2	2275.	11.59	2858.	.112	4.61	85.4	2164.	10.40
29000.50	-4.44	84.9	2130.	10.98	3229.	.130	5.04	83.1	2024.	
29001.50	-4.92	81.9	1990.	10.22	3891.	.151	5,56	80.1	1887.	
29002.50	-4.40	78.9	1554.	9.48	3444.	.137	6.07	.77.1	1755	
29003.50	-4.67	76.8	1722.	6.98	3812.		6.50	75.0	1629.	
29004.50	-3.45	44.00	1590.	8.29	2627.		6.94	72.0	1389.	
29006.50	-4.75	72.0	1472.	7.90	4073.		7.30	70.2	1274	
29007.50	-4.61	68.5	1354.	7.15	4050.	.157	7.84	66.7	1165.	
29008.50	-4.17	and the second second	1245.	6.75	3634.	.142	8.55	64.8	1059	
	-4.71	63.5	1131.	6.14	431B.	.168	8.69	61.7		
29009.50	-4.43		1625.	5.64	4108.	.157	9.12	59.0	958	
29010.50	-3.89		925.	5.23	3599.	.137	9.48	56.8	863	
29011.50	-5.08	The second second	523.	4.70	4946.	.193	9.94	53.8	770	
29012.50	-4.57	The second second	737.	4.50	4470.	.172	10.33	51.3	683	
29013.50	-4.90	17.46	650.	3.77	4909.		10.77	48.0	600	
29014.50	The state of the s	11	567.	3.39	5473.	.212	11.17	45.4	521	
29015.50	-5.37	The second secon	490.	2.46	5185	200	11.57	42.3	449	
29016.50	-5.03		410.	2.55	5163.		11.95	39.1	381	2.3
29017.50	-4.94	The state of the s	352.	2.24	5543		12.28	36.6	. 318	
29018.50	-5.25		240.	1.78	7074		12.69	32.4	259	4
29019.50	-6.61	The Property and the Control of the	235.	1.44	5766		13.03	29.0	508	
29020.50	-5.33			1.22	2384	200	13.21	26.5	163	
29021.50			179.	1.21	2360		13.21	26.3	157	. 1.0
29021.64	-2.08	3 28.1	1170							

TEST NO. 1	44	MARK	III ANT	ISKID/S	TANDARD	TIRES/	DRY RUNI	WAY		
STAND WGT	.8'	FST WGT	(21)	cce Al	т	TEMP	WIND	VEL KTS	WIND 137.0	DIREC DEG MAG
43000 LAS	. 43	3200.LBS	27	576 IN	HG	4.0 C	1 1 0	85 W.F	+ 2	
		. 5 6 1 5	750	TDAV			FAR W	STA	NDARD D	AY
			OTOT ST	KE O	FBR	"UBR	EBR	KTAS 145.0	DIST	40 02
TOD	ACCEL (SND-SPU	2866.	39.46	4173.	.169	•05	145.0	2907	37-69
23791.45	-1.01	143.6	2674	37.16	8610.	3150	1.61	140.7	2479.	31.00
23792.25		133.1	2444	33.87	11039	.391	3.94	134.3 127.2	2257	
23793.25		10/ 0	2225	30.37	11217.		6.42	121.0	2046	27.85
23794.25	11.15	110 0	2018	.27 .46.	11612.		8.70	114.0	1847	24.74
23795.25			1001	24-40	11949.	.374		107.5	1659	22.01
23797.25		1011	1436	21.71	12312	400	13.23 15.36	100.8	1482.	19.36
23798.25	10.85	99.9	1462	19.09	15505.	C. 4373		94.6	1317.	17.04
23799.25	11.61	03 8	1299.	16.81	13580	(4440		86.8	1160.	14.33
23800:25		.86.0	1145.	14.14		477	22:47	76.7	879.	11.19
23802.25	-10.02	76.0	868.	11.04	12211.	.377	23.94	72 71 1 3	754	9.61
23803.25	-9.69	70.4	745.	9.49	11973	.393	25.34	64.9	639.	8.01
23804.25	-10.20	64.3		7.91		.393	26.65	58.7	534.	6.57
23805.25	-9.95		527	6.49	12/10.	356	77 71	53.5	440.	5.45
23806.25	-8.89		434.	5.38	11436.	387	28.72	47.5	354.	4.30
23807.25	9.35		350.	2 36	12202.	.375	29.60	42.2	277	3.40
23808.25	-9.14	41.9	2/4.	3.36	9188	.289	30,28	37.0	210.	2.61
23809.25	-6.93	36.7		2.58			30.59			2.18
23810.25	-3.55	33.6	149.	2010		н.	Y	11,52 199 14	part of w	at a will be
	-								4 >- } >	- A - 1. " "
- 11 to 11 to 12							JOON DIE	LILL A V		
TEST NO.	15A	MARK	A III	ITISKID/	STANDAR	D TIRES	JORY RUI	NWAY		
TEST NO.		. 1		1 4					WIND	DIREC
TEST NO.	iΤ	TEST WGT	r F	RESS A	LT	TEMP	WIN	D VEL	WIND 300-0	DIREC DEG MAG
	Ť	. 1	r F	1 4	LT		WIN	D VEL 5 KTS	300.0	DEG MAG
STAND WG	T	TEST WG1 38875.LBS	r F	RESS A	LT I HG	TEMP 10.0 C	WIN 1.	D VEL 5 KTS	300.0 Andard	DEG MAG
STAND WG 38000.LBS	T	TEST WG1	r F 5 27	PRESS A	LT I HG	TEMP 10.0 C	WIN 1.	D VEL 5 KTS ST KTAS	300.0 ANDARD DIST	DAY
STAND WG 38000.LBS	ACCEL	TEST WGT 38875.LBS	F 27	PRESS A 7.616 IN EST DAY-	LT I HG FBR	TEMP 10.0 C	EBR .02	D VEL 5 KTS ST KTAS 137.3	300.0 ANDARD DIST 2699	DEG MAG DAY KE 31.71
STAND WG 38000.LBS	ACCEL -5.59	TEST WG1 38875.LBS GND-SPD 138.9	7 27 TE DIST 2924•	PRESS A 7.616 IN EST DAY- KE 33.19	FBR	TEMP 10.0 C UBR .087	EBR •02 •76	D VEL 5 KTS ST KTAS 137.3 134.1	300.0 ANDARD DIST 2699 2523	DEG MAG DAY KE 31.71 30.27
TOD 28256.21 28257.00	ACCEL -5.59 -7.07	TEST WG1 38875.LBS GND-SPD 138.9 135.7	DIST 2924. 2641.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69	FBR 1941-	TEMP 10.0 C UBR .087 .176	EBR •02 •76 1•90	D VEL 5 KTS ST KTAS 137.3 134.1 129.8	300.0 ANDARD DIST 2699. 2523. 2307.	DEG MAG DAY KE 31.71 30.27 28.34
TOD 28256.21 28258.00	ACCEL -5.59 -7.07 -8.18	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3	DIST 2924. 2641. 2415.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67	FBR	TEMP 10.0 C UBR .087 .176 .220	EBR •02 •76 1•90 3•45	D VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5	300.0 ANDARD DIST 2699. 2523. 2307. 2099.	DAY KE 31.71 30.27 28.34 26.08
TOD 28256.21 28257.00 28258.00 28259.00	ACCEL -5.59 -7.07 -8.18 -9.64	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3 126.0	DIST 2824. 2641. 2415. 2198.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31	FBR 1941- 3996- 5853-	UBR .087 .176 .220	EBR •02 •76 1•90 3•45 5•28	D VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5	300.0 ANDARD DIST 2699: 2523: 2307: 2099: 1900:	DAY KE 31.71 30.27 28.34 26.08 23.62
TOD 28256.21 28257.00 28258.00 28259.00 28260.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3 126.0 119.9	DIST 2824. 2641. 2415. 2198. 1990.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74	FBR 1941. 3996. 5853. 7902.	UBR .087 .176 .220 .301	EBR •02 •76 1.90 3.45 5.28 7.34	D VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28261.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4	DIST 2824. 2641. 2415. 2198. 1990. 1793.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11	FBR 1941. 3996. 5853. 7902. 9526.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414	EBR •02 •76 1•90 3•45 5•28 7•34 9•40	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28261.00 28262.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38	TEST WG138875.LBS GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608.	PRESS A 7.616 IN KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49	FBR 1941. 3996. 5853. 7902. 9526. 11239.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415	EBR .02 .76 1.90 3.45 5.28 7.34 9.40 11.36	D VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28261.00 28262.00 28263.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11204.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419	EBR .02 .76 1.90 3.45 5.28 7.34 9.40 11.36 13.20	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18
TOD 28256.21 28257.00 28258.00 28259.00 28261.00 28262.00 28263.00 28264.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06	TEST WG1 38875.LBS GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271.	PRESS A 7.616 IN KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11204. 11622. 11467.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419 .413	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28260.00 28262.00 28262.00 28263.00 28264.00 28265.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91	FBR 1941- 3996- 5853- 7902- 9526- 11239- 11204- 11622- 11467- 12010- 12514-	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419 .413 .423	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39
TOD 28256.21 28257.00 28258.00 28259.00 28261.00 28262.00 28263.00 28264.00 28265.00 28266.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29	FBR 1941- 3996- 5853- 7902- 9526- 11239- 11204- 11622- 11467- 12010- 12514- 10333-	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419 .413 .423 .448	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83
TOD 28256.21 28257.00 28258.00 28259.00 28261.00 28262.00 28263.00 28264.00 28265.00 28266.00 28266.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06 -11.27 -11.47	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94	FBR 1941- 3996- 5853- 7902- 9526- 11239- 11204- 11622- 11467- 12010- 12514- 10333- 10734-	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .415 .419 .413 .423 .448 .366 .384	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55
TOD 28256.21 28257.00 28259.00 28260.00 28260.00 28262.00 28263.00 28264.00 28266.00 28266.00 28266.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06 -11.27 -11.47 -9.47	GND-SPD 138.7 138.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9	DIST 2924. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 622.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11204. 11622. 11467. 12010. 12514. 10333. 10734.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419 .413 .423 .448 .366 .384	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55 6.27
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28262.00 28262.00 28264.00 28265.00 28266.00 28266.00 28266.00 28266.00 28269.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06 -11.27 -11.47 -9.65 -9.98	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9 62.0 55.8	DIST 2924. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 622. 522.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60 5.36	FBR 1941- 3996- 5853- 7902- 9526- 11204- 11622- 11467- 12010- 12514- 10333- 10734- 11353- 10743-	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .415 .419 .413 .423 .448 .366 .384 .381	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1 55.0	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696. 591.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55 6.27 5.08
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28263.00 28263.00 28265.00 28266.00 28266.00 28266.00 28267.00 28269.00 28269.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06 -11.27 -11.47 -9.47	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9 62.0 55.8	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 622. 522. 432.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60 5.36 4.54	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11204. 11627. 12010. 12514. 10333. 10734. 10734. 9072.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .415 .419 .423 .448 .366 .384 .381 .377	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1 55.0 50.6	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696. 591.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55 6.27 5.08 4.30 3.43
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28263.00 28263.00 28265.00 28266.00 28266.00 28266.00 28267.00 28269.00 28269.00 28269.00 28271.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.06 -11.27 -11.47 -9.65 -9.98 -9.34	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9 62.0 55.8 51.4	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 622. 522. 432. 349.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60 5.36 4.54 3.63	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11622. 11467. 12514. 10333. 10734. 11353. 9072. 11386.	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .415 .419 .413 .423 .448 .366 .384 .381 .377 .310 .396	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1 55.0 50.6 45.2	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696. 591.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55 6.27 5.08 4.30 3.43 2.65
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28261.00 28263.00 28263.00 28265.00 28266.00 28266.00 28267.00 28269.00 28269.00 28271.00 28272.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.47 -9.65 -9.98 -9.34 -7.85	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9 62.0 55.8 51.4 45.9	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 522. 432. 349. 276.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60 5.36 4.54 3.63 2.81	FBR 1941- 3996- 5853- 7902- 9526- 11239- 11622- 11622- 11467- 12010- 12514- 10333- 10734- 11353- 10743- 9072- 11386- 10929	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .415 .419 .423 .448 .366 .384 .381 .377 .310 .396 .382	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1 55.0 50.6	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696. 591. 495.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 14.18 12.25 10.39 8.83 7.55 6.27 5.08 4.30 3.43 2.65 2.02
TOD 28256.21 28257.00 28258.00 28259.00 28260.00 28263.00 28263.00 28265.00 28266.00 28266.00 28266.00 28267.00 28269.00 28269.00 28269.00 28271.00	ACCEL -5.59 -7.07 -8.18 -9.64 -10.60 -11.70 -11.38 -11.44 -11.47 -9.65 -9.98 -9.34 -7.85	GND-SPD 138.9 135.7 131.3 126.0 119.9 113.4 106.4 99.6 93.0 86.4 79.6 73.5 67.9 62.0 55.8 51.4 45.9 40.4 35.3	DIST 2824. 2641. 2415. 2198. 1990. 1793. 1608. 1434. 1271. 1119. 979. 851. 732. 622. 522. 432. 349.	PRESS A 7.616 IN EST DAY- KE 33.19 31.69 29.67 27.31 24.74 22.11 19.49 17.08 14.88 12.86 10.91 9.29 7.94 6.60 5.36 4.54 3.63 2.81	FBR 1941. 3996. 5853. 7902. 9526. 11239. 11204. 11622. 11467. 12010. 12514. 10333. 10734. 11353. 9072. 11386. 10929. 8664	TEMP 10.0 C UBR .087 .176 .220 .301 .364 .414 .415 .419 .413 .423 .448 .366 .384 .381 .377 .310 .396 .382 .294	EBR	VEL 5 KTS ST KTAS 137.3 134.1 129.8 124.5 118.5 112.0 105.1 98.4 91.8 85.3 78.6 72.5 67.0 61.1 55.0 50.6 45.2 39.7	300.0 ANDARD DIST 2699. 2523. 2307. 2099. 1900. 1712. 1534. 1368. 1212. 1067. 933. 810. 696. 591. 495. 410. 331. 261.	DEG MAG DAY KE 31.71 30.27 28.34 26.08 23.62 21.10 18.59 16.29 14.18 12.25 10.39 8.83 7.55 6.27 5.08 4.30 3.43 2.65 2.02

TEST NO. 158	MARK	III ANT	ISKIO/S	STANDAR	TIRES	DRY RUNK	AY		
	TEST WGT			T	TEMP	WIND	VEL		DEG MAG
STAND WST	34450 . L BS		618 IN	HG	10.0 C	3.9	KTS	90.0	DEG THE
340.01233		TE	ST DAY-				STA		YA
	EL GND-SPO	DIST	KE	FBR	UBR	EBR	KTAS	DIST 2572.	24.90
		2529.	24.41	2178.		.05	128.6	2392.	
30558.15 -5.		2350.	23.00	4251.		1.71	124.9	2188 .	
30560.00 -7.		2146.	21.34	4765.		2.79	115.6	1992 .	20.13
30561.00 -8	66 113.5	1951.	19.64	6579		3.97	110.5	1805 .	18.36
30562.00 -8		1764.	17.88	8157.		5.29	105.0	1626 .	
30563.00 -9		1417.	14.24	90 76.		6.75	98.8	1458 .	
30564.00 -10		1259.	12.42	10423.		8.28	92.5	1300 .	
30565.00 -11		1113.	10.52	10831.		11.24	85.3 78.7	1020 .	
30567.00 -11	09 76.4	978.	8.91	105 43.		12.55	72.1	895 •	
30568.00 -11	.39 69.7	855.	7.42	8639		13.65	65.6	784 .	
30569.00 -8	. 87 63.2	743.	5.46	4172		14.20	62.2	679 •	
	.54 59.8 .66 56.6	541.	4.89	7554		14.78	59.0	575 .	
	.66 56.6 .97 51.0	450.	3.97	9100		15.58	53.5	484 .	
	.06 46.2	368.	3.26	8274		16.26	48.7	323 .	
	.66 41.3	294.	2.61	7960		17.11	40.5	263 .	
	.60 38.0	238.	2.21	4769	186		-0.5	1114	

TAND WG		TEST MGT		PRESS / 7.765 IN	ALT N HG	11.0 C	WIND 3:9	VEL KTS		DIREC DEG MAI
			1	EST DAY	,			ST	ANDARD (DAY
TOD		GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
3394.36	-3.48	127.5	5537.	50:05	247.	.00B	.01	130.8	5858	30.28
3395.25	-3.43	125.6	5447.	28.16	247.	•000	.07	128.9	5665.	29:41
3396.25	-4.20	123.3	5236.	27.14	1326.	.049		126.6	5451.	28.37
3397.25	-3.81	121.1	5031.	26.18	984.	.037	.49	124.4	5241.	27.39
3398.25	-3.95		4828.	25.06	1313.	.04B	.78	121.8	5036.	26.25
3399.25	-3.52		4530.	24.10	945.	.034	1.02	119.5	4834 .	25.28
3400.25	-3.14	114.3	4435.	23.34	573.	.020	1.13	117.6	4635.	24.50
3401.25	-4.08	112.2	4243.	22.47	1874.	.065	1.41	115.5	4439.	23.62
3402.25	-3.68	109.9	4056.	21.57	1510.	.053	1.72	113.2	4248.	22.69
3403.25	-3.36		3872.	20.77	1225.	.042	1.95	111.2	4060.	21.88
3404.25	-4.16		3592.	20.01	2339.	.081	2.26	109.2	3875.	21.11
3405.25	-3.72	103.1	3516.	18.99	1957.	.067	2.68	106.4	3696.	20.06
3406.25	-3.90	101.1	3343.	18.26	2288.	.078	3.00	104.4	3519.	19.31
3407.25	-3.98	98.7	3175	17.41	2515.	.085	3:42	102.1	3346	18.45
3408.25	-3.85		3010.	16.66	2493.	.083	3.80	99.9	3177.	17.68
3409.25	-3.93	94.1	2849.	15.81	2800.	.090	4.26	97.4	3013.	16.81
3410.25	-3.77		2692	15.09	2710	.086	4.66	95.3	2851.	16.07
3411.25	-4.58	89.4	2539.	14.28	3844.	.123	5.19	92.8	2693.	15.24
3412.25	-3.57	87.0	2390	13.51	2692	.085	5.66	90.3	2541.	14.45
3413.25	-4.40	85.0	2245	12:89	3823.	.121	6.10	88.3	2391.	13.81
3414.25	-4.13	A2.1	2105	12.03	3610.	.115	6.66	85.4	2247.	12.92
3415.25	-4.46	144.50	1968.	11.33	4125.	.130	7.17	83.0	2105.	12.20
3416.25	-3.64	77.1	1836.	10.61	3197.	.101	7.66	80.4	1969.	11.45
3417.25	-3.75	The same of the sa	1707.	10.06	3403.	.109	8.06	78.4	1835.	10.89
3418.25	-4.78	72.6	1582.	9.41	4798.	.153	8.59	75.9	1705.	10.21
3419.25	-3.25		1463.	8.78	2976.	.093	9.03	73.5	1581.	9.56
3420.25	-3.39		1345.	8.27	3206.	.104	9.41	71.4	1458.	9.03
3421.25	-5.39		1232.	7.84	5791.	•185	9.88	69.6	1339.	8.58
3422.25	-5.11	61.8	1125.	6.82	5591.	.178	10.61	65.1	1230	7.52
3423.25	-3.43		1021.	6.40	3548.	.111	10.99	63.2	1121.	7.08
3424.25	-4.72		922.	5.90	5243.	.164	11.45	60.9	1016.	6.56
3425.25	-4.73		628.	5.34	5335.	168	11.94	58.1	917.	5.97
3426.25	-4.46		738	4.80	5089.	.157	12.41	55.2	823.	5.40
3427.25	-4.28	49.4	553	4.36	4916.	.155	12.81	52.8	732.	4.94
3428.25	-5.13		571.	3.86	6069.	.188	13.27	49.9	645.	4.41
3429.25	-5.15	12 12 12	496.	3.38	6164	.193	13.73	46.9	564	3.89
3430.25	-5.11	40.5	425	2.92	6179.	197	14.16	43.9	489.	3.41
3431.25	-5.95		359	2.46	7313.	230	14.60	40.5	418.	2.90
3432.25	-5.01	Acres de la companya del companya de la companya de la companya del companya de la companya de l	299	2.06	6192.	. 19A	14.99	37.4-	354.	2.47
3433.25	-5.44		245	1.72	6789	.216	15.33	34.5	294	2.10
	-5.50		195	1.33	6936	.219	15.68	30.7	241	1.67
3434.25	-2.50	6,13	1730	1 # 33	02000		15.77	29.0	210.	1.49

MARK III ANTISKID/REG TIRES/WET RUNWAY

TEST NO. 178

STAND WG	т	TEST WGT	D,	RESS AL	T	TEMP	WINE	VEL		DIREC
36000 LBS		6200 LBS		.775 IN		2 • 0 C		KTS	3.0	DEG MAG
•				OT 0.01				STA	NDARD I)ΔΥ
				KE	FBR	UBR	EBR	KTAS	DIST	::KE
TOD		GND-SPD	DIST		60.			129.5	-	26.71
25866.60	-3.73	126.6	5596 • :	24.69	1339	.055		127.0	5605.	25.70
25867.50	-4.57	124.1	5405	23.81		0.000	.31	124.8	5395.	24.81
25868.50	-2.96	121.9	5198	23.01	731.	.030		122.7	5186.	23.99
25869.50	-3.89	119.8	4993.	22.25	-103	.004	.45	120.7	4982.	23.22
25870.50	-3.24	117.8	. 4793.	21.35	983.	039	.61	118.3	4782.	22.30
25871.50	-3.88	115.4	4590.	20.74	69.	.003	.65	116.6		21.67
25872.50	-2.98	113.8	4402. 4212.	19.89	1337.	.053			4390.	20.81
25873.50	-3.98	111.4		10 00	777	.030	1.00		4200 .	20.13
25874.50	-3.34	109.5	4026.		. 957.	.038	1.20			19.29
25875.50	-3.42	107.2	3943.	18.40 17.75	1438.	.056	1.41	108.1		18.64
25876.50	-3.75	105.3	3563.		1045	.041	.1.62	106.0		17.91
25877.50	-3.31	103.1	3488.	17.05	1575.	.061	1.87	103.8	3473.	17.17
25878.50	-3.68	100.9	3315.	16.32	1895.	.076	2.14	101.8	3300 •	16.53
25879.50	-3.87	99.0		15.69	,	.083	2.50	99.4	3131 -	15.74
25880.50	-3.95	96.5	2982	14.92	2043.	075	2.85	97.1		. 15.02
25881.50	-3.69	94.2	2821.	14.22	2705.	098	3.21		2805.	-14.38
25882.50	-4.18	92.1	2555.	13.60	2562	043	3.66	92.1		13.51
25883.50	3.93	89.2	2512.	12.74	•		4 675		2495	12.90
25884.50	-4.31	87.1	2362.	12.15	3075	138	4.59	87.1	2347.	
25885.50	-4.85	84.2	2217.	11.36	3819.	·178	5.07	84.4		11.35
25886.50	-4.23	81.5	2075.	10.64	3239•	.125	5.52		2065	10.69
25887.50	-4.33	79.0	1943.	10.00	3455	•121	5.98	79.3	1930.	10.02
25888.50	-4.16	76.4	1311.	9.35	3372.	-121	6.39	76.9	1799.	9.42
25889.50	-3.85	74.0	1585.	8.77	3128. 3649.	.129	6.81	74.5	1671.	8.85
25890.50	-4.24	71.5	1561.	F . 22	3793.	.135	7.25	72.0	1548	8.26
25891.50	-4.29	69.1	1443.	7.55		124	7.68	69.5	1430 .	7.69
25892.50	-3.97	66.6	1328.	7.10	3524	.128	8.05	67.3	1315.	7.22
25893.50	-3.97	64.4	1218.	6.54	3591. 3713.	1.35	8.45		1204.	6.68
25894.50	-4.01	61.8	1111.		3715.	1.33	8.83	62.4	1096.	6.20
25895.50	-3.94	59.5	1009.	5.67	4824	.176	9.24	60.0	993.	5.74
25896.50	-4.87	57.1	910.	5.23	5517.	203	9.75	56.7	896.	5.12
25897.50	-5.40	53.8	316.	4.63	-5332•	192	10.20	53.9	804.	4.62
25898.50	-5.16	50.9	729.	4.15	5233.	189	10.65	50.5	717.	4.06
25899.50	-4.99	47.5	546	- 3.62	5102.	182	11.04	47.8	634.	3.64
25900.50	-4.81	44.8	567.	3.22	4868	.172	11.39	45.1	557.	3.24
25901.50	-4.54	42.1	494.	2.84	6107.	.214	11.77	42.1	484.	_
25902.50	-5.58	39.2	425.	2.46	4849.	.172	12.11	38.7	. 417.	
25903.50	-4.40	35.8	362	2.05	5925		12.41	36.4	352	
25904.50	-5.31	33.4	303.	1.79	6312.	.221	12.73	33.2	295.	
25905.50	-5.60	30.2	249.	1.46	5912	.211	13.02	29.8	244.	
25906.50	-5.20	26.8	202.	1.15	3932	.140	13.20	27.1	196.	
25907.50	-3.40	24.1	159.	•93	3666	.130	13.20	26.9	191.	
25907.60	-3.16	23.9	155.	. 92	• 1100C.	• LJU	130.0	-017		

TEST NO. 18A	MA	RK III AN	TISKID/BFG	TIRES/WE	F RUNWAY	-		The state of the s
	TECT WET	000	SS ALT	TEMP	UNIW	VEL		DIREC
STAND WGT	TEST WGT 42850.LBS		04 IN HG			KTS	75.0	DEG MAG
43000.LBS							AUGINDO D	
		TEST	DAY		500		NDAPD D	KE.
TOD ACC	EL GND-SPD	ו בנעי	VE : LOW	CM3 PF	LDIN	146.8		41.02
31980.95 -4.	47 139.1					144.3	6757	
31981.75 -4.	38 136.6	200	5.39 336		·	142.3		
31982.75 -3.				. 0.000	.17	139.6		37.08
31983.75 -4.	30 131.8 %	_,		• ~ •025	37	137.3	6042	_
31984.75 -3.			1.84 234	-		135.0		_
31985.75 -4.			0.73 821		69	132.6		33.48
31986.75 -4.			9.57 1140		92		5362	32.24
31987.75 4.	_	4770 - 2	8.41 - 1115	069	1.19	127.9		
31988.75 -4.			7.38 1851	055			4932	29.82
31989.75 -4.					-1.87	122.7	4722	28.66
31990.75 -4.				- 058			4514.	27.76
31991.75 -4.			4.20 1639 2.96 1935		2.53			26.43
31992.75 -4.			2.12 2375		2.86	115.8	4115.	@ 25.52
	28 - 108.0		0.91 2651		3.39	112.8		24.22
• • • • • • • • • • • • • • • • • • • •	27 105.0	-	0.07 2762		3.80	110.7	3734.	23.32
31995.75 -4.			9.00 2256		4.28	107.9	3551 •	22.17
31996.75 -3.		2911. 1		•	4 . 65	106.0	3367.	21.38
31997.75 -4.		2748. : 1	7.29. 3736		-5.22 -	103.3	3191	20.32
31998 75 -4		: 2589 - 1	6.28. 3052	_	5.77	100.5	3019.	19.22
31999.75 -4.	-		5.56 3094		6.20	98.4	2849.	18.44
32000.75 -3.	96 88.0		4.69 4552		6.79		72684.	
32001.75 -4. 32002.75 -4.			3.71 3590		7.39	92.9		16.43
32003.75 -4.			2.99 3830	116	7.89	90.6	2369.	15.64
32004.75 -4			2.18 3976	119	8.44		. 2218.	14.75
32005.75 -3			1.48 3688	1109	8,94	85.7	2070•	13.97
32006.754.		1596. 1	0.76 4788	. 143	9.48	83.2	1926.	13.19
32007.75 -4			9.91 5254		10.13	80.2		12.24
32008.75 -4		1352.	9.17 4746		10.71	77.5	1655.	11.42
32009.75 -3.		1237.	8.52 416		11.21	74.9	1525	10.69
32010.75 -4	_	1125.	7.93 522		11.72	72.6	1398	10.03 9.21
32011.75 -4			7.20 5496	•165	12.30	69.6	1279. 1162.	8.55
32012.75 -4	15 59.1	917.	6.62 465		12.79	67.0	1049	7.89
32013.75 -5	44 56.4	819.	6.04 6450		13.33	64.4	946.	7.03
32014.75 -5	25 52.8		5.29 632		13.96	60.8 58.2	845.	6.44
32015.75 -4			4.78 4956		14.41	, 55.4	746•	5.85
32016.75 +4		558.	4.27 560		14.85 15.37	52.6	653	5.27
32017.75 -6.		480.	3.78 7798			48.5	572	4.48
32018.75 - 5.		408 •	3.11 681		16.26	46.4	487.	4.09
32019.75 -4		342.	2.79 5287		16.69	42.9	411.	_
0_0_0	.02 34.9	28ů.	2.31 781° 1.91 720°		17.09	39.7	340.	
32021.75 -5		223.			17.49	36.1	276.	
0_0000	.44 28.1	173.			17.71	33.0	216.	
32023 • 75 - 3	.04 24.9	128.	1.18 404					

TEST NO. 1	183	МДН	₹K III	ANTISKI	D/8FG 11	TRES/WE	T RUNWAY			
STAND WGT		TEST WGT 7875.LBS		RESS A	LT HG	TEMP	WIND 6.5	VEL KTS		DIREC DEG MAG
			- 3.55	CT DAV.				STA	ANDARD D)AY
-	40051			SI DATE	FBR	068	EBR	KTAS	DIST	KE
TOD		GND-SPD	01ST = 5592•	29.23	205.	.015 -	.00		6132.	31.68
34456.18	-4.49	132.0	5511.	28.37		0.000	.02		5943.	30.80
34457.00	-3.64	130.1	5294		356.	.017			5716.	29.83
34458.00		127.9	5080.	26.23	835.	037	.25	130.3	5495.	28.56
34459.00	-4.30	125.1	4570.	25.29	583.	.026	.36	128.0	5276.	27.58
34460.00	-4.01		4565.	24.30	504.	026	.50	125.6	5062.	26.55
34461.00	-3.84	120.4		23.56		0.000	.52	123.8	4850.	25.78
34462.00	-3:05	118.5	4463. 4265.	22.74	1151.	.047	-64	121.7	4641.	24.92
34463.00	-4.07	116.5		21.84	1197.	049	-80		4437	23.98
34464.00	-4.02	114.1	4071.	20.81	1555.	064	1.17	116.7	4239.	22.90
34465.00	-4.21	111.4	3880.	20.02	1647	.066	1.40	114.6	4042.	22.08
34466.00	-4.16	109.3	3694.	18.96	2128.	.084	1.82	111.6	3852	20.97
34467.00	-4.42	106.4	3511.	18.34	1497.	.056	2.04	109.9	3664.	20.32
34468.00	-3.76	104.6	3334. 3160.	17.31	2465.	092	2.47	106.9	3482.	19.23
34469.00	-4.43	101.6		16.49	2198	.081		104.5	3303.	18.37
34470.00	-4.07	94.2	2990.	15.70	2898.	.105	3.26	102.1		17.53
34471.00	-4.54	96.8	2825.	14.84	2379.	084	3.69	99.4		16.63
34472.00	-3.97	94.1	2664	14.14	3363.	.118	4.10	97.2	2791.	15.88
34473.00	-4.68	91.8	2507. 2355.	13.17		.131	4.70	94.0	2632.	14.86
34474.00	-4.92	88.6			3648	.124	5.21	91.4	2475.	14.06
34475.00	-4.65	86.1	2207.	12.42		-120	5.74	88.6	2324.	13.19
34476.00	-4.45	83.2	2064	11.60	3533.	.134	6.26	85.9	2177.	12.42
34477.00	-4.72	80.6	1926.	10.88	3967• 3392•	.114	6.76	83.2	2036.	11.65
34478.00		77.8	1793.	10.15 9.46	4694	.160	7.29	80.5	1897.	10.91
34479.00	-5.14	75.1	1564.	8.67	4354.	.147	7.88	. 77.3	1765.	10.06
34480.00	-4.74	71.9	1539.	8.11	3610.	.121	8.32	75.0	1636.	9.45
34481.00	-4.03	69.5	1420.	7.58	3112.	.105	8.70	72.7	1511.	8.88
34482.00	-3.54	67.2	1305. 1193.	7.06	4335	150	9.12	70.3	1388.	8.32
34483.00	-4.52	64.9	1066.	6.48	4317.	.146	9.60	67.5	1272.	769
34484.00	-4.42	62.2		5.93	4524	.152	10.06	64.9	1160.	7.09
34485.00	-4.52		. 983. 885.	5.44	4315	.147	10.48	62.4	1052.	6.56
34486.00	-4.28	57.0	791.	4.88	5309.		10.96	59.4	949.	5.94
34487.00	-5.05	54.0	702.	4.41	4274.		11.37	56.8	850.	5.42
34488.00	-4-10	51.3		3.49	5020.		11.76	54.3	755.	4.95
34489.00	-4.67	48.6 6.0	518.	3.52	5626		12.19	51.3	666.	4.43
34490.00	-5,12	+5•8 (0.0	538 •	3.07	5415		12.60	48.3	581.	3.93
34491.00	-4.88	42.8	463.	2.66	6144.		13.00	45.4	502.	3.46
34492.00	-5.44	39.9	393.	2.23	6046		13.39	42.0	429.	2.96
34493.00	-5.28	36.4	329.	1.88	5760		13.73	39.1	360.	2.57
34494.00	-4.99	33.5	270.	1.56	6501.		14.05	36.0	295	2.18
34495.00	-5.57	30.5	216.	1.22	7421.		14.39	32.5	238	1.78
34496.00	-6.30	26.9	168.	.92	4176.		14.61	29.0	186.	1.42
34497.00	-3.49	23.4	125.	.91	3726.		14.61	28.8	181.	1.40
34497.11	-3.10	23.2	121.	• 71	.,,,,,,,,	-120	A 7 V C) A	-540		

TEST NO. 1	ac	MAF	K III A	NTISKID	/AFG TIR	ES/WET	KUNWAT			
1521 MO. 1	,,C						WIND	VFI	WIND	DIREC
STAND HGT	1	EST WGT		ESS AL		EMP	9.6	KIS	50.0	DEG MAG
34000 LRS		550.LBS	27.	alo IN	nG 16	.5 C	7.0			
34000 LD3								STA	NDARD D	AY
_				T DAY		UMR	ERR	KTAS	DIST	KE
TOD	ACCEL G	GND-SPU	DIST	K€ .	FAR	.038	01	116.0	4012.	20.25
	-3.90	108.1	3583.	17.66	823.	.046	.16	114.3	3988.	19.65
36090.00	-3.98	106.3	3463.	17.28	1061.	.005	.23	112.4	3699.	19.00
36091.00	-3.02	164.4	3256.	16.06	115.	.048	.34	110.5	3512.	18.36
36092.00	-3.94	102.4	3111 •	16.05	1097	.060	.63	108.0	3332.	17.55
36093.00	-4.42	99.4	2940.	15.28	1454	.064	.90	105.4	3157.	16.74
36094.00	-3.92	97.4	2774.	14.50	1468	.107	1.23	103.0	2985.	15.97
36095.00	-4.74	94.9	2511.	13.77	2497.	.128	1.69	100-1	2820.	15.08
36096.00	-5.13	91.9	2453.	12.93	3126	.095	2.11	97.2	2660.	14.23
36097.00	-4.26	89.0	2301.	12.12	2368.		2.50	94.8	2501.	13.51
36098.00	-4.83	86.5	2152.	11.45	3114.	.123	2.96	91.8	2350.	12.68
36099.00	-4.50	83.5	2009.	10.56	2913.	.113	3.31	89.4	2200.	12.04
36100.00	-4.07	81.1	1870 .	16.07	2570.	.100	3.72	86.8	2054.	11.35
36101.00	-4.61	78.5	1735.	9.42	3263.		4.12	84.2	1914.	10.68
36102.00	-4.30	75.9	1506.	8.40	3041.	.117	4.58	81.4	1778.	9.98
36103.00	-5.03	73.0	1479.	8.15	3972.	.149	5.00	78.5	1647.	
36104.00	-5.07	70.1	1359.	્?•∋1	4126.	.150	5.51	75.7	1521 .	8.62
36105.00	-4.58	67.2	1243.	6.90	3724.	.140	5.93	73.0	1399.	8.02
	-4.64	64.5	1132.	6.35	3881.	.147	6.32	70.4	1280.	
36106.00	-4.43	61.8	1025.	5.85	3747.	.142		67.6	1166.	
36107.00.	-5.51	59.0	923.	5.32	5010.	.147	6.77	64.4	1060.	7
36108.00	-4.96	55.7	526.	4.75	4531.	.169	7.23	61.6	955.	
36109.00	-4.81	52.9	734.	4.28	4454.	.167	7.63	58.8	856	
36110.00	-5.37	50.1	543.	3.84	5146.	.191	8.05	55.3	765	
36111.00	-5.20	46.5	566.	3.31	5063.	.192	8.47	52.6	675	
36112.00	-5.09	43.8	489.	2.43	5015.	.192	8.84	49.5	592	
36113.00	-5.27	40.6	418.	2.53	5287.	.204	9.20	46.3	513	
36114.00	-5,47	37.4	352.	2.14	5593.	.510	9.55	43.1	440	
36115.00	-5.78		292.	1.79	5999•	.556	9.90	39.9	373	
36116.00	-5.42		237.	1.46	5680.	.217	10.20	36.5	312	
36117.00	-5.93		189.	1.16	6299•	.530	10.49	33.2	256	
36118.00	-5.44		144.	.89	5839.	.551	10.75	30.0	203	
36119.00	-4.23		166.	•67	4606•	.170	10.95	29.2	186	
36120.00	-2.95		95		3244 •	.120	10.96	29.6		
36120.34	-2,73	C DAT								

TEST NO.	19A	MARK	II A	NT ISK 10/	STANDAR	D TIRES	DRY RUN	YAY		
STAND H	T	TEST WGT		PRESS A	LT	TEMP	WIND	VEL.	WIND	DIREC
40 00 0 . L B	3	40 800 . L 85	2	7.500 IN	HG	15.8 C	4.3	KTS	237.0	DEG MAG
			T	EST DAY-				ST	ANDARD	DAY
TOO	ACCEL	GND-SPO	DIST	KE	FBR	UBR	E BR	KTAS	DIS	
23465.08	-5.51	140.7	2930.	35.73	2468.	.095	.10	133.8	2612 .	31.70
23466.00	-8.05	136.9	2714.	33.87	5981.	.231	1.10	130.2	2415 .	30.00
23467.00	-9.50	131.7	2487.	31.34	8399.	.296	2.80	125.1	2209 .	27.69
23468.00	-10.32	125.9	2269.	28.64	9770.	.345	4.79	119.4	2009 .	25.23
23469.00	-10.82	119.5	2062.	25.79	107 47.	.375	6.95	113.1	1820 .	22.63
23470.00	-9.55		1866.	23.21	9466.	.330	8.90	107.0	1641 .	20.29
23471.00	-9.51	107.9	1679.	21.01	3687.	.336	10.65	101.7	1471 .	18.30
23472.00	-10.23	101.8	1502.	18.72	10879.	.371	12.50	95.7	1310 .	16.22
23473.00	-10.27	95.8	1335.	16.59	11206.	.382	14.32	89.9	1159 .	14.30
23474.00	-9.53	89.8	1179.	14.58	13514.	.361	16.00	84.0	1017 .	12.49
23475.00	-9,94	84.3	1032.	12.85	11249.	.384	17.56	78.6	885 .	10.94
23476.00	-9.83	78.1	895.	11.03	11339.	.389	19.12	72.5	762 .	9.31
23477.00	-9.35	72.7	767.	9.53	10942.	.352	20.48	67.1	648 .	7.98
23478.00	-9.65	67.0	649.	8.10	11502.	.373	21.79	61.6	543 .	
23479.00	-9.74	61.3	541.	6.79	11770.	.392	23.02	56.0	448 .	5.56
23480.00	-9.73	55.6	443.	5.58	11909.	.396	24.15	50.4	361 .	4.50
23481.00	-9.99	49.5	35 4.	4.43	12388.	.414	25.23	44.4	283 .	3.50
23482.00	-7.46		276.	3.54	92 87.	.316	26.93	39.3	215 .	2.74
23483.00	-6.59	40.0	204.	2.89	8288.	.270	26.65	35.1	157 .	2.18
23483.53	-4.82	38.1	170.	2.62	6081.	.198	26.78	33.3	129 .	1.96

TEST NO	. 21A	MA	PK III	ANTISKI	VUSAF T	IKESZWE	ET RUNWA	Υ		
		TEST WGT	Pi	RESS AL	7	TEMP	WIND			DIREC
STAND 40000.L		39800 LBS		.649 IN		6.6 C	1.1	KTS	315.0	DEG MAG
400000	.,,,							Lallet	ANDARD D	AY
			TE	ST DAY-			FBR	KTAS	DIST	KE
TOD	ACCE	L GND-5PD	DIST	KE	FAR			147.2	7396.	38.37
24615.0	6 -3.6	3 145.5	7189.	37.29	0.	0.000	0.00	145.3	7161.	37.40
24616.0	0 -3.7	8 143.6	6960.	36.35		0.000	0.00	142.5	6914	35.95
24617.0	0 -5.1	6 140.8		34.94	1345				6671.	
24618.0	0 -3.6	3 138.2	6484 •	33.65		0.000	. 58	137.8	6433	33.60
24619.0		0 136.1	6252.	32.66	151.	.006	-59	135.5	6199•	
24620.0	0 -3.7	6 133.9	6025	31.60	83.	-003	.30 .38	132.9	5968	31.29
24621.0	0 -3.8	5 131.4	5900.	30.41	390	6016	2 M	131.0	5742	30.38
24622.0	0 -4.2	8 129.4	5580.	29.52	1048.	• 94%	.40	128.4	5520	29.21
24623.0	0 -3.4	7 126.9	5365.	2B ± 34	224	.009	•63	126.3	5301.	28.23
24624.0	_	1 124.8	5151.	27.43	1Hol.	.074	.83		5087	26.97
24625.0		7 122.0	4944.	26.21	558	- 021	1.13	123.4	4877.	
24626.0			4739.	25.48	1072.	.040	1.22	121.7	4671	25.03
24627.0			4539.	24.32	2420.		1.65	118.9		. 23.88
24628.0	_		4343.	23.20	1135.	.041	2.01	116.1.	4271.	
24629.0			4150.	22.47	1527.		5.21	114.3	4077	
24630.0		8 110.5	3962.	21.53	2549	.085	2.63	109.4	3888	
24631.0		6 108.1	3778.	50.60	1562.	.053	2.97	106.9	3701	20.25
24632.0	_		3597.	19.67	2775.	.091	3.40	100.9	3519.	
24633.0		8 ,103.6	3420 •	18.90	2593.	- ₹086	3.82	104.8	3342	
24634.0			3248 .	17.93	2421.	.080	4.29	TACHT	3168	17.72
24635.0			3079.	17.22	2380.		4.66	100-0	2999	16.99
24636.0			2914.	16.51	5585	.073	5.03	.98•0 95•5	2832	16.14
24637.0	_		2752.	15•68	3432.		5.52		2671	
24638.0			2595.	14.89	2933.	.096	6.01	93.0 90.6	251.3	
24639.0		89.5	2442.	14.11	4222•	.137	6.56	87.6	2361	
24640.0		86.6	2294•	13.21	3102.		7.12		2212.	- /
24641.0		0 84.7	2149.	12.65	3002.		7.51	85.8	2067	
24642.0		2 81.9	2008.	11.83	4267.		8.08	82.9 80.5	1927	
24643.0		9 79.6	1872.	11.16	2967.		8.54		1790	
24644.0		3 77.4	1739.	10.56	3903.		8.99	78.4	1658	
24645.0			1511.	9.89	4170.		9.51	75.8	1530	
24646.0	_	72.4	1486.	9.23	4477.		10.05	73.3	1408.	
24647.0			1367.	8.57	4376.		10.57	70.6	1288.	
24648			1251.	7.87	5260.		11.15	67.7	1175	. 7:46
24649		_	1141.	7.25	4399.		11.67	64.9	1066.	
24650			1035.	6.70	5187.	_	12.18	62.4 59.2	962	
24651.		16 58.5	934.	6.03	4525		12.69			_
24652		_	836.	5.55	580H.		13.17	56.8	767	
24653			744.	4.96	-5311.		13.69	53.7		4.62
24654	00 -4-8		557.	4.49	5574.		14.14	51.1	-592	
24655			575.	3.98	5733•		14.60	48.1	511.	
24656		_	496.	3.47	6587.	_	15.08	44.9	437.	
24657			424.	2.99	6716.		15.55	41.7	369.	
24658	- "		358.	2.51	6895.		16.00	38.2		
24659	_		297.	2.12	6227		16.38	35.1	306.	
24660			241.	1.71	7616		16.77	31.6	248	
24661.			191.	1.36	7127.			28.1	197	_
24662	-		147.	1.06	4891		17.37	24.8	152	
24662			141.	1.04	4211	.135	17.37	24.6	145.	1.07

STAND WG		EST WGT		.662 IN		TENF 9.8 C		VEL KTS	0.2SS	DIREC DEG MAG
34000.LRS	34	100V = L 27	ζ,	•(10%)14						
				ST DAY					INDARD D	
TOD	ACCEL 6		DIST	KF	FBR	UBP	EBR	KTAS	DIST	KE KE
27363.05	-3.79	131.8	5571.	26.55	0.	0.000	0.00	129.5	5304.	25.23
27364.00	-4.08	124.7	5361.	25.73	240.	.012	• n 1	127.4	5102.	24.44
27365.00	-4.28	127.1	5145.	24.70	711·	.1134	.15	124.8	4894.	23.45
27366.00	-3.66	124.7	4932.	23.79	143.	• (11) 7	.23	122.5	4690.	22.57
27367.00	-4.50	122.5	47:24 .	22.95	1180.	• (155	.37	120.3	4489.	21.77
27368.00	-4.53	114,4	4520.	21.81	[449.	•055	.70	117.2	4292.	20.67
27369.00	-4.13	117.1	4320.	20.96	1150.	.052	.93	114.8	4100.	19.85
27370.00	-3.91	114.7	4124.	20.11	1066.	.047	1.14	112.5	3913.	19.04
27371.00		112.1	3933.	19.23	1781.	.075	1.43	109.9	3724.	18.19
27372.00	-4.52	109.5	3745.	18.33	2150.	.0KR	1.61	107:3	3548.	17.33
27373.00		105.7	3563.	17.42	2467.	.099	2.24	104.6	3373.	16.45
27374.00	-4.38	104.2	3385.	16.60	2324.	.091	2.66	102.0	3202.	15.67
	-3.98	101.6	3212.	15.79	2029.	.079	3.04	99.5	3036.	14.89
27375.00	-4.09	99.2	3042.	15.05	2272.	.087	3.40	97.1	2873.	14.18
27376.00	-4.25	96.8	2875.	14.33	2555.	.099	3.80	94.7	2715.	13.49
27377.00		_	2715.	13.54	3294.	.129	4.29	92.0	2560 •	12.73
27378.00	-4.84	94.1	2559	12.31	2931	114	4.74	89.4	2410.	12.03
27379.00	-4.38	91.5	2406.	11.95	4232	.163	5.32	86.3	2264.	11.21
27380.00	-5.46	88.4		11.27	2420.	.092	5.77	83.8	2124.	10.56
27381.00	-3.67	85.8	2260.	10.71	3040	1115	6.15	81.6	1988.	10.02
27382.00	-4.16	83.7		10.06	3013.	.113	6.58	79.1	1855.	9.41
27383.00	-4.04	81.1	1979.		3251.	.124	7.02	76.4	1727.	8.79
27384.00	-4.17	74.5	1844.	9.42	3345.	126	7.44	74.1	1602.	8.26
27385.00	-4.17	76.1	1713.	₽.86 0.34	-	.164	7.94	71.4	1482.	7.67
27386.00	-5.06	73.4	1586.	8.24	4401.	.139	8.43	68.4	1366	7.05
27387.00	-4.29	70.4	1465.	7.59	3672. 3556.	134	8.42	66.3	1255.	6.61
27388.00	-4.11	68.3	1348.	7.13		.137	9.25	63.5	1148.	6.08
27389.00	-4.09	65.5	1235.	6.57	3624 • 4719 •	.179	9.67	61.3	1044.	5.66
27390.00	-5.05	63.3	1126.	6.12	4873.	184	10.21	57.9	945.	5.04
27391.00	-5.09	59.8	1022.	5.47		.163	10.61	55.5	852	4.63
27392.00	-4.48	57.4	924.	5.05	4520.	.171	11.04	52.5	763.	4.15
27393.00	-4.62	54.4	930.	4.53			11.49	49.4	678.	3.68
27394.00	-5.53	51.3	740.	4.03	5575 ·	.213	12.04	45.7	579.	3.14
27395.25	-4.95	47.6	535 •	3.46	5056	188		42.8	506.	2.76
27396.25	-5.06	44.7	557.	3.06	5233•	-198	12.44	40.0	438	2.40
27397.25	-5.13	41.8	465.	2.68	5372	.203	12.81		374	1.99
27398.25	-5.43	38.2	417.	2.23	5774.	.217	13.21	36.4	316.	1.72
27399.25	-4.81	35.7	355.	- 1.95	5155.	•194	13.51	33.8		1.39
27400.25	-5.44	32.2	298.	1.59	5889.	•223	13.84	30.4	263.	1.14
27401.25	-5.30	29.4	245.	1.32	5789	219	14.13	27.6	214.	•88
27402.25	-5.26	26.0	199.	1.03	5800.	.218	14.40	24.1	171.	
27402.60	-4.32	24.9	184.	.94	4809.	.179	14.42	23.1	157•	-80
	·									

TEST NO. 2	224			ANTISKI						
STAND WG	T	TEST WGT	. 2	PRESS AL	LT HG	TEMP	WIND 1.7	VEL KTS	WIND 32.0	DIREC DEG MAG
			T	FST DAY-				STA	NUARD I)AY
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBR	EBK	NIAS	DIST	I V Em
25545.30				37.10	·	0.000	~~ 0 . 00	141.3	6488.	
25546 • 25 -			6126.	36.01	48.	.002	•00	139.2	6264.	36.88
25547.25	-4:29	134:8			1060.	039	.19	136.7	6031-	
25548.25	-3-21	132.6	5571.	33.65	0.	0.000	.24	134.6	5802.	
25549-25	-4-25	130-4	-5448	- 32.52	1299	-047	- 41	-132.4		33.35
25550.25	-3.61		5230.	31.40	623.	.022	•59	130.1	5356.	32.22
25551-25			5016.		1713.	.059	- 85	127.9		
25552.25	-4.10		4506.	29.07	1618.	.055	1.22	125.2	4926	
25553.25		120.9			1865.	062	1.57	122.8		
25554.25	-4.76		4398.		2889.		2.09	120.1	4513.	27.48
25555.25			4201.	25.52	2068.	063	2.57	117.4	4313.	_
25556.25	-4.06		4008.		2405.		2.96	115.3	4117.	
25557.25			3818.		2818.	.085	3.49	112.7	3924	24.18
25558.25	-4.39		3533.		3135.	.095	4.01.	110.3	37,37	23.15
25559.25	-4.54		3452.	- '	3493	-104	4.64	107.4	3553	21.97
25560.25	-3.94	103.2	3277-	20.37	2827.	.083	5.15	105.1	3375	
		100.6	31052	19.36	- 3799	112	5.74-	-102.5	3200.	20.01
25562.25	-3.62		2937.		2640.	.078	6.27	100.0	3030.	19.02
25502.65 55568.35-	-4 ·70	95.9	2777	17.59	4187	125	6.81	97.8	2862.	18.21
25564.25	-4.08	93.1	2614.	16-57	3487.	-104	7.44	95.0	2701.	17.17
25565-25			-2458	15.77	4040	120-	8-00	92.7	2542.	-16.35
			2244	14 00	4.600	1 22	9.67	80.8	2389.	15.37
25566.25		85.5	2162	13.97	3158		9.21	87.3	2240.	14.52
25568.25	-4 52	83.3	2019.	13.27	4526.	.131	9.74	85.1	2094.	13.80
25500•25 2554025		80.5	1881.	12-38-	4792	. 141	-10-40-	82.3	-1953	-12-90
つににさん うに	-/: 20	77 A	1747.	11.56	4.307	0167	11.00	19.0	TOTLO	15.00
25571 • 25 ~	-4-33	75-4	-1616-	10-89	4572	134	-11.55	77.3	1684	11.37
25572.25	-4.51		1/07	10 00	7. 13.374	147	12.18	14.4	177/4	10473
25573.25				9.40 ··	5023.	147 -	.12.74	71.9	1434.	9.85
25574.25	-4.71		1257.			-158	13.40	68.7	1315.	8.99
25575 - 25	4-75	64-5-	-1146.	7.95	- 5522.		13.97	-66.3		- 8.37
25576.25	-5.30		1040.	7.19	6363.			63.1	1093.	7.58
25577.25	-4.52	58.0-	- 979	6-44	5412-	1-61-			989.	- 6.82
55570 35	_/. EA	EE 0	843	5.96	5463.	-158	15.72	57.6	890.	6.32
25579•25 255 79 •25	Q.(52. ₋ .7	751	5.31	6477.	188	16.30	54.5	796	5.65
25580•25 2558 1 •25	-4.52	46 - 3	584	4-10	5739	168	1740	48l	623.	4.40
AFERA AF		1. 1. 2.	5/17 -	3 - 76	SARY.	-16/	1/4/9	40.1	2742	7000
25582•25 25583•25	_ E. OE		435	3-16-	7651.	227-	. 18.32.	42.4	468	3.43
SEED4 OF	_/. 3/.	27 4	360.	2.71	5570.	4 101	18.74	39.4	400	こも ブコ
25584•25 25585•25	-4.C4	3E A	309. 209		7281	214	19.12	36.7	-335.	2-56
		31.5	252	1.90	7817.	.236	19.54	33.2	277.	2.10
25586.25	-5.84			and the second second	6341.		19.88		- 223.	1.72
25587.25	-4.69	20.J	201. 155.	1.26	8200.		20.20	27.3	174.	1.42
25588.25	-6.04		116.		4523.		20.41	23.9	133.	1.09
25589.25	-3,25	55.5	1.10	• • • • •	7JEJ#	• I L ()				

TEST W61 PRESS ALT TEMP WIND VEL 32.0 DEG MAG	TEST NO. 228	MARK III,	ANTISKID/	JSAF TIRES	AME I KONWA	T		12
TOD	ATAMP HCT	TECT WET -	DESS ALT	TEMP.	WIND	VEL .		
TOD ACCEL 6NP-SPD UIST KE FBR UBR EBR KTAS DIS1 KE 7700.61 -3.67 130.9 5375. 28.96 44. 002 .00 132.3 5451. 29.43 27701.50 -4.18 128.9 5160. 28.08 795. 033 .09 130.3 5255. 28.55 27702.50 -4.40 126.3 4964. 26.98 1217. 049 .32 127.7 5039. 27.44 27703.50 -4.48 123.5 4754. 25.80 1483. 059 .65 124.9 4828. 26.25 27704.50 -3.57 121.2 4547. 24.85 543. 022 .81 122.6 4620. 25.30 27704.50 -3.57 121.2 4547. 24.85 543. 022 .81 122.6 4620. 25.30 27705.50 -4.37 115.7 4146. 22.65 1843. 071 1.61 117.2 4218. 23.09 27705.50 -4.37 115.7 4146. 22.65 1843. 071 1.61 117.2 4218. 23.09 27705.50 -4.37 115.7 3764. 20.72 2639. 0096 2.37 112.1 3834. 21.15 27709.59 -3.69 108.2 3579. 19.79 1601. 056 2.73 109.6 3648. 20.22 27705.50 -4.57 105.8 3396. 18.93 2774. 098 3.14 107.3 3466. 19.35 27711.50 -4.57 105.8 3396. 18.93 2774. 098 3.14 107.3 3468. 19.35 27711.50 -4.91 103.0 3222. 17.94 3372. 117 3.70 104.5 3288. 18.35 27711.50 -4.62 100.2 3051. 16.99 3164. 108 4.25 101.7 3117. 11.40 27713.50 -4.02 100.2 3051. 16.99 3164. 108 4.25 101.7 3117. 11.40 27713.50 -4.02 180.2 2864. 15.96 3740. 127 4.86 98.6 294.9 16.36 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27716.50 -3.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27719.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27719.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27719.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27719.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 22774. 12.51 27719.50 -4.04 82.4 1976. 11.47 3423. 115 7.67 83.9 2031. 11.83 27720.50 -5.02 79.7 18.84 10.7 3455. 105 5.02 79.7 18.84 10.7 3455. 105 5.02 79.7 18.84 10.7 3455. 105 5.02 79.7 18.84 10.7 3455. 105 5.02 79.7 18.84 10.7 3455. 105 5.02 79.7 18.85 10.7 3457. 105 10.84 67.7 12.9 13.0 9.09 27722.50 -4.04 69.5 14.45 5.00 4.85 8.7 14.55 2. 153 9.78 73.3 1505. 9.03 27724.50 -4.04 69.5 14.45 5.00 4.04 6.55 11.3 6.82 9.7 71.8 14.55 8.7 14.55 1.5 11.3 6.82 9.25 75.9 16.30 9.60 27725.50 -4.64 69.0 13.7	_		7.784 IN HO	12.7			32.0	DEG MAG
TOD ACCEL GND-SPD DIST KE 27700.61 -3.67 130.9 5375. 28.96 44. 002 .00 132.3 5451. 29.43 27701.50 -4.18 128.9 5180. 28.08 795. 033 .09 130.3 5255. 28.55 27702.50 -4.40 126.3 4964. 26.98 1217. 049 .32 127.7 5039. 27.44 27703.50 -4.48 123.5 4754. 25.80 1483. 059 .65 124.9 4828. 26.25 27704.50 -3.57 121.2 4547. 24.65 543. 0022 .81 122.6 4620. 25.30 27704.50 -3.57 121.2 4547. 24.65 543. 0022 .81 122.6 4620. 25.30 27705.50 -4.37 115.7 4146. 22.65 1843. 071 1.61 117.2 4218. 23.09 27707.50 -4.22 113.5 3953. 21.78 1805. 069 1.16 117.2 4218. 23.09 27707.50 -4.22 113.5 3953. 21.78 1805. 069 1.91 114.9 4024. 22.22 27708.50 -4.71 110.7 3764. 20.72 2639. 096 2.77 109.6 3648. 20.22 27708.50 -4.57 105.8 3396. 18.93 2774. 098 3.14 107.3 3466. 19.35 27711.50 -4.91 103.0 3222. 17.94 3372. 117 3.70 104.5 3288. 18.35 27711.50 -4.91 103.0 3051. 16.99 3164. 108.4 25 101.7 3117. 17.40 27713.50 -4.97 97.2 2884. 15.96 3740. 127 4.86 98.6 2949. 16.36 27716.50 -4.31 92.3 2564. 14.42 3175. 110 5.78 93.8 2626. 14.81 27716.50 -4.03 87.1 2622. 12.83 3085. 105 6.77 88.6 2949. 16.36 27716.50 -4.03 87.1 2622. 12.83 3085. 105 6.77 88.6 221.1 3.20 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 221.1 3.20 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 221.1 3.20 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 2217. 13.20 27716.50 -4.03 87.1 2664. 14.42 3175. 110 5.78 93.8 2626. 14.81 27716.50 -4.02 97 6.8 1707. 9.97 3821. 128 8.79 78.3 1760. 10.31 27721.50 -4.04 66.2 100.2 361. 14.92 3175. 110 5.78 8.6 2217. 13.20 27716.50 -4.04 8.22 8.97 2411. 13.60 3184. 111. 6.28 91.2 2472. 13.98 27716.50 -4.04 6.6 2.72 3.15 4.42 3175. 110 5.78 8.6 2217. 13.20 27717.50 -4.04 8.22 8.97 2411. 13.60 3184. 111. 6.28 91.2 2472. 13.98 27712.50 -4.04 6.6 6.2 12.83 3085. 105 6.77 88.6 2217. 13.20 27712.50 -4.04 6.9 6.6 6.2 12.83 3085. 105 6.77 88.6 2217. 13.20 27712.50 -4.04 6.9 6.6 6.2 12.83 3085. 105 6.77 88.6 2.2 1774. 12.51 27725.50 -4.04 6.6 6.2 12.83 3085. 105 6.77 88.6 2.2 1774. 12.51 27725.50 -4.04 6.6 6.2 12.83 3085. 105 6.77 88.6 2.2 17.4 12.51								
TOD ACCEL 6NP-SPD UIST KE F8R UBB LORN 132.3 5451. 29.43 27701.50 -4.81 128.9 5180. 28.96 44. 002 .00 132.3 5255. 28.55 27702.50 -4.80 126.3 4964. 26.98 1217. 049 .32 127.7 5039. 27.44 27.04.50 -4.81 128.9 5180. 28.08 795. 033 .09 130.3 5255. 28.55 27704.50 -3.57 121.2 4567. 25.80 1483. 059 .65 124.9 4828. 26.25 27704.50 -3.57 121.2 4547. 24.85 543. 022 .81 122.6 4620. 25.30 27705.50 -3.57 121.2 4547. 24.85 543. 022 .81 122.6 4620. 25.30 27705.50 -4.22 113.5 3953. 21.78 1805. 069 1.16 117.2 4218. 23.09 27707.50 -4.22 113.5 3953. 21.78 1805. 069 1.91 114.9 4024. 22.22 27708.50 -4.71 110.7 3764. 20.72 2639. 096 2.37 112.1 3834. 21.15 27709.50 -3.69 108.2 3379. 19.79 1601. 056 2.73 109.6 3648. 20.22 27710.50 -4.97 105.8 3396. 18.93 2774. 098 3.14 107.3 3466. 19.35 27711.50 -4.91 103.0 3222. 17.94 3372. 117 3.70 104.5 3288 18.35 27711.50 -4.91 103.0 3222. 17.94 3372. 117 3.70 104.5 3288 18.35 27711.50 -4.97 105.8 396.8 273 3740. 127 4.86 98.6 2949. 16.36 27714.50 -4.97 3.80 -94.6 2723. 15.14 2464 0.84 5.33 96.1 2786. 15.53 27716.50 -4.93 380 -94.6 2723. 15.14 2464 0.84 5.33 96.1 2786. 15.53 27716.50 -4.22 89.7 2411. 13.60 3184 111 5.78 93.8 2626. 14.81 27716.50 -4.22 89.7 2411. 13.60 3184 111 5.78 93.8 2626 14.81 27716.50 -4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 2211. 13.20 27719.50 -4.07 4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 2211. 13.20 27719.50 -4.07 4.03 87.1 2262. 12.83 3085. 105 6.77 88.6 2211. 13.20 27719.50 -4.07 4.86 170.7 9.97 3821. 128 8.79 78.3 1760. 10.31 27722.50 -4.75 4.96 6.2 10.7 9.7 1838. 10.7 3423. 115 7.0 6.8 99.2 2472. 13.98 27725.50 -4.06 6.2 79.7 1838. 10.7 3460. 128 9.25 59.8 947. 2411. 13.60 6.37 4477. 146 11.73 62.9 1049. 6.65 27724.50 -4.75 6.9 0.7 9.7 1838. 10.7 3480. 11.88 8.79 78.3 1760. 10.31 27722.50 -4.75 6.9 0.7 9.7 1838. 10.7 3480. 11.8 8.79 9.78 73.3 1505. 9.03 27723.50 -4.75 6.9 0.7 9.7 1838. 10.7 3480. 11.8 8.79 9.78 73.3 1505. 9.03 27724.50 -4.74 6.90 6.35 111.3 6.82 39571333 11.30 65.0 1157. 7.11 27726.50 -4.74 6.90 6.35 111.3 6.82 39571333 11.30 65.0 1157. 7.11 27		T	ST DAY					KE
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27716.50 -4.03 87.1 2262. 12.83 3085. .105 6.77 88.6 2321. 13.20 277178.50 -3.93 64.7 2117. 12.14 3055. .105 7.21 86.2 2174. 12.51 27719.50 -4.14 82.4 1976. 11.47 3423. .115 7.67 83.9 2031. 11.83 27720.50 -5.02 79.7 1638. 10.73 4572. .155 8.24 81.2 1893. +1.08 27722.50 -4.29 76.8 1707. 9.97 3821. 128 9.25 75.9 1630. 9.69 27722.50 -4.15 74.4 1579. 9.36 3736. 128 9.25 75.9 1630. 9.69 27724.50 -4.74 69.0 1337. 8.06 4633. .157 10.31 70.6 1384. 8.37 27725.50 -4.64 66.2 1223. 7.41 4608. .158 10.84 67.7 1269. 7.71 27726.50 -4.38<	27715.50 -4.31	92.3 2564.		31/511		91.2	2472	13.98
27717.50 -4.03 87.1 2262. 12.14 3055. -105 7.21 86.2 2174. 12.51. 27719.50 -4.14 82.4 1976. 11.47 3423. 115 7.67 83.9 2031. 11.83 27720.50 -5.02 79.7 1638. 10.73 4572. -155. 8.24 81.2 1893. +1.08 27721.50 -4.29 76.8 1707. 9.97 3821. 128. 8.79 78.3 1760. 10.31 27722.50 -4.15 74.4 1579. 9.36 3736. 128. 9.25 75.9 -1630. 9.69 27723.50 -4.74 69.0 1337. 8.06 4633. 157. 10.31 70.6 1384. 8.37 27724.50 -4.64 66.2 1223. 7.41 4608. 158. 10.84 67.7 1269. 7.71 27725.50 -4.64 66.2 1223. 7.41 4608. 158. 10.84 67.7 1269. 7.71 27726.50 -4.		89.7· 241·1·			_			
27719.50			12.83	308510	B 0 1 1	96.2	2174	12.51
27719.50		84 .7 ··· 2117··	12.14	3055	C 7 47	83.0	2031.	11-83
27721.50				342311	5 7.07	91.2	1993	
27721.50	27720.50 -5.02			45/215	9 70	78.3	1760-	10.31
27723.50 -4.75 71.8 1455. 8.71 4552. .153 9.78 73.3 1505. 9.03 27724.50 -4.74 69.0 1337. 8.06 4633. .157. 10.31 70.6 1384. 8.37 27725.50 -4.64 66.2 1223. 7.41 4608. .158. 10.84 67.7 1269. 7.71 27726.50 -4.01 63.5 1113. -6.82 3957. -133. 11.30. 65.0 1157. 7.11 27727.50 -4.38 61.4 1008. 6.37 4477. .146 11.73 62.9 1049. 6.65 27728.50 -5.10 58.2 907. 5.73 5413. .183. 12.26 59.8 947. 6.01 27729.50 -4.47 55.5 811. 5.21 4752. .158 12.72 57.0 849. 5.47 27731.50 -4.84 49.7 533. 4.17 5350. .178 13.65 51.2 667. 4.41 27732.50 -4.48 <td></td> <td>76.8 1707.</td> <td></td> <td>3061</td> <td>0 0 25</td> <td></td> <td>1630.</td> <td>9.69</td>		76.8 1707.		3061	0 0 25		1630.	9.69
27723.50 -4.75 71.8 1435.8 337.8 8.06 4633.157.10.31 70.6 1384.8.8.37.8.7.1 27724.50 -4.64 66.2 1223.7.41 4608.158 10.84 67.7 1269.7.71 27726.50 -4.64 66.2 1223.7.41 4608.158 10.84 67.7 1269.7.71 27726.50 -4.01 63.5 1113.6.682 3957.7.133.11.30 65.0 1157.7.7.11 27727.50 -4.38 61.4 1008.6.37 4477.146 11.73 62.9 1049.6.65 27728.50 -5.10 58.2 907.5.73 5413.183 12.26 59.8.947.6.01 27739.50 -4.47 55.5 811.5.21 4752.158 12.72 57.0 849.5.47 27731.50 -4.84 49.7 533.4.17 5359.179 13.19 54.2 756.4.94 27732.50 -4.84 49.7 533.4.17 5359.178 13.65 51.2 667.4.41 27733.50 -5.43 44.1 475.3.29 6175.21 14.49 45.7 583.3 3.99 27736.50					0.78	73.3	1505	9.03
27724.50 -4.74 69.0 1337 7.41 4608. 158 10.84 67.7 1269. 7.71 27725.50 -4.64 66.2 1223. 7.41 4608. 158 10.84 67.7 1269. 7.71 27726.50 -4.01 63.5 1113. 6.82 3957133. 11.30 65.0 1157. 7.11 27727.50 -4.38 61.4 1008. 6.37 4477. 146 11.73 62.9 1049. 6.65 27728.50 -5.10 58.2 907. 5.73 5413. 183. 12.26 59.8. 947. 6.01 27739.50 -4.47 55.5 811. 5.21 4752. 158 12.72 57.0 849. 5.47 27730.50 -4.94 52.6 720. 4.68 5389. 179. 13.19 54.2 756. 4.94 27731.50 -4.84 49.7 533. 4.17 5350. 178 13.65 51.2 667. 4.41 27732.50 -4.48 47.1 552. 3.76 4980. 168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. 211 14.49 45.7 504. 3.65 27735.50 -5.83 37.				400Z • • 10				
27725.50 -4.64 68.2 1223. 7.41 2708.50 -4.01 63.5 1113. -6.82 3957. -133. 11.30. 65.0 1157. 7.11. 27727.50 -4.38 61.4 1008. 6.37 4477. .146 11.73 62.9 1049. 6.65 27728.50 -5.10 58.2 907. 5.73 5413. .183 12.26 59.8 947. 6.01 27729.50 -4.47 55.5 811. 5.21 4752. .158 12.72 57.0 849. 5.47 27730.50 -4.94 52.6 720. 4.68 5389. .179. 13.19 54.2 .756. 4.94 27731.50 -4.84 49.7 533. 4.17 5350. .178 13.65 51.2 667. 4.41 27732.50 -4.84 47.1 552. 3.76 4980. .168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7						67.7		7.71
27726.50 -4.01 63.5 1413.6 6.37 4477. 146 11.73 62.9 1049. 6.65 27727.50 -4.38 61.4 1008. 6.37 4477. .146 11.73 62.9 1049. 6.65 27728.50 -5.10 58.2 907. 5.73 5413. -183 12.26 59.8. 947. 6.01 27729.50 -4.47 55.5 511. 5.21 4752. .158 12.72 57.0 849. 5.47 27730.50 -4.94 52.6 720. 4.68 5389. .179 13.19 54.2 .756. 4.94 27731.50 -4.84 49.7 533. 4.17 5350. .178 13.65 51.2 667. 4.41 27732.50 -4.84 47.1 552. 3.76 4980. .168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7 504. 3.05 27735.50 -5.83		11.1.1.1		2057 13	11.30			
27727.50 -4.38 61.4 1008. 6.37 5.73 5413. 12.26 59.8. 947. 6.01 27728.50 -5.10 58.2 907. 5.73 5413. 12.26 59.8. 947. 6.01 27729.50 -4.47 55.5 811. 5.21 4752. 158 12.72 57.0 849. 5.47 27730.50 -4.94 52.6 720. 4.68 5389. 179. 13.19 54.2 756. 4.94 27731.50 -4.84 49.7 533. 4.17 5350. 178. 13.65 51.2 667. 4.41 27732.50 -4.48 47.1 552. 3.76 4980. 168. 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. 211. 14.49 45.7 504. 3.51 27734.50 -5.66 41.0 403. 2.85 6526. 220. 14.93 42.6 430. 3.05 27736.50 -5.83 37.1	_ , ,				4 11.73	62.9		
27729.50 -4.47 55.5 811. 5.21 4752. -158 12.72 57.0 849. 5.42 756. 4.94 27730.50 -4.94 52.6 720. 4.68 5389. .179. 13.19. 54.2 756. 4.94 27731.50 -4.84 49.7 533. 4.17 5350. .178 13.65 51.2 667. 4.41 27732.50 -4.48 47.1 552. 3.76 4980. .168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7 504. 3.51 27734.50 -5.66 41.0 403. 2.85 6526. .220 14.93 42.6 430. 3.05 27735.50 -5.83 37.1 337. 2.33 6814. .229 15.38 38.7 362. 2.52 27736.50 -5.18 34.4 277. 2.00 6100. .204 15.74 35.9 300. 2.17 27738			5 73	E413 .18	3-12-26-	59 - 8-	947.	
27729.50 -4.47 55.5 511. 5389. .179. -13.19. 54.2 .756. 4.94 27731.50 -4.84 49.7 533. 4.17. 5350. .178. 13.65. 51.2 667. 4.41 27732.50 -4.84 47.1 552. 3.76. 4980. .168. 14.05. 48.7 583. 3.99. 27733.50 -5.43 44.1 475. 3.29. 6175. .211. 14.49. 45.7 504. 3.51. 27734.50 -5.66. 41.0 403. 2.85. 6526. .220. 14.93. 42.6 430. 3.05. 27735.50 -5.83 37.1 337. 2.33. 6814. .229. 15.38. 38.7 362. 2.52. 27736.50 -5.18. 34.4 277. 2.00. 6100. .204. 15.74. 35.9 300. 2.17. 27737.50 -6.22. 30.6 222. 1.58. 7398. .251. 16.35. 29.3 191. 1.45. 27738.50 -2.61. <td></td> <td></td> <td>າະ ລາ ລາະ</td> <td>7760 .19</td> <td>8 12.72</td> <td>57.0</td> <td>849</td> <td>5.47</td>			າະ ລາ ລາະ	7760 .19	8 12.72	57.0	849	5.47
27730.50 -4.94 52.0 72.0 72.0 17.0 13.65 51.2 667. 4.41 27731.50 -4.84 49.7 533. 4.17 5350. .178 13.65 51.2 667. 4.41 27732.50 -4.48 47.1 552. 3.76 4980. .168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7 504. 3.51 27734.50 -5.66 41.0 403. 2.85 6526. .220 14.93 42.6 430. 3.05 27735.50 -5.83 37.1 337. 2.33 6814. .229 15.38 38.7 362. 2.52 27736.50 -5.18 34.4 277. 2.00 6100. .204 15.74 35.9 300. 2.17 27737.50 -6.22 30.6 222. 1.58 7398. .251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 173	F11 - 7					.54.2	756.	
27731.50 -4.84 49.7 553. 4.1 552. 3.76 4980. .168 14.05 48.7 583. 3.99 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7 504. 3.51 27734.50 -5.66 41.0 403. 2.85 6526. .220 14.93 42.6 430. 3.05 27735.50 -5.83 37.1 337. 2.33 6814. .229 15.38 38.7 362. 2.52 27736.50 -5.18 34.4 277. 2.00 6100. .204 15.74 35.9 300. 2.17 27737.50 -6.22 30.6 222. 1.58 7398. .251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 173. -1.30 3171. .105 16.35 29.3 191. 1.43								
27732.50 -4.48 47.1 352. 3.29 6175. .211 14.49 45.7 504. 3.51 27733.50 -5.43 44.1 475. 3.29 6175. .211 14.49 45.7 504. 3.51 27734.50 -5.66 41.0 403. 2.85 6526. .220 14.93 42.6 430. 3.05 27735.50 -5.83 37.1 337. 2.33 6814. .229 15.38 38.7 362. 2.52 27736.50 -5.18 34.4 277. 2.00 6100. .204. 15.74 35.9 300. 2.17 27737.50 -6.22 30.6 222. 1.58 7398. .251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 173. -1.30 -3171. .105 16.35 29.3 191. 1.43 27738.50 -2.61 27.7 -173. -1.30 -3171. .105 16.35 29.2 183. 1.43	42							
27734.50								3.51
27735.50 -5.83 37.1 337. 2.33 6814229 15.38 38.7 362. 2.52. 27736.50 -5.18 34.4 277. 2.00 6100204 15.74 35.9 300. 2.17 27737.50 -6.22 30.6 222. 1.58 7398251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 173. 1.30 3171105 16.35 29.3 191. 1.45 27738.50 -2.61 27.7 173. 1.30 3171105 16.35 29.3 183. 1.43	211001						. 430 •	3.05
27736.50 -5.18 34.4 277. 2.00 6100204 15.74 35.9 300. 2.17 27737.50 -6.22 30.6 222. 1.58 7398251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 1731.30 -3171105 16.35 29.3 191. 1.45 1.43						38.7	362.	
27737.50 -6.22 30.6 222. 1.58 7398251 16.12 32.2 242. 1.74 27738.50 -2.61 27.7 1731.30 3171105 16.35 29.3 191. 1.45							300.	
27738.50 -2.61 27.7 -1731.30 -3171. ·10516.3529.3 191. 1.45	W 1 1 1					32.2	242.	
21/30-30 72-31 190 7573 000 16.35 20.2 183. 1.43					16.35		191.	
21138.00 -2.07 21.0 100. 1.27	2110000					29.2	183.	1.43
	21138.00 -2.09	27.0 100.	200		*			

STAND WG 43000.LBS		TEST WGT		RESS AL		TEMP 9.5 C	WIND	VEL KIS	225.0	DIREC DEG MAG
• - + gas - s Afferda	wis limit		TE	ST DAY-				ST/	NDARD D	AY
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
24111.80	-3.58	152.7	00/.4	1.1. 27	0.	*000	0.00	148.9	8347	42.20
24112.75	-4-19		8502***	-43-63-	0.	# 0 0 0	0.00	-146.8 -	8113	41-00
24113.75	-4.55	147.8	8351.	42.04	813.	.032		144.0	7869.	39.47
24114.75	-4.05	145.4	8103.	40.70	348.	.013			7630	
24115:75	-4.20	142.8	7861.	39,29	797.	.029	.40	139.1	7395.	36.83
24116.75	-3.68	140.5	7622.	38.00	267.	010		136.7		
24117.75	-4.31	138.0	7386.	36.67	1252.	•045	.76	134.3	6938	34.31
24118.75	-3.21	135.8	7155	35.51	0 •	*000		-132.1		
24119.75	-4.08	133.7	6927.	34.43	1255.	.044	1.01	130.0	6497.	32.17
24120.75	-3.88	131.2	6704.	33.17	1141.	.039	1.30	127.5		30.96
24121.75	-3.65	129.3	6484	32.18	944.	•032	1.47.	125.6	6071.	30.01
24122.75	-3,55	126.9	6268.	31.03	945.	.032	1.70	123.2		28.91
24123.75	-3.53	124.8	6055.	30.00	1106.	.036		121.1	5659	27.92
24124.75	-3.43	122.9	5847.	29.09	1068.	.035	2.13	119.2	-5460 ·	
24125.75	-3.77	120.5	5641.	27.97	1705.	.055	2.46	116.8		
24126.75	-3.79	118.4	5439.	26.99	1907.	.059	2.82	114.7	5068	25.04
24127.75	-3.05	116.5	5241.	26.12	1040.	.032	3.07	112.8	4879.	24.21
24128.75	-3.64	114.6	5046.	25.29	2057.	.062	3.39		4693	
24129.75	-2.97	112.4	4855.	24.34	1292.	.038	3.72	108.7	4511.	22.50
24130.75	-3.54	110.4	4666.	23.49	2158.	•065		106.8		
24131.75	-3.13	108.6	4482.	22.71	1739.	.051	4.42	104.9	4155.	20.95
24132.75	-3.68	106.5	4301.	21.84	2598	.075	4.84		3982	20.12
24133.75	-3.44	104.2	4123.	20.92	2370.	.069	5.31	100.5		
24134.75	-3.60	102.3	3948.	20:14	2707.			98.6		
24135.75	-3.49	100.1	3777.	19.30	2649.	•077	6.21	96.4	3484.	17.70
24136.75	-4.02	97.8	3611.	18.42	3477		6.75	94-1		10.81.
24137.75	-3.42	95.5	3447.	17.57	2780.	.080	7.26	91.9	3169.	18.06
24138.75	-3.35	93.5	3288.	10.03	2764	-080	7.71		3018	
24139.75	-4.11	91.5	3131.	16.11	3890.	•110	8.22	87.8	2869.	14.68
24140.75	-3.02	89.2	2979.	15.32	2509			85.5		13.93
24141.75	-4.24	87.4	2829.	14.70	4219.	.123	9.17	83.7	2584.	13.35
24142.75		85.0	2684.					81.3	2440	12.39
24143.75	-3.74	83.0	2543.	13.28	3742.	107	10.19	79.4		12.00
24144.75	-3.53	80.6	2405.	12.52	3557			77.0		11.28
24145.75	-3.43	78.5	2270.	11.87	3488.	.099	11.18	74.9	2055.	10.67
24146.75	-3,13	76.6	2139.		3149		-11.60	73.0		10.15
24147.75	-4.28		2012.	10.71	4756.	.139	12.11	71.0		9.58
24148.75	-3.79		1888.		4198.		12.69	68.3	1505	8.67
24149.75	-2.93		1768.	9.47	3112.	.087	13.09	66.5	1585	
24150.75	-3.72	68.0	1651.	8.90	4242.		13.54		1475	
24151.75	-3.52	66.0	1538.	8.38	4047.	•113	13.99	62.4	1370	7.40
24152.75	-3.53		1429.	7.83				60.2	1171	4 55
24153.75	-2.00	62.2	1323.	7.46	2092.	.060	14.68	58.6	1171.	6.55

TAND WG	r 0,28	TEST WGT	2	PRESS A	LT HG	TEMP 13.4 C	WIN 3.	D VEL 5 KTS	WIND 225.0	DIREC DEG MAG
1 1	45 050		TI	EST DAY-		3 / 50		ST	ANDARD D	AY
TOD		GND-SPD	DIST	KE		UBR	EBR	KTAS	DIST	
14.68	-3.45	140.2	7417.	33.23	0.	*000	0.00	135.9	6964.	31.08
		138.7	7223.	32.54		000		134.5		
16.50	-4.46		6991.	31.31	945.	.041		131.8	6555.	
17.50	-3.76	133.6	6763.			.014	.31	129.4		28.16
18.50	-3.98	131.4	6539.	29.18	7.08.	.029	.41	127.2	6121.	27.20
19.50		129.0	6319.		996.		.63	124.8	5909.	
20.50	-3.18	126.9	6104.		79.	.003	.69	122.8	5704.	
	-3.66		5891.		739.	.029	.83		-5499	
22.50	-4.04		5682.	25.46	1352.	.052	1.02	118.5	5300.	
23.50	-3.55	120.1	5478.	24.39		.035	1.29	116.0	5103.	
24.50	-3.53	118.2	5276.	23.64	1014.	.038	1.44	114.1	4911.	21.90
25.50	-3.37		5079.		930.	.035	1.64	112.0	4722.	
26.50	-3.80	114.2	4884.	22.07	1569.	.058	1.86	110.1	4537.	
	-3.47		4594.	51.15		.050		107.7		
28.50	-2.87	110.0	4507.	20.48		.028	2.34	106.0	4177.	18.89
29.50	-3.91		4322.	19.76	2153.	.075		104.0	4001.	18.20
30.50	-3.61	105.7	4142.	18.91		.068	3.03	101.7		
31.50		103.5	3965.	18.11		.071	3.39	99.4		
32.50		101.7	3792.	17.47		.061	3.69	97.6	3497.	16.03
33.50		99.4	3621.	16.71		• 00.3	4.00	95.4		
		97.5	3456.		2468.	.083	4.44	93.5	3178.	14.70
	-2.95		3293.				4.76	91.4		
	-3.76	93.4	3133.	14.74		.091	5.13	89.4	2872.	13.43
38.50		91.6	2977.	14.18	2201.	.073	5.46	01.6	2726.	12.91
		87.2		12.87		.079	6.25	85.4	2441	11-67
40.50		85.7	2530.	12.41		.089	6.58	81.7	2304.	11.24
41.50		83.3	2387.		3436.		7-05	79.3		
42.50		81.0	2249.	11.09		.118	7.51	79.3 77.1	2039.	9.99
43.50		78.4		10.38	4243.	.140			1912.	
44.50		75.7	1984.	9.70	3384.	-112	8.55	71.8		8.68
			1958.	9.21	3386	114	8.95	69.9		
	-3.66	71.3		8.59	3462.	.116	9.40	67.4		7.64
47.50				8.11		-146	9.85	65.4		
48.50	-3.51	66.6	1502.	7.51	3424.	.116	10.31	62.8	1338.	6.63
49.50	-4.24	64.6	1391.	7.06	4361	.145	-10.72-	60.8	1235.	6.22
50.50	-4.66	61.7		6.44			11.24		1134.	5.64
51.50	-4.20		1182.	5.93	4468.		11.70		-1039.	5.16
52.50	-4.45	56.7	1084.	5.43	4840.	.163	12.16	52.9	948.	4.70
53.50	-3.72	54.2	991.	4.97	4041.	.134	12.56	50.4	862.	4.28-
54.50	-4.11	52.1	901.	4.59	4556.	.151	12.93	48.3	780.	3.93
55.50	-4.83	49.3	816.	4.11	5473.	.185	13.37	45.5	700.	3.49
56.50	-4.03	46.7	735.	3.68	4579.	.155	13.76	42.9	626.	3.10
57.50	-3.95	and the second second	658.	3.29	4549.	.152	14.12	40.4	556.	-2.75
58.50	-4.27	42.1	585.	3.00	4976.	.164	14.44	38.4	490.	2.48
59.50	-4.13	39.3	517.		4874.	.157	14.79	35.6		2.13
60.50	-3.73	36.9	452.	2.31	4454.	.141	15.08	33.3	370.	1.86
61.50	-4.31	34.8	391.	2.05	5185.	-162	15.36	31.2		1.63
62.50	-5.44	31.7	335.	1.70	6552.	.217	15.71	28.1	265.	1.33
63.50	-4.24	28.8	284.	1.41	5167.	.173	# 7 D 7 D 8	25.2		1.07
64.50	-4.49	26.4	237.	1.18	5494.	.185	16.23	22.8	179.	.87
65.18	-3.64	24.5	208.	1.02	4516.	150	16.33	- 20 9	154.	- 474

STAND WG		TEST WGT 34200.LBS		RESS -657	ALT IN HG	15.8 C	3.9		505°0 MIND	DEG MAC
			TE	ST DA	Υ			ST	ANDARD I	
TOD.	ACCEL	GND-SPD						KTAS	DIST	KE
28685.36	-4.31	132.8	6728.	26.7			.02	127.9	6227.	24.61
28686.25	-3.93		6531.	25.7			•13	125.6	6039.	23.73
28687.25	-4.49		6312.	24.8			•26	123.3	5831.	22.89
8688.25		125.5		23.8				120.7		21.92
28689.25	-4.13		5888.	23.0			•58	118.6	5428	21.16
8690.25			5682.				• 75	116.0		
8691.25	-4.18	118.9	5479	21.3			.89	114.1	5040 • - 4851 •	19.59
		116.1						111.3	4668.	18.11
8693.25			5086.	19.8			1.25			17.42
8694.25			4895.	19.1		- 038 - 045	1.41	107.6 105.2	4309	
8695.25			4707.	18.2				103.8		-16-23
8696.25			4523.	17.8			2.06	101.3	3966	15.44
8697.25	-3.95	105.9	4342.	16.9	9 1796 8 2081		2.40	99.0		-14.76
8698.25				15.6			2.69	96.9	3635.	14.14
8699.25	-3.23		3992.				2.95			- 13.57
8700.25			3656.	14.3			3.23	92.8	3320.	12.97
8701.25	-3.28		3493.				3.51	90.8	3167	12:42
8702-25	-3.46		3333.	13.7			3.75	89.1	3018.	11.96
8703.25 8704.25	-3.03		3177.	12.7	4 2409				-2872	11.45
8705.25			3024	12.0			4.43	84.9	2728.	10.84
8706.25			2875				4.70		2590	
8707.25	-3.75		2729.	10.9			5.08	80.7	2452.	9.79
8708-25	-2.89			10.5			5-34		- 2321.	
8709.25	-3.28		2447.	10.0			5.67	76.9	2191.	8.89
8710.25	-3-28			9.6			5-94	75-4-		
8711.25	-4.21	77.3	2178.	9.0			6.37	72.9	1941.	7.99
8712.25	-3.56		2050.	8.5			6:74	70.8	1822.	7.55
8713.25	-2.87		1925.	8.0			7.06	68.6	1706.	7.08
8714.25	-4.05		1802.	. 7.7	5 3439	129	~7.35	67.2	1594	6.80
8715.25	-3.91	68.4	1584.	7.0	8 3399		7.81	64.1	1483.	6.19
8716.25	-3.36	67.4	1570.	6.8	8 - 2832	106-	···-8 • 06 ··		1380.	
8717.25	-4.51	64.2	1459.	6.2		•158	8.52	60.0	1276.	5.42
8718.25	-2.82	62.3	1352.	5.8			8.82			5.08
8719.25	-4.43		1248.	5.5	4 4185	• 154	9.15	56.3	1084.	4.77
8720:25	-3.46	57.5	1148.		0 3226		9.55			4.27
8721.25	-3.84	56.4	1052.	4.8			9.81	52.2	906.	4.10
8722.25	-4.75	··· 53.1	~~960%~	4.2	6 - 4718		10.25		820-	
8723.25	-4.29	50.8	872.	3.9			10.61	46.7		3.28
8724.25	-3.88	48.2	789.	3.5			10.95	44.1	665	2.93
8725.25	-4.25		709.	3.1			11.28	41.7	593•	2.62
8726.25	-3.58	43.7	634.	2.8			11.56	39.7		2.37
8727.25	-4.29	41.3	562.	2.5			11.86	37.3	462.	2.10
8728.25	-4.54	38.5	495.	2.2			12.18	34.5		1.79
8729.25	-4.47	35.7	432.	1.9			12.49	31.8	345.	1.52
8730.25	-4.06	33.3	374.	1.6			12.74	29.4	294	
8731.25	-3.83	30.9	320.	1.4			12.97	27.0	247.	1.10
8732.25	-3.30	29.0	269.	1.2			13.16	25.1	205	
8732.91	-2.27	27.6	237.	1.1	6 2577	.097	13.23	23.7	178.	•85

TEST NO. 246	MAR	K II DW.	riskidzs	CRACIPAT	TIKES	INET KUN	WAY .		
STAND WGT	TEST WGT		ESS AL		TEMP.	WIND		WIND	DIREC DEG MAG
		27	564 IN	HG 1	7.5 C	3.9	NIS		
	3//86.485	· .TE					ST/	ANDARD D	AY
TOD ACCE	L GND=SPD		KF	FBR			KTAS	DIST	КЕ
27189.80 -4.0		7557.	33.22	127.	.005	.01	138.3	7331.	32.18
	2 138.3	7332.	32:01	508	.021	15	135.8	7111	31.00
27101 75 -3.7	5 136.2	7101.	31.04	81.	• UV3				
27192.75 -4.4	7 133.6	5573.	29.35	1107		38	131.0	6460	27.92
27193.75 -3.5	5 131.4	1665	20 86	1/6-	~ [11] 7	48	128.8	6442	
27194.75 -3.9	9 129.1		27.88	342	0.33	-60	124.1	6015	25.90
27195.75 -4.1		6214.		1178 · · · · · 339 · · ·	013	99:	121 0	5808-	25.01
27196.75 -3.3				1174.			120.0	5605.	24.20
27197.75 -3.9	1 122.4	5793		330		1.27	117.9	5406	
_	7 120.4	5387.	23.22	1825.		1.57	115.4	5208.	22.41
27199.75 -4.2			122155	417.		1.70	113.7	5016.	21.75
27200.75 -2.9		.4996	21.09	1297.	. ()40	1.93	111.5	4826	
27201.75 -3.6 27202.75 -3.3		~4906 · **	21.00	1050	T-038	2.12	109.7"	4640	50.53
27203.75 -3.3		4519.	20.19	1269.	. ()45	2.37		4458.	19.45
27204.75 -3.4			19.40	1444.	.052		105.4	4278	18-68
27205.75 -3.1	1 107.7 3 105.7	4254.	18.70	1237.	.044	2.89		4102	17.99
27206.75 -3.1		4078	_18.55 _		.047		102.1		17.53 16.61
27207.75 -3.5	4 101.6	3904.	17.28	1933•	.067 .039	3.44	99.4 98.1 96.0	3594	
27208.75 -2.7	9100.4		16.85	1117.	.039	3.61	96.0	3431.	
27209.75 -3.7	4 98.2	- 3566•	16.13	2328	1911	3.96 4.29 4.54	93.7	3271	
27210.75 -3.0		3402	15.38	1626 • 1954 •	067	4.54	92.2	3115.	A
27211.75 -3.2	6 94.4		14.91	2005	009	-4.86	90.2	-2962.	
27212.75 -3.2		2928.	17 68	2534.	-087	5.20	88.3	. 2812.	13.10
27213.75 -3.6		~-2777.	13.05	-2144	074	5.55	86.2	2665.	
		2530	12.51	2867.	.098	5.91	84.4	2522.	
27215.75 -3.7 27216.75 -3.1		2486	11:90	2325		- 6.29	82.2	2382.	
27217.75 -3.8	35 82.3	2345.	11.33	3184.	•10e	6.68	80.5	2245.	
27218.75 -3.4		~ 2208.	10.77	2856		7.07	78.2		10.28
27219.75 -3.6	4 77 0	2075.	10.15	3120.	• 106	7.49	75.8	1983	9.67
27220.75 -3.0	75.9	1945.		3533		7.91	73.8	1735	
27221.75 -3.4	73.3	1519.	8.99	3074.	-103	B 34	71.3	1616.	
27222.75 -3.9	71.5	1596.	8.55	3675			69.5 67.0	1501.	
27223.75 -3.9		1578.	7.97	3725•	.124		~ 64.8	1391	
27224.75 -3.		1463.		3729			62.6	1284.	
27225.75 -3.1	64.5	1353	6.96	3854		10.43	60.1	1180.	
27226.75 -3.				3856.	129	10.79	58.3	1081.	5.72
27227.75 -3.	78 60.2 26 57.7	1142. 1043.	5.56	4492			-55.8	985.	5.23
27228 - 75 -4 -4		948.	5.02	5305.		11.70	52.9	893.	
27229.75 -4.6		857		4072-		12:09	50.7		
27230.75 -3. 27231.75 -4.		771.	4.20	5016.	-164	12.48	48.3	723•	
27232.75 -4.	•	589	3.70		165	-12-90-	45.2	644	3.44
27233.75 -4.		611.	3.35	5013.		13.27	43.0	570 •	
27234.75 -3 .		538	2.95					500 · 434 ·	A
27235.75 -4.	18 39.9	469	2.67	4825	.160		38∙2 - ≟35∙6-		2.13
27236.75 -4.	37.3	403		5715	188	14.2 5 14.59	32.7	314.	
27237.75 -4.	5.7 34.3	343.	1.97	5382	-182	14.88			
	68 31.7			5571 • 6218 •			27.0	213.	
27239.75 -5.	21 28.6	236.	1.37			15.43	24.3	170.	.99
27240.75 -4.	12 25.9	190° 169°	1.02	3926			23.1	150.	.90
27241.25 -3.	19 24.7	1074	1.00	U / L U #	-				

TEST NO. 2	240	MARK	TI ANT	TSKIUZS	TANDARD	TTHES/	WET KUNI	VAY		
TEST NO. 2	-46	.,,,,	• •						w T NID	DIREC
STAND WGT	г	TEST WGT		KESS AL	•	TEMP	MIND	KTS	240.0	DEG MAG
34000 LBS		3630.LBS	27.	561 IN	HG 2	0.b C	3 • 0.	11.13	12.100	
-								STA	NDARD E	AY
			TES	ST DAY		UBR"	- EQÓ ··	KTAS	DIST	KE
TOD	"ACCEL"	GND-SPD "	DIST				*01	127.3	6045	24.41
29667.43	-4.15	131.7	6380•	25.84	414.	.020 .025				~23,69
29668 . 25	-4.16	129.8	6200.	25.10	530.0	.007	:50	122.9	5661.	22.73
29669.25	-3.64	127.3	5983.	24.11	137•	009		121.1	5455%	22.09
29670.25	-3.55	125.5	5770.	23.44		.054	.41	118.7	5252.	21.20
29671.25	-4.35	123.0	5560.	22.52	1211. 935.	.042		116.2	5054	20.32
29672.25	-3. 96	120.5	5355.	21.61	838.	.636	.78	114.1	4860.	19.59
29673.25	1-3.75	118.3	5153.	20.85	1642.	.070	1.08		4668.	18.67
29674.25	-4.38	115.6	4955.	19.90	728	0.32	1.23	109.5	4482.	18.05
29675.25	-3.42	113.7	4762	19.25	1087.	. 1146			4299.	17.35
29676.25	-3.63	111.5	4572.	18.52 17.86	1096	.046	1.60	105.4	4120.	16.71
29677.25	-3.54	169.5	4385.	17.16	1142.	.047	1.81	103.2	3945	16.04
29678:25	-3.47	107.4	4203.	16.48	1249	.052	2.03	101.1	3773.	15.39
29679.25	-3.46	105.2	4023. 3847.	15.82	1435.		5.58	99.0	3604	-14-76
29680.25	-3.55	103.1		15.23	1497.	.061	2.52	97.1	3439.	14.19
29681.25	-3.48	101.1	3575-	14.54	1814.		2.82	94.8	3276	13.53
29682 - 25	-3.69	98.8	3506.	13.97	1872.	.075	3.10	92.9	3118.	12.98
29683.25	-3.62	96.9	3341. 3179.	13.40	1679		3.38	90.9		12.44
29684.25	-3.33	94.9	3021.	12.80	2062	.081	3.na	8.86	2813.	
29685.25	-3.61	92.7	2566.	12.11	3497.	.134	4.14	86.3	2664.	
29686.25	-4.85	90.2		11.40	1855	.070	4.53	8.88	2521	10.58
29687.25	-3.17	87.7	2716. 2569.	11.01	2054	.077	4.79	82.r		10.15
29688.25	-3.29	86.0	2426	10.50	2174.	.082	5.11	80.1	2245.	
29689.25	-3.34	84.0	2286.	10.02	2523.	.045	5.42	78.2	2112.	
29690 • 25	-3.60	82.0	2150.	9.57	2851.	,107	5.83	75.6	1982.	
29691 • 25	-3.81	79.3 77.9	2017.	9.05	2032.	.078	6.09	, , ,	1857	
29692.25	-3.00	75.8	1587.	5.55	3154.	.119	6.45	72.1	1734.	
29693.25	-3.98	73.3	1762.	5.00	3247.	.123	6.86	69.6	1615.	
29694.25	-3.99	71.0	1540.	7.51	2167.	.052	7.19	67.3	1500.	
29695 • 25	-2.89	69.6	1521.	7.21	2964.	-108	7.46	65.9.		
29696.25	-3.59 -4.81	რი, მ	1400.	ဂ်•ဗ5	4303.	.163	7.93	63.2	1279	
29697.25	-3.42		1296.	6.18	2920.	113	8.30	60.8	1175	
29698 • 25	-3.99		1189.	5.78	3587•	.134	8.64	58.7	1075 978	
29699.25 29700.25	-3.96		1085	5.28	3637.	•136	9.04	56.0	886	
29701.25	-3.81	•	986.	4.94	3533•		9.36	54.1	797	_
29702.25	-3.95		591.	4.54	3739.	.142	9.72	51.7	712	
29703.25			80u.	4.13	4172.	.157	10.08	49.2	632	
29704.25	-3.43		713.	3.80			-10.38		554	
29705.25		47.9	529.	3.41	6372•	.236	10.81	44.5 41.2		
29706.25	-3.90		553.	2.95		147	11.19		414	
29707.25			478.	2.62	5662		11.53	38.6 35.5		1 -90
29708.25		_	411.	2.24	5083.		11.90		294	
29709.25			348.	1.93	5515		12.22	32.7 29.4		130
29710.25	-4.63		290.	1.59	4947.		12.53		194	
29711.25		_	237.	1.35	5244		12.78	26.9 24.0	151	
29712.25			188.	1.10	3807.		13.00	23.2	127	
29712.91			159.	1.03	2126.	.074	13.05	23.2		

TEST NO.	254	MARK	II AM	TISKID/S	TANDARD	TIRES/	WET HUN	WAY	102	4. 1.47
1621 40.						TEMP	WIND		WIND	DIREC
STAND HG		TEST AGT		529 IN		5.5 C	5.5		225.0	DEG MAG
40000 .LHS	1200 4	+0086.L85	211			S 100 - 1		Trade Street		-
			TF	ST DAY				STA	NUARD D	AY
700			DIST	KE.	FBR	UHR	ERR	KTAS	DIST	KF
100		GND-SPD	6404.	38.78		0.000	0.00	144.2	7999.	36.82
24402.52	-3.79	147.8	2165.	37.37	408.	.035	.14	141.5	7765.	35.46
24403.50	-4.72	142.5	.5567	35.01	124.	.005	.24	138.9	7530 .	34.15
24404.50	-3.94	140.2	7564.	34.69	841.	.034	.33		7299.	33.06
24405.50	-4.39	137.4	7449.	33.44	570.	.024	.57.		7073.	31.71
24406.50	-4.06	135.6	7219.	32.03		0.000	.57	132.1	6852.	30.89
24407.50	-3.34	133.1	6952.	31.45	810.	.032	.72	129.6	6632.	29.75
24408.50	-4.02	130.9	67t9.	30.41	921.	.035	.90	127.4	6417.	28.75
24409.50	-3.97	128.7	6551.	29.40	. 0.	0.000	.99	125.3	6207.	27.79
24410.50	-3.14	126.5	6335.	24.39	1048.	.040	1.14	123.1	1000	26.81
24411.50	-3.85	124.4	6123.	27.48	936.	.634	1.33	121.0	5795.	25.94
24412.50	-3.65	122.3	5915.	26.50	372.	.014	1.48	119.0	5595.	25.06
24413.50	-3.12	150.9	5710.	25.40	481.	.017	1.51	117.4	5399.	24.42
24414.50	-3.09		550H.	24.92	1052.	.U38	1.75	115.2	5204.	23.48
24415.50	-3.46		5309.	24.22	570.	*050	1.86	113.5	5014.	55.81
24416.50	-2.99		5114.	23.42	1627.	.058	2.10	111.6	4827.	22.04
24417.50	-3.73		4922.	22.42	1226.	.043	2.43	109.1	4642.	21.09
24418.50	-3.31	112.4	4734.	21.90	615.	.055	2.52	107.8	4462.	20.59
24419.50	-2.75	111.1	4548.	21.05	1016.	.035	2.75	105.6	4284.	19.76
24420.50	-2.96		4365.	20.42	1389.	.048	2.94	104.0	4109.	19.16
24421.50	-3.19		4186.	19.74	1815.		3.72	.102.3	3938.	18.52
24422.50	-3.42		4010.	18.93	1586.	.053	3.54	100.1	3769.	17.74
24423.50	-3.17		3837.	18.31	1375.	F8. 18. 1 LZ	3.78	98.4	3604.	17.14
24424.50	-2.92		3567.	17.62	1579.		4.05	96.5	3442.	
24425.50	-3.03		3499.	16.95	2775.		4.42	94.6	3282.	
24426.50	-3.90		3337.	16.32	837.	10.00	4.70	92.8	3127.	
24427.50	-5.26		3175.	15.86	2245.		4.42	91.4	2974.	14.80
24429.50	-3.36		3617.	15.00	3471.		5.45	48.9	-5853•	
24429.50	-4.20	4.4		14.33	1955.		5.54	86.8	2678	13.34
24430.50	-2.94		2710.	13.09	2373.		6.18	84.8	2535.	
24431.50	-3.20			13.15	3022		6.50	83.1	2395.	
24432.50	-3.67	24/36/200	2425.	12.39	3464		7.00	80.6	2258	11.49
24433.50	-3.93			11.81	2219.	4 44 4	7.42	78.6	2126.	
24434.50	-2.86		5560.	11.35	2944		7.75	77.1	1997.	
24435.50	-3.41		2150.	10.73	3075		8.17	74.8	1871.	9.91
24436.50	-3.44		2017.	10.20	3665		8.59	72.9	1748	
24437.50	-3.85		1701.	9.55	3795		9.01	70.5	1628	
24438.50	-3.8		1539.	9.04	2793	20.12	9.45	68.5	1513.	
24439.50				8.58	3326		9.81	66.7	1401.	
24440.50	-3.4		1920.	2.07	4014	6. 75.00	10.24	-64.6	1292	
24441.50	-3.8	9 67.4	1292.	7.47	453H		10.73	62.0	1186	
24442.50	-4.2			I was to be a like	2668		10.98	60.2	1097	6.41
24443.38	-2.6	8 63.0	1198.	1.03	4,000		-			

STAND WGT 36000.LBS	TEST #6T 36086.195	PAESS 27.535 1	ALT N dG	TEMP		VEL	WIND	DIREC
				1000 (۷.	4 KTS	34.0	DEG MAG
TOO """	~	TEST DAY					raain ana	
TOD ACCE	L GND-SPD DIST	KE	` FBR	TUBE		KTAS	ANDARD	DAY
26719.933.9		28.01		005	.00			-KE
26720.75 -4.4	8 130.4 6126.	27.18	787.	039	.13	132.7	6303.	28.07
26721.75 -4.09		26.05	501.			130.1	6124.	
26722.75 -4.3:	3 125.1 5595.	24.99	926			128.1	5911.	26.13
26723.75 -4.13	3 122.7 5485.	24.05	932.	.040			5701	
26724.75 -3.59	5 120.4 5280.	23.15	435.	.018		123.1	5495.	24.16
26725.754.61	1 115.2 5078.	22.31	1760.	•073		120.8	5293.	23.27"
26726.75 -3.43	3 115.8 4861.	-21,40	594			118.7	5094.	22.45
26727.75 -3.67	7 113.8 4567.	20.69	975.			116.3	4900.	21.55
26728.75 -3.53		19.95	901.	-036	1.51	114.4	4708.	20.84
26729.75 -3.36			844.	.034		112.4	4521.	20.12
26730.75 -3.84		18.53	1503.	•058	1.69	110.1	4337	19.32
26731.75 -3.99		17.62	1799.		1.87	108.4		18.71
26732.75 -2.42	163.5 3773	17.12	153.	0071	5.22	105.7	3978.	.17.81
26733.75: -4.02	101.5 3500.	16.46	2029	-006	2.30	104.3		17.32
26734.75 =3.71	99.1 3431.	15.69	1806	-080	2.53	102.3	3632.	16.56
26735.75 -3.53	96.8 3265.	14.97	1732.		2.87	99.9	3465.	15.91
26736.75 -3.90	94.9 3103.	14.39	2523	.067	3.17	97.6	3301.	15.19
26737.75 -3.28	92.4 2945.	13.64		• 086	3.47	95.8	3140.	14.62
26738.75 -4.13	90.5 2789.	13.08	10000	. 003	3.79	93.3		13.87
26739.75 -3.28		12.44	2717.	.102	4.12	91.4	2829.	13.31
26740.75 -3.05	86.8 2492.		1839.	•070	4,44	89.2	2680.	12.69
26741.75 -4.70		11.36	1674.			87.8		12-28
26742.75 -3.07	82.0 2207		3627.	- 135	5.06	85.4	2389	11.61
26743.75 -3.36	80.4 2071	10.13	1888		5.42	*83.1	2250.	11-01-
26744.75 1-3.90	77.7 : 1937.	10.32	5282	.086	5.68	* NOT 12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2112	1 4 4 4
26745.75 -3.89	75.7 1507.	9.64	2982	.115	··· 6.08~ ··	78.8	1980	9-00-
26746.75 -4.18	73.2 1582.	9.15	~ ~ ~ .	4112	0.40	76.9	1850.	9.41
26747.75 -3.60		2.57	3488	.128	6.88	- 74 64	-1725	
26748.75 -3.76		8.03	2919.	.107	7.26	72.1	1604.	8.29
26750.00 -4.09	1446	7.51		118	7.71		1485	~7.77.
26751.00 -4.65		6.90	3064.	•134	8-11	67.1	1242	7 1 7
26752.00 -4.09		6.40	4368.	*161 -	8.55	64.6	1233	6. 66
26753.00 -3.96	60.4 1087.	5.62	3843.	138	8.98	61.8	1129.	6:00
26754.00 -4.12	58.1 986.	5.39	-3763.	•137	9.35		1027	6.08
26755.00 -5.22	56.2 591.	5.04	3988.	.148	9.69	57.6	920	E 20
26756.00 -4.95	52.8 798.	4.46	5327	.196 -	10.17	54-4	767.	5.29
26757.00 -5.10	50.4 711.	4.06	5089.	.188	10.58	52.0	749	
·	- 0004	3.51	5358		11.03 -	-48.5		4.31
	44.3 552.	3.14	4545.	.161	11.38	46.0	500	
	41.5 479.	2.75		_		-43.2··-	588.	3.37
	36.6 412.	2.34	4722.	-	12.10	40.3		
26761.00 -4.82	36.3 349.	2.11	5312.		12.39		445.	2.59
26762.00 -5.38	32.7 291.	1.71			12.74	38.1	379.	2.31
26763.00 -4.74	30.1 237.	1.45				34.5	320.	1.90
26764.00 -5.27	26.9 189.	1.15		-225	13.30	32.0	264.	
26764.98 -2.62	24.4 147.	.95		·105	13 ""	28.8	214.	1.32
				• 1 v D	13.45	26.3	169.	1.10

TEST NO. 26A	MÄRK	II ANTISK	(ID/SOMMERS	TIRES/	WET RUNWA	ΑY		
STAND WGT	TEST WGT	PRESS	ALT	TEMP	WIND	VEL	WIND	DIREC
	39436.LBS	27.545	IN HG	15.8.C	. 4.2	KTS	280.0	DEG MAG
1		· TroT f	\ A U			CTA	NDADD F)ΑΥ
TOD ACCEL		IST KE	AY FBR	· UBR		KTAS	DIST	KE.
25002.87 -4.60		394 40		0.000	0.00	149.3	7264.	39.47
25003.75 -4.68		170. 38		0.000	0.00	146.9	7041.	38.19
25004.75 -4.49				0.000		144.2		-36.80-
25005.75 -4.23		675 . 36			.02	141.7	6548	35.54
25006.75 -4.41		434. 34.			.20	138.8	6308.	34.11
25007.75 -3.81		197. 33.		.004	22	136.7	6073.	33.10
25008.75 -4.40		964. 32.					-5841	-31.83
25009.75 -4.26		736. 31.		.040	.61	131.7	5614.	30.73
25010.75 -3.89			21 742.	.029		129.0 ~		-29.47
25011.75 -4.06		291. 29.		.041		126.9	5173.	28.52
25012.75 -4.12		075. 28.		.049-	-1.29 -	124.4	4958.	27.41
25013.75 -4.27		863. 26.		.062	1.64	121.8	4747.	26.26
25014.75 -3.88		555. 26.		.048	1.90	119.6	4542.	25.32
25015.75 -4.11		451. 24.		.064	2.22	117.1	4340.	24.30
25016.75 -4.22	117.2 4	251. 23.	97 2025.	.074	2.61	114.7	4141.	23.28
25017.75 -4.11	114.8 4	055. 23.	02 2040.	•075		112.3	3948.	22.34
25018.75 -4.36	112.2 3	864. 21.	98 2496.	.091	3.45	109.7		21.31
25019.75 -4.05		576. 21.		.081	3.88	107.2	3573.	20.35
25020.75 -3.84	107.5 3	493. 20.		- 075	4.26	105.1		19.55
25021.75 -4.12		314. 19.		•093	4.73	102.4	3215.	18.57
25022.75 -3.62		139. 18.			5.10	100.3		17.82
25023.75 -3.80		967. 17.		•086		98.0	2873.	17.01
25024.75 -4.24		799. 16.		- 108			.2708	16.18
25025.75 -4.12		536. 16.	05 3043.	.107	6.45	93.4	2547.	15.45
25026.75 -4.56	· ·	477. 15.		•131	7.03		2390 •	14.51
25027.75 -4.65		322. 14.		•137	7.61	87.9	2238•	13.68
25028.75 -4.16		172. 13.		.120	8.18	85.1		12.82
25029.75 -4.13		026. 12.		.122	8.65 . 9.22	82.9	1947.	12.18
25030 - 754 - 45		984. 11. 747. 11.		124	9.72	77.8	1673.	10.72
25031.75 -4. 06 25032.75 -4. 92		513. 10.		•164	10.32		1542.	9.94
25032.75 -4.92 25033.75 -4.76			74 4716.	161	10.90	72.3	1416.	9.24
25034.75 -4.71			00 4748		-11.50			
25035.75 -4.75		242. 8.			12.06	66.6	1180.	7.86
25036.75 -5.05			64 5369		12.64			
25037.75 -4.54			96 4837.	.164	13.19	60.8	963.	6.54
25038.75 -4.91			37 5379.	180	13.72	58.0		- 5.96
25039.75 -5.00		815. 5.	78 55.75.	186	14.26	55.1	764.	5.38
25040.75 -4.72					14.75			
25041.75 -5.55		530. 4.		.210	15.27	49.5	586.	4.34
25042.75 -5.78		545. 4.		.230	15.82		504.	3.76
25043.75 -6.49		466. 3.		.258	16.40	42.4	428.	3.18
25044.755.68		394. 2.			16.90	38.9	. 359.	2.69
25045.75 -5.87		328. 2.		.234	17.36	35.4	295.	2.21
25046.75 -5.79	-	267. 2.			17.78	32.0	237.	1-•81
25047.75 -5.50	30.9	212. 1.		•229	18.15	28.6		- 1.45
25048.75 -4.60		162. 1.		-187-	18.46	25.3	140	
25049.17 -3.30	26.8	145. 1.	26 4199.	•130	18.49	24.5	125.	1.06

TEST NO. 26B	MAR	K II AN	TISKID/	SOMMERS	TIRES/	WET RUNW	AY		
CTAND UCT	TEST WGT		RESS A	LT	TEMP	WIND	VEI	MIND	DIREC
STAND WGT	35786.LBS		-545 IN			1.6			DEG MAG
			CT DAY-				ST	ANDARD ()ΔΥ
	L GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	ΚE
		6123.	30.50	299.	- 015		136.2		- 29.57
27116.00 -4.4		5891.	29.42	343.	.016	.07	133.7	5714.	28.51
27117.00 -4.2				1023.		25	131.1	5492	
	0 · 133.6	5663. 5440.	27.10	806.	037	.47	128.3	5274.	26.24
27119.00 -4.3		5221.	26.14	326.	.014	-56	126.0	5061.	
27120.00 -3.7		5006.	25.13	1331.	.057	.78	123.5	4851.	24.32
27121.00 -4.5	_	4795.	24.21	494	.021	.94	121.3	4646.	
27122.00 -3.6	_		23.33	990.	.040	1.10	119.0	4444.	
27123.00 -3.9		4589.	22.47	1145.	048	1.32		4247.	
27124.00 -3.9		4386.	21.57	1197.	.049	1.56	114.4	4053	
27125.00 -3.9		4187.	20.73	1267.	.052	1.80	112.1	3863.	_
27126.00 -3.8		3992.	19.91	1586.	.066	2.07	109.9	3677.	19.23
27127.00 -4.0		3801.	19.01	1883.	•075	2.42	107.3	3494	18.36
27128.00 -4.1		3613. 3431.	18.22	2264.	.089	2.78	105.1	3316.	17.59
27129.00 -4.3		3252.	17.34	2024.	.07A-	3.18	102.5	3142.	
27130.00 -3.9		3077.	16.58	2339.	.089	3.55	100.2	2972.	15.99
27131.00 -4.1		2907	15.78	2497.	.097	3.97	97.7	2806	
27132.00 -4.1		2740.	15.00	2724	.103	4.40	95.2	2644.	14.46
27133.00 -4.2		2578	14.20	2573		4.85	_		13.68
27134.00 -4.0		2420.	13.57	3102.	.115	5.26	90.5	2333.	13.07
27135.00 -4.4		2266	12.72	3070.	-114		87.6	2184.	
27136.00 -4.2		2117.	12.09	3039.	.112	6.20	85.4	2039.	11.62
27137.00 -4.1 27138.00 -4.2		-1971	11.41	- 3243.		6.66	82.9	1897.	10.96
		1830.	10.75	3521.	.131	7.13	80.5	1761.	10.32
_,			10.08	-3372.				1628.	9.67
27140.00 -4.1 27141.00 -4.8		1561.	9.42	4228.		8.11	75.3	1499.	9.03
27142.00 -4.8		1433.	8.71	4295.	.159	8.66	72.3	1375.	8.34
27143.00 -4.3		1311.	8.11	3857.		9.15	69.8	1256.	7.76
27144.00 -4.9	368.8	i i 92.	7.50			.9.65	67.1	1142.	7.17
27145.00 -4.0		1079.	6.89	3669.		10.13	64.2	1032.	6.57
27146.00 -5.3		969.		5262.		10,61	61.8	926.	6.09
27147.00 -5.6		865.	5.65	5648.		11.22	58.1	825.	5.38
27148.00 -5.0		767.	5.10	5123.	.185	-11-71	55.1	730 •	
27149.00 -5.6		573.	4.55	5857.		12.23	52.0	640.	4.31
27150.00 -4.8		585.	4.06	5082.	.183-	12.69	49.1	555.	3.84
27151.00 -5.7		502.	3.58	5155.		13.15	46.0	475•	3.37
27152.00 -5.9		425.	3.06	ti 374 .	.231	13.63	42.5	401.	2.88
27153.00 -6.3		354.	2.59	- 364.	.243	14.09	39.0	333.	2.43
27154.00 -6.1		289.	2.12	-6818.		14.53	35.2	270.	1.498
27155.00 -6.8		230.	1.72	7672.	.285	14.95	31.6	214.	1.59
27156.005.9		178.	1.33	6675.	.238	15.30		165.	1.22
27157.00 -6.9		131.	1.00	7918.		15.63	23.8	120.	•91
27157.50 -4.5		112.	.84	5235.	.188	15.70	21.8	102.	. 76

TEST NO. 27A	MARK II AN	TISKID/SOM	MERS TIRES/W	ET. RUNW	AY	* 1	
			- TEMP	MIND	VEL	WIND	DIREC
	Ed. III	RESS ALT		_	KTS	248.0	DEG MAG
43000 LBS 43	3200 LBS 21	.747 IN HG	1201 C	347	,		
	T	CT DAY			STAN	NDARD D	AY
700 ACCEL C	SND-SPD DIST	KE F	BR UBR	EBR	KTAS	DIST	KE
TOD ACCEL G	148.1 6933.	41.95	0. 0.000	0.00	144.4	6583.	39.69
23665.85 -3.70			811031	÷09	142.2	6366.	38.47
23666.75 -4.37	145.9 6710. 143.5 6466.		775028	.24	139.8		37.20
23667.75 -4.20	140.7 6226.		469 054	•56	137.0	5897	35.73
23668.75 -4.62	138.3 5991.	136.59	660 023	.76	134.6	5670 •	34.50
23669.75 -3.83 23670.75 -4.25	135.9 5759.		357047	1.03	132.2	5446 •	33.24
200100	133.5 5532.		292044	1.32	129.8	5226.	32.05
23671.75 -4.07 23672.75 -3.61	131.0 5309.		786027	1.57	127.3	5011.	30.85
	128.9 5089.	31.77	720058	1.83		4799.	29.83
	126.4 4874.		744058	2.22	122.7	4591.	28.64
	124.0 4563.	29.41 1	716057	2.57	120.3	4388	27.55
	121.9 4455.	28-41 1	183 036	2.86	118.2	4189.	26.59
200100	119.8 4251.	27.46 . 3		3.28	116.1	3993.	25.68
23011013	116.9 4051.		458073	3.89	113.2	3800.	24.39
23678.75 -3.99 23679.75 -4.33			3005090		-111.2		- 23.53 -
	112.1 3664.	24.02 - 2	715080		108.4	3429.	22.37
	110.0 -3477.	23.16 18	361	· 5 • 36·	106.4		21-54
23682.75 -4.29		100 10 0	101	5.92	103.9	3073.	20.54
	105.1- 3113.	21.12 - 3	3841114	~=6.55···	101.4	2901	19.55
23684.75 -4.53	102-4 2939.	20.04	3925116	1.23	70.	51740	10000
	-99.5 2768.	18.92	593135	7.98	95.8		17.48
23686.75 -4.16	96.7 2603.	17.88	3687 108			2412	16.48 15.63
23687.75 -4.24-	94.3 - 2441.	16.99	3914. 1.114		90.6	2100	14.79
23688.75 -4.58	91.8 2284.	16.11	4478131	9.91	88.1	1064	13.84
23689.75 -4.49	88.9 - 2132.	200	4470. 132			1824.	13.06
23690.75 -4.39	86.5 1984.		4442131		2 82•8 79•8		12.11
23691.75 -5.50	83.4 1840.		6048179			1555.	11.16
23692.75 -4.93	80.2 1702.		5388 • 164	12.83	76•6 -73•8		10.38.
23693.75 4.68	77.5 -1569.		5150156	13.51		1308	9.59
23694.75 -4.76	74.6 1441.	-,	5384157	14.19	71.0 67.9		8.77
23695.75 -5.19	71.5 1317.		6063 178	14.91	0, 6,	1079.	8.08
23696.75 -4.55	68.8 1199.		5293155	15.55		974	7.49
23697.75 -4.82	66.3 1085.		5732 169	16.15	59.3	871.	6.70
23698.75 -5.47	63.0 976.		6698 • 200	16.86	56.3	774.	6.03
23699.75 -5.11	59.9 872.		6318 • 185	17.52	53.1	682	5.37
23700.75 -5.15	56.7 774.	7	6449191	18.16	50.2	596.	4.81
23701.75 -5.07	53.8 681.		6423188	18.73 19.34	46.9	514.	4.19
23702.75 -5.42	50.5 592		6972205	19.86	44.2	439.	3.72
23703.754.98	47.8 510.		6448190 7648226	20.42	40.9	368.	3.18
23704.75 -5.82	44.4 432.	T	7648 • 226 8566 • 255	21.00	37.2	302.	2.63
23705.75 6.45	40.8 360		7936233	21.54	33.4	243.	2.12
23706.75 -5.92	36.9 294	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	5058153	21.82	30.4	193.	
23707.70 3.75	33.9 238	£ + £ 0	20201 4123				

TEST NO. 278	MARK	II ANTIS	(ID/SOMMERS	TIRES/V	ET RUNWA	AY		
STAND WGT	TEST WGT	PRESS	ALT	TEMP	WIND	VEL	WIND	DIREC
STAND WGT 38000.LBS	38350 LBS			14.2 C	5.7		230.0	DEG MAG
						STA	NICLARIN IN	AV
				UBR	EBR	KTAS	DIST	KE
		DIST KE			0.00		5731.	31.33
26042.34 -3.6				0.000 .036		.134.3	5527.	30.36
26043.25 -4.5			.73 820. .43 -1078.		•33	131.6	5306	
26044.25 -4.6			43 1078 09 1030	.043	.62	128.7	5088.	27.88
26045.25 -4.3			13 603		.75	126.6	4878	26.98
26046.25 -3.8			93 1172		1.00	124.0	4669.	25.87
26047.25 -4.2		_	88 1098	.043	1.25	121.6		24.89
26048.25 -4.0			85 1385	.054	1.53	119.2	4266.	23.92
26049.25 -4.1			84 1689	.065	1.84	116.9	4070	22.98
26050.25 -4.2		4339. 24		.069		114.2	3878.	21.93
26051.25 -4.1		-	84 1682			-112.0	3692.	21.12
26052.25 -3.9 26053.25 -4.1			81 2098		2.97	109.5	3508.	20.16
	-		84 2761		3.44	107.0	3329.	19.26
26054.25 -4.5 26055.25 -3.7			87 1990.		3.89	104.5	3154.	18.36
26056.25 -4.4			06 2883.		4.32	102.3	2983.	17.61
26057.25 -4.6			99 3316.		4.93	99.4	2815.	16.62
26058.25 -4.5			.09 3273.		5.49	96.9	2653.	
26059.25 -3.9			.17 2783.	.093	6.01	94.2	2495.	14.94
26060.25 -4.2			.41 3197.	.108	6.49		2341.	14.24
26061.25 -4.4	_		.50 3508.	.120	7.08	89.3	2191.	13.40
26062.25 -3.8		2352. 14	.76 2939.	.099	7.56	87.0	2046.	12.72
26063.25 -4.6	2 90.6	2196. 13	.93 3984.		8.13	84.3	1904.	11.96
26064.25 -4.7			.10 4271.		8.76	81.6	1767	10.50
26065.25 +3.8	_		.33 3273.		9.30	79.0	1635.	9.91
26066.25 -4.2		1758. 11	.68 3841.		9.79	76•7 73•7	1382.	9.15
26067.25 -5.3			.85 5210.		10.45		1262	8.47
26068.25 -4.5	-		.09 4359.		11.06	68.1	1147.	7.81
26069.25 -4.8			•37 4913•		11.66 12.24	65.4	.1037.	7.20
26070.25 -4.6			.69 4716.		12.87	62.5	931	6.56
26071.25 -5.5			.98 5908. .21 5666.		13.53	59.1	830.	5.87
26072.25 -5.2			.21 5666. .58 5356.		14.11	56.2	735.	5.31
26073.25 -4.9			.95 5733		14.67	53.2	646.	4.76
26074.25 -5.2			24 6761		15.31	49.6	559.	4.13
26075.25 -5.9			66 6244		15.87	46.4	480.	3.62
26076.25 -5.4			.07 7048	_	16.44	43.0	406.	3.11
26077.25 -6.0			·52 6533		16.97	39.6	338.	2.64
26078.25 -5.5 26079.25 -5.9			.01 7005		17.46	36.2	275.	2.21
			.54 7660		17.94	32.8	218.	1.81
			99 8989		18.46	28.4	166.	1.36
26081.25 -7.4 26082.25 -6.4		_	56 7853		18.89	24.5	122.	1.01
26083.25 -7.2		-	.16 8875		19.29	20.4	84.	.70
26084.25 -4.5			.84 5639		19.57	16.4	- 54.	.45
26084.54 -3.4			.80 4350.	.134	19.58	16.0	47.	.43

DUBLISHAY

TEST NO. 2	7.0	MARI	K II AN	TISKIDVS	OMMERS T	TIRESYW	ET RUNW	AY		
IEST NO. Z	, с						1		WIND	DIREC
STAND WGT		TEST WGT	- P1	RESS AL	•	TEMP	WIND	KTS	230.0	DEG MAG
34000.L85	34	4550.LBS	27	757 IN	HG 10	0.00	۵,• د.			
				T DAY				STA	D GRADIN	AY
	ACCEL /	GND-SPD	DIST	, k€	FBR	UBR	EBR	KTAS	DIST	KE,
		135.0	5493.	27.86	346.	.016	-01	128.1	4894	24.68
	-4.14 -4.53	132.8	5298	26.95	914.	. 43	.16	125.9	4715.	23.84
		130.1	5076.	25.90	470.	.021	.32	123.3	4511.	22.88
201111	-3.95 -4.07	127.9	4359.	25.03	719.	.033	.42	121.1	4311.	22.07
200,010	-4.66	125.3	4645.	24.02	1523.	.068	.68	118.5	4115.	21.15
	-4.55	122.5	4436.	22.95	1556.	.069	1.02	115.8	3923.	20.17
F001F1-0	-3.98	120.0	4231.	22.04	1125.	.049	1.27	113.3	3735•	19.33
	-4.23	117.7	4031.	21.20	1571.	.066	1.53	111.1	3553	18.56
	-4.47	115.0	3834.	20.24	2013.	₽ 083	1.90	108.4	3373.	
28095.00 28096.00	-4.79	112.2	3542.	19.25	2488.	.103	2.37	105.6	3197.	16.78
28097.00	-4.10	109.6	3455.	18.38	1963.	•077	2.76	103.1	3027.	15.98
	-4.53	106.9	3272.	17.47	2564.	.101	3.21	100.3	2859	15.15
28099.00	-3.94	104.6	3094.	16.72	2042.	.080	3.59	98.0	2698	14.47
28100.00	-5.08	101.7	2920.	15.83	3440.	.132	4.12	95.3	2539.	12.90
28101.00	-4.38	99.0	2751.	15.00	2798.	.108	4.62	92.6	2386.	12.14
28102.00	-4.47	96.2	2586.	14.15	3031.	•116	5.12	89.8	2236.	11.54
28103.00	-4.31	93.9	2425.	13.49	2930.	.114	5.55	87.6	1950	10.82
28104.00	-4.68	91.1	2269.	12.70	3476.	• · · · · · · · · · · · · · · · · · · ·	6.08	84.8	1814.	10.21
28105.00	-4.07	188.6	2117.	12.02	2916.	-111	6.53	-82.4	1683.	9.62
28106.00	-4.45	86.2	1970.	11.36	3434.	.128	6.99	79.9	1554	8.93
	-4.68	83.2	1527.	10.60	3786.	•143	7.53	77.0 74.5	1430	8.35
28108.00	-4.19	80.7	1588.	9.95	3365.	.125	8.01 8.46	72.2	1312.	7.85
28109.00	-4.55	78.4	1554	9.39	3828.	•144	9.04	69.2	1196.	7.20
28110.00	-5.43	75.3	1424	8.67	4864	188	9.62	66.1	1085.	6.58
28111.00	-4.99	72.2	1299.	7.97	4506.	•172 •160	10.11	63.4	980.	6.05
28112.00	-4.56	69.4	1180.	7.37	4125	•184	10.63	60.6	878.	5.52
28113.00	-5.18	66.6	1065.	6.78	4892	•169	11.14	57.7	783.	5.00
28114.00	-4.72	63.6	956.	6.19	4483	164	11.59	55.0	691 .	
28115.00	-4.52	60.9	851.	5.67	4349. 5773.	• 226	12.10	52.1	604.	4.09
28116.00	-5.79	58.0	750.	5.14	5982	.226	12.67	48.4	521.	3 • 53
28117.00	-5.88	54.2	655.	4.50 3.97	6029	235	13.18	45.1	445.	3.07
28118.00	-5.86	50.9	566.		6588	-245	13.71	41.5	374.	2.59
28119.00	-6.29	47.2	483.	3.41 2.92	6090	.226	14.18	38.0	309.	2.17
28120.00	-5.75	43.7	407.		6528	.238	14.62	34.6	249.	. 1.80
28121.00	-6.09	40.2	336.	2.47 2.05	6828	.257	15.04	31.0	196.	1.45
28122.00	-6.32	36.6	271.	1.65	6868	251	15.43	27.3	148.	. 1.12
28123.00	-6.29	32.8	212.	1.05	7607.	299	15.80	23.4	107.	.83
28124.00	-6.95	28.9	160.	. 95	7501	.293			72.	
	6.80	24.9	115.	.64	8766	.332	16.44	15.0	43.	
28126.00	-7.92	20.4	76 . 46 .	.41	5186	.196	16.62	11.0	22•	•18
~~~	-4.55		42.	.39	4667.	.175	16.62	10.7	20.	•17
28127.14	-4.06	16.0	76.	- :						-

TEST NO. 284	ФАНК	[i] ANT	15×10/9	SUMMERS	THEST	WEI HUNW	AY		
STAND MGT	TEST WGT	بإخا	ESS 4	LÏ	TEMP	WIND	VEL	WIND	DIREC
43000 LBS	43500.655		760 IN		12.h C	-	KTS		DEG MAG
450000000					н				
		TES	T DAY-				• • •	ANDARD (	
TOD ACCE	L GNU-SPD	DIST	ĸ£	<b>ਜੰਜੇ</b> ਜ਼	UAR	ERR	KTAS	DIST	KE
22962.89 -4.3	8 153.4	7240.	45.34	U •	0.000	0400	150.2	6876	42.92
22963.75 -4.1	2 151.0	7025.	43.94		0.000	0.00	147.8	6663	41.57
22964.75 -3.9	7 146.4	6773.	42.42		0.000	•	145.2	6420.	40.11
22965.75 -4.5	7 140.0	5524.	41.06		0.000	0.00	142.8	6181.	38.80
22966.75 -4.1	0 143.2	.0350	39.49	0.	0.000		140.0	5946	37.29
22967.75 -3.6	1 141.2	6040.	38.39	280.	•009	•02	138.0	5716.	36.24
22968.75 -4.2	8 138.7	5603.	37.03	1154.	• 042	• 50	135.5	- 5489	34.93
22969.75 -4.1	0 136.4	5572.	35.05	1113.	• 11 3 8	•47	133.2	5267.	33.80
22970.75 -4.0	5 133.7	5344.	34.46	1245.	.1147	•,81	130.5	5048	32.43
22971.75 -4.0	7 131.7	5120.	33,411	1397.	• 046	1.03	128.5	4834.	31.45
22972.75 -4.8	4 120.8	4900.	31.795	2665.	<b>.</b> 0∂6	1.55	125.7	4622.	30.06
22973.75 -4.2	4 125.1	4585.	30.02	2015.	• 955	2.04	123.0	4416.	28.78
22974.75 -4.3	0 123.7	4474.	24.47	2342.	.074	2.48	120.6	4214.	27.67
22975.75 -4.2	9 171.0	42c7.	28.18	2604.	• u78	3.04	117.8	4016.	26.44
22976.75 -3.9	6 118.6	4065.	27.08	2297.	•068	3.50	115.5	3823.	25.39
22977.75 -4.2	8 115.1	3567.	25.95	2877	• 084	4.04	113.0	3634.	24.30
22978.75 -4.4		3573.	24.80	3209.	. 195	4.65	110.4	3448.	23.21
22979.75 -3.7		3484.	23.61	2425.	.070	5.14	108.1	3268.	22.26
22980.75 -4.8		3290.	22.50	3268.	.097	5∙ธฮ	105.8	3091.	21.29
22981.75 -4.2		3117.	21.71	3324.	.099	6.29	103.2	2918.	20.26
22982.75 -4.6		2934.	20.64	4041.	.118	6.94	100.6	2748	19.28
22983.75 -4.0		2707.	19.63	3377.	.098	7.59	97.9	2584.	18.26
22984.75 -4.5		2594.	10.71	4104.	.123	8.55	95.6	2424.	17.39
22985.75 -4.6		2435.	17.55	4350.	.127	8.96	92.6	2268.	16.31
22986.75 -4.8		2476.	16.53	4935.	•141	9.69	89.9	2117.	15.37
22987.75 -5.1		2121.	15.50	5273.	.156	10.48	86.8	1970.	14.34
22988.75 -4.9		1972.	14.49	5194.	.152	11.27	8.68	1828.	13.37
22989.75 -4.6	6 84.1	1828.	13.62	4384.	-146	11.96	81.2	1692.	12.55
22990.75 -5.1	1 81.1	1584.	12.05	5016.	.166	12.71	78.2	1559.	11.63
22991.75 -4.6		1554.	11.74	~5048°	.149	13.41	75.3	1432	10.80
22992.75 -4.8		1424.	10.93	5450.	.158	14.08	72.7	1310.	10.05
22993.75 -4.7		1300.	10.16	5497.	.160	14.76	69.8	1192.	9.27
22994.75 -5.7	8 69.0	1180.	9.20	6934.	.206	15.53	66.5	1079.	8.42
22995.75 -5.6		ໄມ້ຄວ້•	8.37	6811.	-198	16.32	63.1	971.	7.58
22996.75 -4.9		957.	7.51	5990.	•173	16.98	60.1	869.	6.87
22997.75 -5.7		553.	6.50	7204.	.207	17.66	57.1	771.	6.20
22998.75 -5.6	7 56.5	755.	6.15	7192.	.206	18.36	53.7	680.	5.50
22999.75 -5.8		562.	5.40	7484.	.216	19.03	50.2	593.	, 4.80
23000.75 -6.2		575.	4.70	8156.	.634	19.71	46.7	512.	4.15
23001.75 -4.7		496.	4.12	6252.	.181	20.26	43.6	438•	3.61
23002.54 -3.9		435.	3.71	5163.	.140	20.50	41.2	382.	3.23
				-					

## COPY AVAILABLE TO DRG DOES NOT PERMIT FULLY LEGIBLE PROBLETION

STAND HGT		TEST MGT		.765 1	ALT N HG	TEMP 16.9 C	WIND 3.0	VEL KTS		DIREC DEG MAG
38000 LHS								ст	ANDARD D	ΔΥ
			TE		FRY	Uer	EBR	KTAS	DIST	KE
TOD		GN-SPD	015T	KE.		0.000	0.00	135.4	5460.	30.82
2500A.91	-3.34	134.2	55+1.	33.04		-029	.10	133.3	5275.	29.88
25009.75	-4.31	137.1	5545.	32.05		.019	.22	130.8	5058.	28.79
25010.75	-3.98	134.6	5415.	30.40	the second secon		.43	128.3	4844.	27.69
25011.75	-4.37	132.1	5190.	29.14			.52	126.2	4636.	26.79
25012.75	-3.53	130.0	4970 .	29.79		.045	.71	123.9	4431.	25.81
25013.75	-4.15	127.6	4752.	27.75		.035	.91	121.6	4230.	24.87
25014.75	-3.85		4539.	26.75	1034	.039	1.12	119.3	4032.	23.94
25015.75	-3.81	123.0	4329.	25.77		.048	1.35	117.1	3838.	23.08
25016.75	-3.89		4123.	24.86		.069	1.70	114.8	3648.	22.15
25017.75	-4.22	116.4	3455.	23.68		.064	2.08	112.2	3462.	21.19
25018.75	-3.49		3725.	55.36		.082	2.52	109.7	3280.	20.23
25019.75	-4.28		3531.	21.84	10 mm 1 m	1 200,000	3.02	107.2	3101.	19.32
25020.75	-4.48		3342.	20.67		and the state of t	3.47	104.7	2928.	18.46
25021.75	-4.08		3157.	19.95			4.01	102.0	2758.	17.51
25022.75	-4.64	105.5	2977.	18.45			4.62	99.4	2593.	16.61
25023.75	-5.04		5501.	18.00			5.29	96.3	2432.	15.60
25024.75	-4.87		2530.	16.43		100000000000000000000000000000000000000	5.88	93.6	2276.	14.75
25025.75	-4.63		54044	16.00	3540.		6.47	91.0	2124.	13.92
25026.75	-4.72	94.3	5303.	15.14			7.10	88.3	1978.	13.11
25027.75	-5.17		2146.	14.67			7.73	85.0	1835.	12.17
25028.75	-4.11	64.2	1995.	13.27			8.27	82.9	1698	11.55
25029.75	-5.18		1847.	12.00	4727.		8.96	79.4	1563.	10.59
25030.75	-4.75		1705.	11.59		The second second	9.53	77.1	1436.	10.01
25031.75	-5.03		1564.	10.97			10.18	73.9	1312.	9.18
25032.75	-4.81	75.9	1435.	10.09			10.76	71.4	1193.	8.57
25033.75	-5.06	74.4	1307.	9.4			11.44	68.0	1078.	7.77
25034.75	-5.15		1185.	8.56			12.02	65.2	969.	7.15
25035.75	-5.14		1067.	7.9			12.70	61.8	864.	6.43
25036.75	-5.91		955.	7.13		The second second	13.36	56.5	766.	5.76
25037.75	-5.65		948.	6.4			13.94	55.3	673.	5.14
25038.75	-5.10		748.	5.7			14.44	52.3	585.	4.61
25039.75	-4.72		553.	5.1			15.01	49.4	501.	4.10
25040.75	-6.31		562.	4.0			15.64	45.4	423.	3.47
25041.75	-6.64		477.	3.94			16.20	41.5	352.	2.90
25042.75	-6.07		390.	3.3			16.74	38.0	286.	-2.42
25043.75	-7.12	+0.5	327.	2.8			17.24	34.0	227.	1.95
25044.75	-6.39		263.	2.00			17.72	29.8	174.	1.49
25045.75	-7.3		294.	1.7		100 100 100	18.16	25.9	128.	1.12
25046.75	-7.30	S.42	153.	1.3		1.500	18.37	55.5	90.	.83
25047.75	-2.59	24.6	110.	1.0	3 3270.	109	10.31	CC.		- 1

STAND VGT		TEST WOT	0	PESS I	AL T	TEMP	WIND	VEL		DIREC
34000.L95		34450.L35		.759 I	1 40	17.7 C	2.6	KTS	225.0	DEG MAG
3400000				2000						
								The state of the s	ANDARD I	
TOD	ACCEL	GND-SPD	DIST	KE	EB3	1168	EBR	KTAS	DIST	KE
85.88695	-3.84	131.0	4731.	26.18	119.		.01	126.5	4373.	24.10
26989.25	-4.04	128.7	4525.	25.25	503.		.09	124.2	4174.	23.22
26990.25	-3.98	126.4	4309.	24.36	571.	71.674	.50	122.0	3972.	22.39
26991.25	-3.91		4095.	73.42	511.		•32	119.7	3775.	21.56
26992.25	-4.31	121.6	3591.	22.55	1213.		.53	117.2	3581.	20.69
26993.25	-3.83		3558.	21.70	831.		.72	115.0	3391.	19.89
26994.25	-4.94	116.7	3444.	20.76	5190		1.05	112.4	3205.	19.01
26995.25	-4.75		3294.	19.75	2181.		1.47	109.6	3023.	18.06
26996.25	-4.96		3104.	14.71	5686.	.10A	1.96	106.6	2846.	17.09
26997.25	-5.27		2919.	17.77	3184.		2.49	103.8	2673.	16.22
26998.25	-4.98		2740.	16.72	3045.	.120	3.06	100.6	2506 •	15.24
26999.25	-5.29		2565.	15.63	3526.	.137	3.61	97.8	2343.	14.40
27000.25	-5.87		2397.	14.80	4306.	.167	4.30	94.5	2185.	13.44
27001.25	-5.28		2233.	13.84	3925.	.147	4.94	91.3	2033.	12.55
27002.25	-5.75		2075.	12.88	4462.	.175	5.52	88.0	1885.	11.65
27003.25	-4.70		1923.	12.05		.133	6.19	85.0	1744.	10.87
27004.25	-5.58		1775.	11.24	4544.	.172	6.79	82.0	1607.	10.12
27005.25	-5.42		1533.	10.34	5031.	.195	7.48	78.6	1475.	9.29
27006.25	-5.61		1497.	9.47	4847.	.183	8.16	75.1	1348.	8.49
27007.25	-5.10	The second second	1367.	8.77	4407.	.168	8.73	72.1	1228.	7.83
27008.25	-5.79		1241.	A.03	5266	.196	9.34	69.0	1112.	7.16
27009.25	-5.14		1122.	7.31	4664	.177	9.94	65.6	1001.	6.49
27010.25	-5.45		100%	6.70	5088.	.148	10.47	62.7	897.	5.93
27011.25	-6.64		594.	5.96	6475	. 251	11.13	59.0	796.	5.24
27012.25	-5.04		797.	5.24	4894.	.186	11.70	55.4	702.	4.63
27013.25	-5.33	The second secon	699.	4.80	5266.	.199	12.17	52.7	614.	4.18
27014.25	-6.02		508.	4.21	6089.	. 234	12.70	49.2	530.	3.65
27015.25	-6.24		522.	3.64	6417.	. 245	13.24	45.6	452.	3.13
27016.25	-6.53		442.	3.11	6810.	. 565	13.75	41.9	379.	2.64
27017.25	-6.03		369.	2.63	6352	. 244	14.21	38.3	314.	5.21
27018.25	-6.74		302.	2.17		. 270	14.56	34.6	253.	1.90
27019.25	-6.34		242.	1.77		195.	15.06	31.0	200.	1.44
27020.25	-7.04		187.	1.35			15.46	26.8	152.	1.08
27021.25	-4.91		141.	1.04			15.75	23.2	111.	.81
27021.83	-3.39		116.	.43		The second of the second	15.81	21.8	90.	.72

TEST NO. 294		MARK	III AM	TISK1	DISOMME	us.	TIKES!	WET RUNY	VΔΥ		
STAND WGT		TEST WGT		CO. 10 10 20 11	ALT IN HG	1000	TEMP		VEL KIS		DIREC DEG MAG
Jan Sale and		Dinon	TE			10		10000	STA	ANDARD D	ΑΥ
700	CEL	GMD-SPD	DIST	KE	FHR		UBR	EBR	KTAS	DIST	KE.
			7441.	41.2		0.	0.000	0.00	144.5	6699.	36.97
THE RESERVE OF THE PARTY OF THE	3.43	151.7	7210.	40.2	Charles I Francisco		550.	.03	142.6	6492.	35.99
Comment of the Commen	.56	149.9		38.7	STATE SHOULD BE CARD		.005	.16	139.9	6259 .	34.63
The second secon	50.	147.0	6966. n720.	37.4		4 1	.027	.26	137.5	6031.	33.47
	.36	144.6		35.2		4.	.004	.35	135.1	5807.	32.32
5 - CO TO THE REST OF COMMENT AND ADDRESS OF THE PARTY OF	3.75	142.2	6474.	35.1			.013	.40	132.9	5587.	31.26
	3.42	139.9	6240.	33.9			.032	.58	130.5	5370 .	30.15
	+.07	137.5	6005.	and the second second	Committee of the Commit		.016	.67	128.5	5159.	29.22
The Transport of the Section 1999	3.63	135.5	5775.	32.9	The second second second	0.	0.000	.72	126.3	4951.	28.26
	3.18	133.3	5540.	31.8	THE POSSESSED FOR THE PARTY OF		.059	.90	124.4	4746.	27.42
	.36	131.4	5325.	30.9		0.	0.000	1.03	122.1	4545.	26.41
**************************************	.19	129.0	5167.	29.5	The second second second		.054	1.17	120.6	4347.	25.74
	+.29	127.5	4889.	29.1				1.57	117.9	4151.	24.60
THE RESERVE OF THE PARTY OF THE	3.78	124.7	4577.	27.9			.046	1.97	115.6	3960.	23.66
	+.55	4.551	4465.	25.8			.086	2.46	113.0	3772.	22.60
THE RESERVE THE PARTY OF THE PA	+.08	119.8	4264.	25.7			.072	2.92	110.6	3589.	21.66
	.16	117.4	4064.	24.7			.100	3.49	107.9	3409.	20.63
	+.56	114.7	3867.	23.5	Committee of the commit			4.10	105.3	3233.	19.62
	+.58	111.9	3575.	22.4			.104	4.53	102.9	3063.	18.76
	3.30	109.6	3490 .	21.5	2 175		.106	4.99	100.9	2897.	18.02
	+.46	167.5	3396.	20.7			The second second second	5.51	98.4	2734.	17.15
	3.76		3127.	19.7			.061		96.0	2575.	16.32
	4.40	102.6	2952.	18.8			.110	6.06	93.6	2420	
	3.77	100.2	2751.	17.9		-	.130	7.19	91.1	5568	14.70
	4.74	97.6	2513.	17.0			.113	7.80	88.5		:13.98
	4.22	95.0	2451.	16.1			.138	8.45	85.9	1978.	13.06
	4.74	92.3	5563.	15.0			.133	9.08	83.3	1840.	12.27
	4.53	10.75.02.5	2139.	14.4			.157	9.80	80.3	1705.	11.42
THE COURSE OF TH	5.03	86.6	1990.	13.4			.140	10.41	77.9	1576.	10.74
	4.52	84.2	1547.	12.7			.179	11.16	74.6	1450.	9.86
Market Street St	5.45	80.9	1707.	11.7			.153	11.83	71.8	1330 .	9.13
MINIOCOLO DE LA NEW	4.68	78.0	1573.	10.9			The state of the s	12.44	69.4	1215.	8.53
	4.89	75.6	1444.	10.2			.164	13.10	66.0	1103.	7.71
	5.20	72.1	1319.	9.3				13.45	62.9	997.	7.01
The second secon	5.23	69.0	1500.	8.5			.183	14.45	60.2	897.	6.42
	4.30	66.3	1086.	7.8			-169	15.07	57.3	800.	5.81
	4.93		977.	7.1			-177	15.66	54.4	709.	5.24
	4.99		872.	6.5			.182	16.27	51.3	622	4.66
	5.27		773.	5.5	Total Particular		.195		48.1	541.	4.10
	5.07		579.	5.4			.190	17.40	45.2	465.	3.61
M. M. M. T. T. T.	5.40		590.	4.5			.205	17.96	41.9	393.	3.11
The second secon	5.90		507.	4.1				18.55	38.1	326.	2.58
	6.30		429.	3.4					34.9	267.	2.16
	5.94		358.	2.9				19.06	31.1	515.	1.71
	6.49		293.	5.4					27.4	163.	1.33
	6.63		234.	1.5				20.04	23.4	121.	.97
	6.19		181.	1.:				20.47	21.1	92.	.79
23303.57 -	3.16	26.6	144.	1.0	27 417	1.	.128	20.52	21.1	76.	

TEST NO. 29H	MARK	III AN	FISKIDZSOMMER	S TIRES!	WET RUNW	YAI		
÷ -34		· Pi	1.	TEMP			WIND	DIREC
STAND WGT	TEST WG1		697 IN HG	18.7 C	4.1	KTS	219.0	DEG MAG
	6375.LBS		PAL IN UU	10000	64			
*** *** *** *** *** *** *** *** *** **		TE	5T ()AY			STA	INDARD D	
		ATOT	KE FAK.	UER	EBR	KTAS	DIST	KE
	GNL-SPD -	5721.	30.82 521	024	01	132.0	5182.	27.79
	138.3	5520.			.18	129.6	4995	26.76
25670.00 -4.02		5292.	28.80 595		. 22	16103		25.92
25671.00 -4.11	133.7	5069.		. 030	43	124.9	4577.	
		4850.		. 0.000	- 45	1-040	4375	24.10
25673.00 -3.27		4533.	25.92 813		•56		4175	23.24
			24.90 1986	081	.88	118.3	3979.	22.30
		4213.	23.81 1553		1.25		. 3787.	21.29
		4010	22.79 2151		_/l63	113.0	3599.	20.35
	116.5		21.85 1808		2.00	110.6	3416.	19.48
2001000	114.1	3517.	20.45 2014		2.37	108.2		18.64
25679.00 -4.17		3427.	20.03 216		2.77	1030,		17.80
230000		3240.	19.16 2542	091	3.21	103.3		17.00
25681.00 -4.37	106.4	3058.	18.23 2809	101	3.71	100.6	2724.	16.14
LD00mt-1	103.7		17.33 3455	124	4.25	98.0		15.31
25683.00 -4.95	160.5	2709.	16.26 - 379	138	4.92		2402.	14.32
	97.8	2541.	15.39 2992	. 107	5.45	92.1	.: 2248 ·	13.53
23003403	95.2	2373.	14.59 /3756		6.00		-2100 ·	× 12.80
25686.00 -4.88		5551.	13.66 419	-	6.65	86.6	1955.	11.94
2300.00		2067.	12.78 416		7.28	83.6	1815.	11.14
25688:00 -5.01		1920.	11.97 - 389	140	7.HB			10.40
		1777.	11.28 - 316		.8.36	78.3	1551.	9.77
25690.00 =3.94		1537.	10.58 467		8.92	75.7	1425.	9.14
25691.00 -5.18		1503.	9.75 418		9.54	72.5	1303.	
25692.00 -4.66		1374.	9.13 479		10.09	70 ₽0	1187.	7.82
25693.00 -5.11	75.3 71.9	1250.	8.32 486		10.72	66.7	1074.	
25694.00 -5.07		1131.	7.57 538		11.31	63.9	967.	6.50
25695:00 -5.45	69.0 65.7	1017.	6.95 554		11.43	60.6	865.	5.86
25696.00 -5.49		909.	6.30 548		12.52	57.5	768.	5.27
25697.00 -5.37	62.6 59.2	506.	5.65 571	-	13.10	54.2	676.	
25698.00 -5.48		704.	5.08 555	5 . 146	13.63	51.2	590•	4.18
25699.00 -5.27	56.2 52.9	517.	4.50 611		14.17	48.0	50分•	3.67
25700.00 -5.70	49.3	530 ·	3.91 693		14.73	44.4	433.	3.15
25701.00 -6.35	45.6	450.	3.35 634		15.25	40.B	362•	2.66
25702.00 -5.75	42.2	376.	2.67 668		.15.72	37.5	293.	2.24
25703.00 -6.00		30⊁.	2.40 737		16.19	34.0	240.	1.84
25704.00 -6.55	38.6 34.6	240	1.42 765		16.65	30.0	186.	1.43
25705.00 -6.72	34.1	191.	1.51 779		17.00	26.1	140.	1.09
25706.00 -6.79	26.8	143.	1.16 746		17.41	22.3	101.	
25707.00 -6.45 25708.00 -5.67	55.8	101.	83 662		17.71	18.4	67.	•54
	20.5	74.	70 399		17.80	16.5	48.	•44
25708.73 -3.32	20.7	, - •						

TECT NO. 204	MARK ITT ANT	ISKID/USAF T	IRESZWET RUNWA	Y	
TEST NO. 30A			TEMP WIND		DIREC
	T WGT PPES			KTS 225.	DEG MAG
43000.LBS 4300	U.LBS 27.59	5 IN HG 1	100		1
	TOOT	_ ~} .\{\		STANDARD	DAY
	-spo nisi k	E FBK	UAR EBR	KTAS DIST	KE
TOD ACCEL GND	310			150.0 8217	
2001/00/	200		0.000 -0.00-	147.9 7990	• 41.64
50000 BD0			0.000 0.00	145.8 7745	
23001.00		3.96: 104.	.004 .13	143.0 7500	
73005030			0.000 .13	141.0 7264	• '37.87
2300040	7	.42 310.	.011 .22	138.6 7029	
		.27 - 137.	.005 .24	136.5 6800	
23003430		9.11 408.	.015 .30	134.4 6574	
57000120		7.83 561.	.021 45	132.1 6351	. 33.22
E3001.030			0.000 -48	130.1 6133	
52000000	1205 51	5.64 1141.	.040 .64	128.0 5917	
23037430		4.43 1213.	.04293	125.7 5704	
200,0000		3.25 1796	.062 1.27	123.4 5496	
23071030	1404	1.94 1275.	.043 1.64	120.8 5290	
230,200		0.97 1086.	037 1.87	118.8 5090	
2307300		0.04 1660.	.056 . 2.10	116.9 4895	
23024000	m4 4: 3	8.83 2204.	.073 -2.60	114.4 4700	
23073400		7.63 2731.	.OHB 3.15	111.8 4509	
230,000		6.73 1031.	.033 3.46	109.9 4325	
53011420 mm		5.87 2076.	.006 3.78	108.0 4145	
53030430		4.84 2747.	.089 - 4.26	105.7 3966	
23099930		3.86 2794.	.086 4.78	103.4 3791	
2310000		2.60 3584.	.112 5.39	100.9 3619	
7310100		1.80 2525.	.078 5.94	98.5 3451	
53105430		1.06 2208.	.068 6.31	96.7 3290	
E3103430 GAILE		0.16 3621.	.110 6.85	94.5 3130	
		9.33 2435.	.074 7.35	92.3 2979	
5210300		8.57 3185.	.096 7.81	90.4 2824	
L310300.	,,,,,,	7.58 3815.	•113 8•44	87.7 2673	-
23101031	) U =	6.82 2882.	.088 8.94	85.6 2529	
23/00/00	,,,,,	6.06 4248.	.127 9.51	83.5 2388	
53107030		5.13 3590.	.106 10.13	80.9 224	
23110100	87.3 2551. 1	4.49 2335.	.086 10.57	79.0 2118	
[3111430		3.89 3979.	.119 11.06	77.2 1989	
23112.50		3.05 4131.	.124 11.67	74.6 186	
C3113150		2.38 3954.	.119 12.20	72.4 174	
23/14130		1.69 3920.	.117 12.73	70.2 162	
23113439		1.06 3620.	.104 13.23	68.1 150	
23/10430		0.56 3191.	.095 13.63	66.3 139	_1
23/1/13/	72.2 1610.	9.92 4249.		64.1 128	
23/13/20 34.4	70.0 1489.	9.33 4534.		61.9 118	
	67.8 1373.	8.75 3091.		59.8 108 59.6 107	
23120030	67.6 1358.	8.71 2671.	.077 15.05	59.6 107	C. U.13

1231 NO. 300	3								
STAND WGT	TEST WGT	رو	PESS AL	T	TEMP	WIND	VEL	WIND	DIREC
38000.LBS	38200.LBS		.592 IN		20.0 C		KTS	235.0	DEG MAG
20000111111	307 40 1235	٠,	• 3 / 2 • 1				*		
		TF	ST DAY				ST	ANDARD (	)AY
	_ GND-SPD	DIST	KE	FäR	UAR	EBR	KTAS	UIST	KE
26088.73 -3.7		7082.	33.97		0.000	0.00	133.8	6317.	30.12
26089.50 -4.0		6898.	33.10	456.	.019	•05	132.0	6147.	29.32
26090.50 -3.9		6564 .	31.98	437.	.018	•17	129.7	5931	28.28
26091.50 -3.4		6434.	30.96	14.	.001	.20	127.5	-5719.	27.35
26092.50 -3.4		6207.	30.08	129.	•005	.51	125.6	5511.	26.54
26093.50 -4.2		5984	29.10	1294.	.051	•39	123.5	5306.	25.64
26094.50 -3.4		5765.	28.01	474.	.019	.60	121.0	5104.	24.64
26095.50 -2.9		5550 .	27.60	0.		.63	129.2	4907.	23.89
26096.50 -3.4		5337.	26.44	734.	.628	.71	117.4	4713.	23.19
26097.50 -3.6		5128	25.51	1043.	.039	.93	115.2	4522.	22.34
26098.50 -3.4		4922.	24.02	1019.	.039	1.16	113.1	4333.	21.53
26099.50 -3.7		4720.	23.86	1521.	.056	1.40	111.3	4150.	20.83
26100.50 -4.3		4522.	22.79	2441.	.088	1.86	108.6	3967.	19.85
26101.50 -3.9		4328.	21.64	2078.	.073	2.29	106.2	3790 .	18.99
26102.50 -4.2		4136.	20.98	2551.	.087	2.71	104.0	3617.	18.20
26103.50 -4.2		3952.	19.89	2793.		3.26	101.1	3445.	17.21
26104.50 -2.9		3771.	19.24	1258.		3.55	99.4	3282.	16.62
26105.50 -4.5		3593.	18.39	3292.		4.03	97.0	3120.	15.84
26106.50 -3.9		3419.	17.54	2665.		4.52	94.6	2961.	15.06
26107.50 -3.9		3249.	16.71	2785.	.095	5.00	92.3	2807.	14.32
26108.50 -3.5		3083.	16.07	2444.		5.39	90.4	2658	13.73
26109.50 -4.5		2920	15.21	3699.		5.94	87.8	2510	12.96
26110.50 -3.7		2763.	14.48	.2866.		6.43	85.5	2368.	12.30
26111.50 -3.6		2609.	13.73	2371.	.097	6.89	83.1	2229.	11.62
26112.50 -4.4		2458.	13.06	3868.		7.39	80.9	2094•	11.01
26113.50 -3.7		2312.	12.26	3185.	.108	7.93	78.3	1962.	
26114.50 -3.3		2170.	11:78	2743.	.093	8.29	76.6	1836.	9.86
26115.50 -4.3		2031.	11.08	4010.	.133	8.81	74.1	1712.	9.24
26116.50 -4.5		1897.	10.42	4360.	.147	9.35	71.7	1592.	8.66
26117.50 -3.7		1767.	9.55	3486.	.117	9.90	68.8	1475.	7.97
26118.50 -4.1		1641.	9.16	4021.	•137	10.34	66.9	1364.	7.53
26119.50 -3.6		1519.	8.54	3505.	.117	10.81	64.4	1256.	6.98
26120.50 -4.8		1399.	7.99	5068.		11.31	62.1	1152.	
26121.50 -3.7	4 66.2	1286.	7.41	3795.	_	11.79	59.6	1052.	5.98
26122.50 -4.2	0 63.9	1176.	6.92	4414.	. —	12.23	57.4	956.	5.55
26123.50 -4.8		1071.	6.36	5278		12.75	54.9	864.	5.06
26124.50 -4.4	2 58.6	970.	5.80	4814.		13.25	52.1	776.	4.57
26125.50 -4.2	1 55.8	-374.	5.26	4642.		13.72	49.4	692	4.10
26126.50 -4.8	6 53.3	781.	4.61	5462		14.17	47.0	613.	3.72
26127.50 -4.4	0 50.0	694.	4.24	5000.		14.66	43.8	537.	3.22
26128.50 -4.7	5 47.9	511.	3.88	5464.		15.06	41.7	468.	2.92
26129.50 -4.4	3 44.7	533.	3.38	5157.		15.49	38.5	402.	2.50
26130.50 -4.6	9 42.3	459.	3.05	5509.		15.86	36.1	341.	2.20
26131.50 -5.3	2 39.4	390.	2.63	6311.		16.27	33.3	284.	1.87
26132.50 -4.5	2 36.3	327.	5.55	5415.		16.63	30.2	232.	1.54
26133.50 -5.3	6 33.5	267.	1.90	6464.		16.98	27.6	185.	1.28
26134.50 -4.1		214.	1.56	5057.		17.28	24.4	142.	1.00
26135.50 -2.9	5 28.4	164.	1.37	3682.		17.45	22.6	106.	•86
26135.58 -2.8	0 26.3	160.	1.35	3509.	•114	17.45	22.4	103.	•85

	Ly	46.		*(1° )	. ;	* 1 ₁ 1 2			16 175
TEST NO. 30C	νΔ:	K III ANT					/		
	11	,				7 A I C	VEL .	LITIND	OTREC
STAND WGT	TEST WGT 34200.LBS	PRES 27.59	O IN HG		Z*2 C	4.0	NIS	230.0	DEG MAG
• 1		T.CCT					STAN	IDARD I	)AY
4-7-m-		OTET R	re F	B D	URR	FBR -	KTAS	DIST	KE
	GNU-SPD	5404 27	28	112-	-006	01	126.8	5713.	24.21
28018.753.93		,6174., 26	43.	495.	.024	05	124.8	5506.	23.43
28019.75 -4.19		5959. 25	49	0.	0.000		122.4	5304.	22.57
28020.75 -3.24	129.8			133.	.054	23	120.2	5103.	21.75
28021.754.49	127.5		73			.31	118.0		
28022.75 -2.89			3.02	784-	036	.38	116.1	47.16.	20.30
28023.75 -3.90		/	2.25	0.	0.000		114.1		
28024.75 -2.99			.511		.058	.59	112.1		18.92
28025.754.18			69	662	.029	.78 .	109.9	4161.	18.17
28026.75 -3.44				320.		97	107.8 :	3983.	17.50
28027.75 -3.92				688	.073	1.28	105.3		16.69
28028.75 -4.15				440.	.062	1.58	102.9		15.93
28029.75 -3.79		2001		725.	.074	1.83	101.0	3468 .	15.36
28030.75 -3.95	5. 107.9 1 105.3		· , . ,	248.	095	2.21	98.5	3304	. 14.61
28031.75 -4.3		-3595 19	1	504.	.105		95.9	3143.	13.86
28032.75 -4.44	_			313.		3.01	93.6	2988	313.20
23033.75 -4.15				257	.093	3.43	91.0	2835.	12.45
28034.75 -3.97	_		-	732.	.070	3.71	89.1	2688.	11.95
28035.75 -3.39		2935 • 1		372.	.090	4.07	86.9	2544	11.35
28036.75 <b>-</b> 3.93	- ,			885	.136	4.52	84.5	2403.	10.75
		,		187.	.086	4.94	81.8	.2266.	10.07
28038.75 -3.4° 28039.75 -3.8°				600.	.104	5.27	79.9	2133.	9.61
				898.	1118	5.66	77.8		9.10
28040.75 -4.07 28041.75 -4.29				254.	.130	6.12	75.0	1878.	8.46
28042.75 -4.03				3119.	.125	6.54	72.7		7.96
28043.75 -3.2	-		3.92 2	357.	.090	6.88	170.6.°	1639.	7.50
28044.75 -4.0			3.52 3	3254.	.129	7.21	68.9	1526.	7.15
28045.75 -4.8				187.	•163·	7.71	66.0	1414.	6.56
28046.75 -4.0	_		7.29 3	3496.	.13A	8.16	63.4	1307.	6 • 05 -
28047.75 -4.8			5.81 4	389.	.174	8.60	61.1	1204.	5.62
28048.75 -4.1			5.23 3	3712.	•145	9.05	58.3	1106.	5.12
28049.75 -3.7	_	1226.	5.80. 3	377.	.130	9.41	56.1	1012.	4.73
28050.75 -3.6			5.44 3	3361.	.130	9.74	54.1	923•	4.41
28051.75 -4.5				356.	.166	10.13	51.6	835.	4.01
28052.75 -4.1		929.	4.57 - 4	012.	•153	10.51	49.3	753	3.66
28053.75 -4.1		339.	4.16 4	077.	.161	10.88	46.8	674.	3.29
28054.75 -3.7			3.80 3	3681.	.143	11.19		. 599•	2.99
28055.75 -5.8		569 .	-	015.	•231	11.61	41.9	527.	2.65
28056.75 -4.1		593.	2.96 4	331.	•165	12.00	38.8	461.	2.27
28057.75 -4.0		520.		+197.	.158	12.29	36.5	399.	2.01
28058.75 -3.9		451.		150.	.154	12.57	34.4	342	1.78
28059.75 -5.3				5682	.216	12.90	31.7	287•	1.51
28060.65 -3.2		332.	1.78 3	3538.	.135	13.08	29.1	243•	1.20

TEST NO. 314	MARK II	ANTISKID/USAF	TIRES/WET	RUNWAY

STAND WST		TEST WGT		PRESS	ALT	TEMP	WIND	VEL	WIND	DIREC
40050.LBS		40350 .LBS	;	27.488		11.7 C	5.1	KTS	236.0	DEG MAG
400030003		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,								
				TEST NA	Y			51	ANDARD I	)AY
103		GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
	-3.69		8373				0.00	138.8	7573.	34.12
23984.00							0.00	137.0	7344.	33.24
23985.00	-3.54		8123				• 13	134.5	7117.	32.06
23985.00	-4.27		7887							30.95
23987.00	-3.91		7650				• 26	132.2	6894	
23989.00	-3.95		7417					129.9	6675	29.88
23983.00	-3.76		7189				. 60	127.5	6459.	28.78
23990.00	-3.31	132.3	5964			008	• 67	125.4	6248	27.86
23991.00	-3.89	130.2	6742				. 84	123.3	6041.	26.93
23992.00	-3.19	128.1	6524	29.3	0 323	012	• 99	121.2	5837.	26.02
23993.00	-3.46	126.2	6310	. 28.4	7 816	029	1.09	119.4	5638.	25.25
23994.00	-3.76		6098		9 1374	049	1.38	117.0	5439.	24.26
23995.00	-3.30		5891		6 996	634	1.59	115.1	5247.	23.48
23995.00	-3.75		5687				1.90	113.0	5056.	22.60
23997.00	-2.78		5487				2.12	111.0	4870 .	21.82
23999.00	-3.92		5289	24.0			2.38	109.3	4689.	21.17
23999.00	-3.18		5095	23.0			2.79	106.8	4507.	20.18
			4905				3.06	105.2	4332.	19.59
24000.00	-3.62						3.44	102.9	4158.	18.76
24001.00	-3.23		4718				3.76	101.1	3989.	18.09
24002.00	-3.43		4535						3822	17.37
24003.00	-3.33	105.7	4355				4.13	99.1		16.73
24004.00	-3.10		4178				4 • 45	37.2	3660.	
24005.00	-3.35		4004				4 • 81	95.2	3500.	16.05
24005.00	3.33		3834				5.18	93.4	3.344.	15.43
24007.00	-3.08	98.0	3567				5.54	91.4	3191.	14.78
24005.00	-3.47	- 96.2	3503	16.5	5 2596	083	5.90	89.6	3042.	14.23
24009.00	-3.37	93.9	3343	. 15.7	6 2571	081	6.35	87.3	2894.	13.51
24013.00	-3.48		3186	. 15.1	6 2786	088	6.74	85.6	2751.	12.96
24011.00	-3.32		3032	. 14.4	5 2678	084	7.19	83.4	2610.	12.32
24012.08	-3.34		2882			087	7 . 57	81.5	2475.	11.80
24013.00	-2.74		2735				7.94	79.6	2341.	11.23
24014.00	-3.77		2591				8.35	77.9	2211.	10.73
24015.00	-3.13		2450				8.77	75.8	2084.	10.16
24015.00	-4.15		2313				9.27	73.5	1959.	9.57
			2180				9.75	71.3	1838.	9.01
24017.00	-3.61						10.23	69.1	1722.	8.46
24015.00	-3.63		2051				10.65	67.0	1609.	7.95
24019.00	-3.51		1925					64.9	1499	7.46
24023.00	-3.75		1802				11.12		1393.	6.98
24021.00	-3.98		1683				11.59	62.8		
24022.00	-2.93		1569				12.01	60.6	1291.	6.49
24023.00	-3.91	65.2	1457				12.40	58.8	1193.	6.13
24024.00	-4.12	62.5	1349	. 6.9			12.91	56.2	1096.	5.59
24025.00	-3.43	60.3	1246	. 6.9	0 3825	119	13.33	54.0	1005.	5.16
24025.00	-4.39		1145	. 6.0	.5083		13.77	52.0	917.	4.79
24027.00	-3.54		10,50			125	14.22	49.3	832.	4.30
24028.00	-3.79		958				14.61	47.2	752.	3.95
24023.00	-3.45		869				14.97	45.1	677.	3.61
24030.00	-4.54		7.84				15.40	42.5	603.	3.22
	-3.98		784				15.80	48.2	534.	2.86
24031.00			627				16.18	37.8	468.	2.53
24032.00	-4-17						16.42	35.5	413.	2.25
24032.90	-4.12	41.8	562	. 3.1	. 3 3166	129	10045	39.63	7400	

TEST NO. 3	3 1 B	HAF	ek II	ANTISK	IO/USAF	TI	RES/WET	RUNHAY			
STAND WEI		TEST WGT		PRESS	ALT		TEMP	WIND	VEL	WIND	DIREC
36000.LBS		36200.LBS	2	7.495	IN HG		4.0 C	5.8	KTS	230.0	DEG MAG
			T	EST DA	v				ST	ANDARD	DAY
			DIST	KE	FBR		UBR	EBR	KTAS	DIST	KE
100		GND-SPD	7389.			0.	. 010	. 01	130.1	6569.	
26611.39	-4.01	138.1				6.	. 004	. 03	128.2	.6384 .	
26612.25			7190 .	· · · · · · · · · · · · · · · · · · ·			. 045	.18	125.7		
	-4.42		6962.				.029	. 35	123.3	5961.	
		131.2	6738.		7	66.			121.2		
26615.25			6518.			8.	. 036	. 65		5556.	
26615.25	-3.80		6303.	25.7	3 77	77.	.033	.75	116.7	5360.	
	-3.45		6091.		8 51	16.		. 93 .	114.7		
26618.25			5882.			.2.	. 035	1.03	112.5	4978.	
	-3.48		5678 .			14.	. 034	1.32	110.4	4791.	
25621.25	-3.75		5470.								
26621.25	-3.01	115.4	5278.					1.47	108.5	4430.	
26622.25	-3.90		5084.				. 167	1.75			
26623.25			4893				. 047	2.00	104.4		
26624.25	-3.17	110.2	4706.				. 043	2.24	102.4		
26625.25						71.	. 074	2.55	100.3	3914.	
26625.25	-2.94		4341				.042		98.2	3749.	
26627.25	-3.46		4153			29.	.066	3.11	96.4	3587.	
26628.25	-3.47	132.1	3989					3.43	94.5	3429.	
26623.25	-3.56		3819			38.	. 077	2012	2 4 4 4	3273.	
25631.25	-3.42	37.9	3652			72.	. 074	4.13		3121.	
26631.25	-3.11	95.9	3488			11.	. 065		88.3	2973.	
25632.25	-3.46	94.3	3328			73.	.081	4.75	86.7	2829.	
26633.25	-3.46	92.0	3171	. 13.5		65.	. 084	5.13	84.5	2687 •	
25634.25	-2.97		3017			95.	. 967	5 . 45	82.5	2549.	
26635.25	-3.18	88.4	2867	. 12.5		Ců.	.078	5.75	80.8	2414.	
25635.25	-3.29	86.3	2719	. 11.9		02.	. 085	6.13	78.8	2282.	
25637.25	-3.47		2575	. 11.4		87.	.095	6.47	76.8	2153.	
26633.25	-3.40	82.4	2434	. 10.8		73.	.095	6.83	74.9	2027	
26633.25	-3.65		2297	10.3		53.	. 107	7.24	72.8	1905.	
26641.25	-3.31		2163	. 9.7		24.	. 097	7.62	79.7	1785.	
26641.25	-3.83	76.1	2033	. 9.2	28 33	85.	.119	8.02	68.7	1670.	
26642.25	-3.42		1906	. 8.7		61.	.105	8 45	66.3	1557	
25643.25	-3.65	71.8	1783			20.	. 117	8.83	64.4	1443	
26644.25	-3.26	59.8	1664			40.		9.18	62.5	1345.	
26645.25	-4.28		1543			57.	. 147	9.61	60.3	1243.	
26645.25	-3.48	65.2	1436	. 6.8	31 33	ն 8 •	. 117	10.02	57.9	1144	5.34
26647.25	-4.21	53.3	1327	. 6.4		91.	. 152	10.40	56.0	1051	
26649.25	-4.07		1223	. 5.8		38.	. 145	10.87	53.0	958	
26643.25			1122	. 5.4	47 43	88.	.158	11.25	51.2	872.	
26651.25	-3.63		1027		30 37	52.	.132	11.65	48.7	789.	
26651.25	-4.38		934	. 4.5	58 45	90.	. 161	12.04	46.3	710	
26652.25	-3.98		845	. 4 . :	18 42	16.	. 144	12.41	43.9	635	
26653.25	-4.4		762			54.	. 168	12.80	41.4	564	
26654.25			682	. 3.	38 44	22.	. 151	13.15	38.8	496	
26655.25	-3.7		606			66.	. 144	13.47	36.7	434.	
26653.25	-3.2		534			63.	. 125	13.75	34.5	376	
26657.25	-4.5		465			.83	.178	14.05	32.5	321	
26653.25	-4.7		401			71.	.189	14.40	29.5	268	
26653.25	-4.5		342			49.	. 187	14.70	26.9	221	
26651.25	-4.6		287			52.	.184	14.99	24.1	178	
26661.25	-4.6		236			15.	. 184	15.26	21.4	139	
26652.04	-3.7		196			69.	. 151	15.40	19.2	110	59
20002104					1						

(12)	JI. 1					#1142197 IVE				
STAND WG	T	TEST WGT	F	RESS A	LT.	TEMP	WIND	VEL	WIND	DIREC
40000.LBS	. 4	40200.LBS	27	.583 IN	I HG	25.6 C	5.5	KTS	20.0	DEG MAG
									ANDARD [	
TOD		GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
37440.32	-3.65	128.3	7753.	29.27	504.		-02	126.7	7515.	28.44
37441.25	-3.64	126.2	7553.	28.36	621.		•14	124.8	7325.	27.57
37442.25	-3.63	124.2	7342.	27.43	755.		.27	122.7	7123.	26.68
37443.25	-3.63	122.0	7134.	26.47	892.		<b>.</b> 46	120.6	6926.	25.76
37444.25	-2.88	120.0	6930.	25.64	74.		•53	118.7	6731.	24.97
37445.25	-3.71	118.3	6729.	24.89	1221.		•65	117.0	6539	24.25
37446.25	-3.76	115.7	6531.	23.83	1438		98	114.5	6351.	23.23
37447.25	-3.00	114.0	6338	23.13	579.		1.10 1.33	112.9	6166. -5984.	22.56 21.72
37448.25	+3.43	111.8	6147.	22.25	1256.			109.0	5805	21.04
37449.25	-3.05	110.0	5960.	21.55	884.		1.51		5629	20.35
37450.25	-3.23	108.2	5776.	20.82	1211. 1779.		-1.71 2.01	107.2 105.1	5456	19.57
37451.25	<del>-</del> 3.58	106.0	5595. 5417.	20.01 19.41	807.		2.18	103.6	5286	18.99
37452.25	-2.73	104.4	5243.	18.66	1969.		2.47	101.6	5119.	18.27
37453.25 37454.25	-3.59 -2.82	102.4 100.7	5072.	18.05	1120.		2.69	99.9	4955	17.68
37455.25	-3.07	98.6	4903.	17.30	1534.		2.97	97.9	4794	16.97
37456.25	-2.42	97.3	4739.	16.85	781.		3.10	96.6	4635	16.54
37457.25	-2.99	95.2	4575	16.14	1598		3.37	94.6	4480	15.85
37458.25	-3.73	93.6	4415.	15.60	2609.		3.68	93.1	4326	15.34
37459.25	-2.44	91.4	4260	14.67	1097.		4.00	90.9	4178.	14.63
37460.25	-3.06	90.1	4106.	14.43	1946.		4.21	89.6	4029.	14.21
37461.25	-3.08	88.2	3956	13.85	2159.		4.53	87.8	3885.	13.65
37462.25	-3.26	86.1	3809.	13.21	2478.		4.91	85.8	3744.	13.03
37463.25	-1.99	84.7	3665.	12.77	941.		5.11	84.4	3605.	12.61
37464.25	-2.37	83.4	3523.	12.39	1478.	■ 046	5.29	83.1	3468.	12.24
37465.25	-2.84	81.8	3383.	11.92	2121.	.067	5.57	81.6	3333.	11.78
37466.25	-3.05	80.2	3246.	11.44	2461.	•076	5.87	80.0	3201.	11.32
37467.25	-2.54	78.2	3113.	10.88	1893.	• 059	6.20	78.0	3073.	10.78
37468.25	-1.49	77.5	2982	10.69	615.		6.28	77.4	2945.	10.60
37469.25	-3.28	75.9	2852.	10.26	2895.		6.56	75.8	2820.	10.18
37470.25	-2.97	73.9	2726.	9.72	2596.		6.93	73.9.	2698	9.66
37471.25	-2.12	72.6	2603.	9.39	1568.		7.15	72.6	2579	9.34
37472.25	-2.93	71.0	2481.	8.97	2639.		7.44	71.0	2461.	8.93
37473.25	-2.67	69.2	2363.	8.52	2383.		7.75	69.3	2347•	8.50
37474.25	-1.22	67.9	2248.	8.21	617.		7.91	68.0	2235.	8.20
37475.25	-2.36	67.2	2133.	8.02	2064.			67.3	2122•	8.02
37476.25	-4.03	65.1	2021.	7.54	4217.			65.3	2014. 1911.	7.55 7.11
37477.25	-1.47	63.1	1914. 1807.	7.09	1078.		8.72 8.86	63.4 62.8	1805.	6.99
37478.25	-2.45	62.5 60.3		6.96 6.48	2325.	-099	9.21	60.7	1705	6.52
37479.25 37480.25	-2.37	59.1	1603.	6.22	2326		9.45	59.5	1607.	6.27
37481.25	-2.85	57.3	1505.	5.84	2988	_ ,	9.74	57.7	1511.	5.89
37482.25	-3.28	55.5	1409.	5.49	3567		10.05	56.0	1418.	5.55
37483.25	-2.54	53.6	1317.	5.12	2690.		10.35	54.1	1328.	5.19
37484.25	-2.28	52.5	1228.	4.90	2386.		10.55	53.0	1240.	4.98
37485.25	-3.13	50.9	1141.	4.60	3504.		10.82	51.5	1155.	4.69
37486.25	-2.01	48.9	1056	4.26	2161.		11.07	49.6	1072.	4.35
37487.25	-2.68	48.2	974.	4.14	3014.		11.24		990•	4.23
37488.25	-2.90	46.1	895.	3.78	3340.		11.53	46.8	912.	3.88
37489.25	-2.91	44.5	818.	3.52	3391.		11.77	45.2	837.	3.62
37490.25	-3.50	42.7	745.	3.25	4161.		12.05	43.5	764.	3.35
37491.25	-3.53	40.3	675.	2.90	4252.	.131	12.36	41.2	696.	3.01
37492.25	-2.87	38.5	508.	2.64	3471.	•106	12.60	39.4	630.	2.75
37493.25	-3.13	36.8	544.	2.41	3836.		12.83	37.8	566.	2.53
37494.25	-2.43	35.0	484.	2.18	3011.	• 0HB	13.04	36.0	506.	2.29
37495.25	-2.73	33.7	426.	2.03	3404.		13.21	34.8	446.	2.14
37496.25	-3.30	31.8	370.	1.80	4126.		13.42	32.9	391.	1.92
37497.25	-1.65	30.2	318.	1.62	2091.		13.58	31.3	338.	1.74
37497.47	-1.05	30.0	307.	1.60	1348.	•042	13,58	31.2	326.	1.72

	VARMIN	TIRES/WET	ATENATA	STTLAM T	MARK		ASE C	TEST N
TEST_NO. 320	MAHK	II ANTISK	IDZBEG 3	TRECIME	T DUMBLAY		1 000 500 1.	
NIND DIREC	MARK WIND VEL POR FAST 261.06646	TEMP	AL T	22390	TOW	TEST	Tow	STAND
DATAND? WOTS	Pow Fast	PHPSES	IN HOT JA	FRANTS	WA BIS	409904	WIRB-	Egggod'
36000.LHS	36550.L85	27.576 10	N HG	27.0 C	2.2	KIS	336.0	DEG MAG
TAMEN	The same the test in the same time and	to bell the case and staff the last last last last	ALCOHOLD DE LA COLUMN	011 1 2 411	De 100 AND 100 100 100 100	~ <b>** ** **</b> ** ** ** **	46 405 We all	
TOD ACCEL		TEAT DAY	_EH1	-34	121604	- UND STA	MARKD D	AVEL
30466 70 ACCEL	GND-SPD NOT	ST PIONE OF	CALLORA	P. ANHBO	CHAR E	KTAS CO	DISTA	TANTE
39465.70 -4.34 39466.50 ÷3.74 39467.50 -3.79	123.3 / 651	1. 24 61	130 1195V	4. [850.	23623362	121 950 1874 650	65856°	53.68
39467.50 -3.79	121.3 -670	7. 23.80	H20	W. 2834	0 25/134	630 556	Engage	STATE .
39468.50 -3.71	・・117・リード つつし	14	894°	0.36	16. 4 254 U	· Pra 7ea	• AUC 2 C =	1 4 D. L. L. J. C
39469.50 -3.92	116.7 530	5. 10 22.02	1254	.050	7H E	112 216.	·Saco ??	124792
39470.50 -2.81	114.8 611	0.21.33	1152	2005 V	297	111.70	CERU!	10000
39471.50 -3.50	112.9 4591	8. 20.61	977	.040	.99	109.A	55115	1.14.51
39472.50 -3.74 39473.50 -3.42		4. 19.78	14036	056	1.25	107.6	5336	18.45
39474.50 -3.79	106.4 536	4. 19.14	1400	045			5165	17.86
39475.50 -3.39	104.2 518	S. 1.7.18	1070	062	10.01	103.5	4998	17.08 16.41
39476.50 -2.98	@ 102.4 - 501	0. 16.98	9814	- 2038 A	2.20	99.7	4672	15.85
39477.50 -3.39	453	9. 16.33	1528.	059	2.43	97.8	4514	15.25
39478.50 -3.23	98.6 . 457	1. 15.75	1446.	300 (156 V	2.66	96.1	435H.	14.71
39479.50 -3.21	96.7 450	5. 15.13	1524.	.058	2.91	94.2	4206.	14.14
39480.50, +2.59 39481.50, +3.27		5. 14.57	906	.034	3.09	92.5	4057.	13.62
39482.50 -2.88		6. 14.11. 0. 13.48	1406	0000 n	3.30	91.0	3909	13.19
39483.50 -2.45		7. 73.08.	967	0.75	3.71		3765. 3623.	12.61
	87.9 372	6. 12:49	3494	-130		85.7		11.69
39485.50 -2.52	85.5 358	1. 11.84	1242.	.046	4.43		3350.	11.09
39486.50 -2.33	64.3 - 343	H. 11.50	1074	040	4.57	82.2		10.78
39487.50 -3.17	82.6 329	7. 11.05	5103	0.077 d	4.81	80.6		10.36
39488.50 -2.93 39489.50 -2.18	80.5 *315° 79.4 *302	4. 410.49	1921.	.070			2958	9.44
39490.50 -2.81		1. :9.72	1102.	.041	5.78		2833.	9.56
39491.50 -2.58	76.3 276	9.41	1695	061	B-72		2710. 2589.	9.13 8.84
	74.3 263		· 2115 ·		6.00		2471.	8.39
39493.50 -2.74		0. 8.59	2006.	.071			2356	8.08
39494.50 -2.30	71.3 238	8.55	1564.		6.45			7.73
39495.50 -3.03		7.86	2439	· 088		68.1	2132.	7.40
39496.50 -2.83 39497.50 -2.87	~ 68.0 2150	3. 7.4H	2277.		6.96	66.5	2024.	7.04
39498.50 -2.47	66.4 2046 64.7 1929	9. " 7.12 " 9. " 6.76	2380.	.084	7.22	04.9	1918	6.71
39499.50 -3.47		6.47	3160.	. 114	7.72		1815. 1714.	6.38 6.10
39500.50 -2.18		6.04	1770.		8.00		1617.	5.70
	60.3 151.	F. 5.6H-	1944.		8.15		1521.	5,56
39502.50 -2:60	58.6 1514		2323.	•085			1428.	5.25
39503.50 2.54	57.0 1416		2293.			55.9	1337.	4.98
39504.50 -2.96 39505.50 -3.16	55.6 1321 53.6 1229		~ 2815. ~3104.	•100	8.84	54.5	1248	4.74
39506.50 -2.57	51.7 1139		2495		9.13	,	1162.	4.41
39507.50 -2.50	.50.8 1053		2430		,		998.	3.96
39508.50 -3.29	48.8 969		3385.			47.9	920.	3.66
39509.50 -3.25	46.8 884		3377.	.120	10.09		844.	3.38
39510.50 -3.37	44.9 811		3555.		10.36	44.2	771.	3.11
39511.50 -2.04	43.3 737		2098	.073	10.55	42.6		2.89
39512.50 -3.78 39513.50 -2.74	41.8 665 39.3 597		4112. 2986.		10.78	41.1	634.	2.70
39514.50 -3.20	38.1 531		3533.	.103	11.04	38.8 37.6	570. 508.	2.40
39515.50 -3.43	35.7 469		3835		1.48	35.3	450.	1.98
39516.50 -3.27	34.0 410	1.87	3692.			33.7	394	1.81
	31.9 354	1.64	3814.	135	1.89	31.6	342.	1.59
39518.50 -3.50	30.0 302		4019.			29.8	292.	1.42
39519.50 -3.55	27.7 253	1.24	4118.	144	2.29	27.6	246.	1.21
39520.50 -3.82 39521.50 -4.07	26.0 208 22.9 166	and the same of	4771.		2.47		203.	1.07
39521.90 -2.47	27.1 152		2980.		2.68		164.	.84 .78
		• • • •		4103		~ C. • C.	1770	D (1)

TEST NO.	33A	МАІ	RK II AN	TISKID/	DUNLOP 1	IRES/W	ET RUNW	AY		
STAND WG	T	TEST WGT		RESS AL 584 IN	•	TEMP	WIND	VEL KIS	WIND (	DIREC DEG MAG
40000.LBS								-74	LOADO D	AV
			TES	ST DAY				STA		KE
TOD	ACCEL	GND-SPD	DIST	KE.	FBR	UDK	CDN	KTAS	DIST 7400.	36.76
22998.56	-4.34	145.6	7623.	37.87	0.	#000	0.00	144.1	7177.	35.54
22999.50	-3.74	143.2	7393.	36.62	0.	*000	0.00	141.7	6944.	34.51
23000.50	-4.25	141.1	7153.	35.57	470.	019	•03	139.6	6714.	33.17
23001.50	-4.62	138.3	6917.	34.18	1120.	.044	•27	136.9	4 4 5 5	32.03
23002.50	-3.36	135.9	6686.	33.01	0.	#000	•35	134.5		31.07
23003.50	-3.78	133.9	6458.	35.03	371.	.014	•38	132.5	6050	29.99
23004.50	-4.05	131.5	6234.	30.91	8/2.	.033	•54	130.1	5836	28.95
23005.50	-3.70	129.2	6014.	29.84	588.	.022	.70	127.9	5626	27.94
23006.50	-3.91	127.0	5798 •	28.80		•036	.87	125.6	5419.	26.93
23007.50	-3.68	124.7	5585.	27.76	856.	.031		123.3 121.4	5217.	26.11
23008.50	-3.65	122.8	5377.	26.92	918.		1.20	118.9	5017.	25.02
23009.50	-4.29	120.2	5172.	25.80	1899.	<b>.</b> 068	1.55	116.6	4822	24.08
23010.50	-3.42	117.9	4970.	24.83	989	•035	2.03	114.8	4630.	23.33
23011.50	-3.67	116.0	4773.	24.06	1477	.050	2.36	112.4	4442.	
23012.50	-3.64	113.6	4579.	23.07	1561.	•053	2.62	110.5	4257.	
23013.50	-3.54	111.7	4389.	22.30	1598.	.053	3.02	108.1		20.69
23014.50	-3.92	109.3	4203.	21.34	2211•	.073	3.38	106.0	3898	19.90
23015.50	-3.81	107.2	4020.	20.53	2191.	.072	3.85	103.5	3724.	18.97
23016.50	-3.96	104.7	3841.	19.57	2504.	.083	4.19	101.7	3554	18.30
23017.50	-3.67	102.8	3666.	18.88	2253.	.073		99.1		17.38
23018.50	-3.78	100.2	3494 •	17.94	2517.		4.65	97.4		16.81
23019.50	-2.87	98.6	3327.	17.35	1460	.047	5.53	95.4	3065.	16.12
23020.50	-3.98	96.5	3162.	16.64	2940.	.095	6.05	91.8	2832.	14.92
23022.00	-4.29	92.9	2922.	15.40	3507.	.111	6.60	89.2	2682.	14.08
23023.00	-4.12	90.2	2768	14.53	3403. 2443.	.079	6.98	87.2	2536.	13.48
23024.00		88.3	2617.	13.92	3779.	.121	7.47	85.0	2393.	12.79
23025.00		86.0	2470.	13.20	2943	.093	7.93	82.7	2254.	12.11
23026.00		83.7	2327	12.51	3257	.103	8.38	80.5	2119.	11.46
23027.00		81.4	2188	11.84	3505	.108	8.83	78.3	1987.	10.87
23028.00		79.3	2052	11.23 10.55	3867	.120	9.33	75.9	1859.	10.21
23029.00		76.9	1921.	9.94	3350	.106	9.78	73.7	1735.	9.62
23030.00		74.6	1793	9.35	4455		10.26	71.5	1615.	9.04
23031.00		72.3	1568	8.66	4657.	.146	10.83	68.8	1498.	8.38
23032.00		69.6	1548	8.10	4209.	135	11.31	66.5	1387.	7.83
23033.00		67.3	1433.	7.46	4422	.139		63.8	1279.	
23034.00		64.6	1322.	6.96	3711.	.117	12.24	61.6	1175.	6.72
23035.00		62.4	1215.	6.45	4075	.131	12.66	59.3-	1074.	6.23
23036.00			1111.	5.99	5350	.173	13.11	57.2	978.	5.79
23037.00			1012. 917.	5.31	5529	.172	13.68	53.8	885.	5.12
23038.00			827 ·	4.95	3420	.107	14.01	52.0	799.	4.78
23039.00			740	4.46	5882.	.181	14.45	49.3	714.	4.30
23040.00			658	3.95	5873.	.188	14.93	46.4	634.	
23041.00			580	3.48	5962.	.187	15.37	43.5	560.	
23042.00			509.	3.08	5056.	.154	15.75	40.9	490.	
23043.00	-4.15	41.5	441.	2.73		.156		38.5	424.	2.63

5273.

5894.

5548.

7067.

5758.

5374.

3901.

.156

.183

.181

.225

.182

.170

.118

16.45

16.76

17.13

17.42

17.67

17.76

2.26

2.00

1.59

1.33

1.08

.94

362.

305.

251.

204.

160.

132.

35.7

33.6

30.0

27.4

24.7

23.1

441.

376.

317.

262.

213.

168.

138.

2.73

2.08

1.66

1.39

1.13

.99

-4.27

-4.74

-4.45

-5.60

-4.52

-4.18 -2.97

23044.00

23045.00

23046.00

23047.00

23048.00

23049.00

23049.71

39.1

36.3

34.1

30.5

27.9

25.2

23.5

STAND W	GT S	TEST WG1 36550.LBS		PRESS /	ALT N HG	TEMP 15.5 C	WIN .0	D VEL 0 KTS	WIND 225.0	DIREC DEG MAG
			1	EST DAY-				ST	ANDARD I	DAY
TOD		GND-SPD	DIST	KE	FBR	UHR		KTAS	DIST	
25101.69	-4.30	136.7	7111.	30.25	241.	.012	.00	134.6	6791.	28.88
25102.50			6926.	29.40	0.	*000	.03		6614.	28.08
25103.50	-3.77	132.4	6700.	28.36	0.		.03	130.4	6399.	27.09
25104.50			6478.		135.	.006	.04	128.3	6187.	26.25
25105.50			6260.		669.	.030	.17	125.9	5978.	25.24
	-4.09		6046.	25.52	763. 727.	.033	.28	123.7	5774.	24.37
25107.50	-3.91	122.9	5836.	24.44	727.	.032	.49	121.0	5574-	23.34
25108.50			5631.	23.81	0.	4000	.49	119.4	5377.	22.74
25109.50			5428.	23.05	1038. 505.	.044	•60	117.5	5184.	22.01
			5229.	22.07	505.	.051	.79	115.0	4994.	21.08
25111.50	-4.21	114.7	5033.			. 000	1.02	112.9	4806.	
25112.50			4842.	20.44	506.	.021	1.21	110.7	4624.	19.52
25113.50		110.2	4653.		1056.			108.5		18.77
25114.50		108.5	4469.	19.06	1866.	.077	1.62	106.9	426B.	18.20
25115.50	-3.98	105.4		17.98	1860.	.076	2.06	103.8	4096.	
25116.50	-2.11	103.9	4112.		0.	0000	2.13	102.3	3927.	16.67
25117.50	-3.73	1.501	3937.	16.87		.071	2.30	100.6	3760.	16.11
	-3.80	99.9	3767.	16.16	1940.			98.4	3598.	15.43
25119.50	-2.93	97.B	3501.	15.49	1064.		2.88	96.3	3439.	14.79
25120.50		96.3	3437.	14,99	1208.		3.05	96.3	3282.	14.32
25121.50	-3.86	94.2	3276.	14.35	2304.	.090	3.35	92.7	3128.	13.70
25122.50	-4.31	91.4	3119.	13.52	2954 -		3.82	90.0		12.91
		89.6	2966.	13.00	487.	.019		88.2		12.41
25124.50	-3.94	88.1	2816.	12.57	2682.		4.76	86.8	2689.	12.01
25125.50	-3.15	85.6	2669.	11.86	1895.		4.63	84.3	2549.	11.33
	-3.21	84.1	2526.	11.44	2031.		4.87	82.8	2412.	10.93
25127.50	-3.13	82.2	2386.	10.95	2019.	.077		81.0		10.45
25128.50	-3.21	80.2	2249.	10.40	5511.	.081	5.47	78.9	2148.	9.93
25129.50	-2.94	78.4	2115.	9.95	1970.	.072	5.73	77.2	2020.	9.51
25130.50	-3.55	76.5	1984.	9.47	2734.		6.04	75.3	1895.	9.05
25131.50	-3.86	74.1	1956.	8.89	3182.		6.44	73.0	1772.	8.49
25132.50	-3.07	72.5	1733.	8.50			6.74	71.4	1655.	8.11
25133.50	-4.40	70.0	1512.	7.93	3951.		7.16	68.9	1540.	7.57
25134.50	-3.45	67.6	1496.	7.40	2950.	.109	1.54	66.6	1429.	7.07
25135.50	-3.95	65.5	1384.	6.95	3593.	.134	7.91	64.5	1321.	6.63
25136.50	-3.63		1275.	6.49	3306.	.125	8.58	62.4		6.20
25137.50	-3.82		1170.	6.02	3599.	.133	8.65	60.0	1117.	5.75
25138.50	-3.43	59.0	1069.	5.64	3217. 3858.	.119	8.97	58.1	1021.	
25139.50	-3.93		971.	5.20	3858.	.142	9.34	22.8	927.	4.97
25140.50	-4.44				4513.		9.73	53.6	838.	4.57
25141.50	-3.89	51.8	<b>788</b> .	4.34	3949.	.147	10.10	51.0	752.	4.14
25142.50	-4.29	49.4	702.	3.95	4481.	.162	10.47	48.6	670.	3.77
25143.50	-4.15	46.9	621.	3.55	4399.	.155	10.83	46.1	593.	3.39
25144.50	-4.33	44.3	543.	3.17	4670.	.164	11.18	43.6	519.	3.03
25145.50	-4.12	41.8	471.	2.83	4496.	. 156	11.51	41.2	450.	2.70
25146.50	-4.73	39.0	402.	2.46	5245.	.184	11.85	38.4	384.	2.35
25147.50	-3.96	36.5	338.	2.15	4416.	.158	12.15	35.9	323.	2.05
25148.50	-4.66	34.3	278.	1.91	5247.	.191	12.42	33.8	266.	1.82
25149.50	-4.91	30.9	223.	1.54	5605.	.200	12.75	30.4	213.	1.47
25150.50	-4.48	28.5	172.	1.32	5151.	.187	12.99	28.1	164.	1.26
25151.50	-6.02	25.3	125.	1.04	6961.	.247	13.28	25.0	119.	.99
25152.50	-5.62	21.5	85.	.75	6555.	.237	13.56	21.2	81.	.71
25153.25	-2.52	19.6	59.	.62	3076.	.107	13.64	19.3	56.	.59

STAND WGT		T WGT	PRE:	SS AL 80 IN	*	TEMP 24.6 C	WIND	VEL KTS		DEG MAG
550000 \$2170								ST	ANDARD (	DAY
TOD A	CCEL GND			KE	FBR	UBR	EBR	KTAS	DIST	KE
		5.2 7		1.33	0.	*000	0.00	131.1	7105.	28.93
				0.61	683.	.028	• 05	129.6	6937.	28.27
				9.34	1224.	.049	•32	126.9	6731.	27.10
				9.73	1059.	.036	2.53	104.1	4605.	18.25
		. • -		9.06	1319.	.044	2.76	102.4	4439.	17.62
•		*		8.41	1572.	.052	3.01	100.6	4277.	17.02
				7.75	903.	.030	3.23	98.8	4117.	16.42
_				7.19	1887.	.063	3.47	97.2	3959.	15.90
					1492.	.049	3.77	95.2	3805.	15.25
			951. 1	5.93	1882.	.062	4.04	93.6	3653.	14.73
				5.34	1283.	.042	4.29	91.8	3505.	14.19
	_			4.88	1570	052	4.50	90.5	3359.	13.77
				4.33	1241.	.041	4.72	88.8	3215.	13.27
				3.80	2365	.078	5.02	87.1	3073.	12.77
				3.26	1909.		5.32	85.4	2935.	12.27
		•		2.67	2500	.082	5.67	83.5	2800.	11.73
				2.17	2141.		5.98	81.9	2667.	11.27
				1.64	2162.	.071	6.28	80.0	2538	10.78
				1.12	2818	.091	6.63	78.2	2410.	10.30
		-			1852	.061	6.92	76.5	2286.	9.84
		-		0.62		.098	7.25	74.9	2164.	9.44
		-		0.19	2986	.067	7.53	73.3	2046	9.04
				9.76	2042	.098	7.90	71.2	1930.	8.53
			-	9.21	3016.	_	8.18	69.9	1817.	8.22
				8.86	2421. 3043.	.049	8.55	67.7	1706.	7.71
				8.32	2926.		8.85	66.3	1598	7.40
				7.98			9.25	64.0	1494.	6.89
				7.43	3412.		9.56	62.5	1393	6.56
				7.07	3041.		9.96	60.2	1295.	6.10
		- +		6.57	3698		10.28	58.3	1200.	5.72
				6.16	2790.		10.59	56.7	1107.	5.40
				5.82	3326.		10.96	54.5	1018.	4.99
3660,0.,				5.38	3873		11.32	52.4	932.	4.63
				4.98	4055			50.4	849.	
				4.60	3559.		11.65 11.96	48.6	770.	-
O				4.27	3646			46.4	693.	-
	. •		746.	3.89	5144.		12.33	43.9	621.	
O E 14 1 IE V . V	. =		668.	3.48	4815		12.71 13.08	41.4	552	
	_		593.	3.09	5364			39.2	489.	The second second
			525.	2.77	4051.		13.39	37.0	427.	
32245.75		38.0	458.	2.47	4639		13.67		370	1200
	-4.45	35.5	396.	2.16	5326		13.98	34.6	317.	7 7 7 7
		32.8	339.	1.84	5192.		14.29	32.0	268	
32248.75	-3.88	30.4	286.	1.58	4749.		14.54	29.7	221.	
		27.8	236.	1.32	5721.		14.80	27.1		
	-2 02 2	25 2	192.	1.09	3777.	.125	15.01	24.7	180.	4.0.

-3.03

-2.27

32250.75

32251.05

25.2

24.8

192.

179.

1.09

1.05

3777.

2881.

.125

.093

15.01

15.01

24.7

24.2

168.

.99

1

769	ST NO.	34C	"MA	es II a	a T15K10	COUNTRY.	TIRESA	FET RUNK	YAY	51	71. 18 A
- 1		r	IEST WGT	. 0	ness AL	T	TEMP	WIN	VEL	Ciriv	DIREC
	AND HE	•	34 <b>700.</b> L85		1.575 IN		4.7 C		KTS.		DEG MAG
.541	000.LBS	,	J~1700.CDJ		• ., , , ,			•	•		
								64 the sip pay per 100		ANDARD T	
-	TOD	ACCEL	GND-SPU	DIST		FBR _	UHR	EBR	KIAS.	DIST	KF
340	051.37	-3.86	129.1	7087.	CD * DT	214 "		( - U l	125.2	6535	23.63
341	052.25	-4.00	126.9	6896.	24.74	541.	.025	.12		6360.	
340	053.25	-3.25	124.9	6584.	23.95	O ₄	*000	•14	121.2	6165	22.10
344	054.25	-3.92	122.6	6475.	23.15			.20	119.2	5973 • 5784 •	20.51
340	055.25	-4.26	120.3	6269.	32.23	1213.		43	116.7	5600.	19.78
340	056.25	-3., 24	118,1	6068.	21.42	241 - 7		•54	114.6	5418.	19.15
	157.25	-3.50	116.2	5971+	2,00	- 636	.027 .032	.62 .77	110.7	5239.	
	058.25	-3.58	114.0	5576	19.96		015	85	108.9		17.85
	159.25	-2.98	112.2	5486.	19.33	884.	.037	.97		4891.	
_	060.25	-3.44	110.3	5298.	18.65	1316.	055	1.17	105.1		16.64
_	061.25	-3:74	108.3	5114.	18.01 17.21	1228.	.051	1.43		4556	
-	062.25	-3.53	.105.8	4933.	16.63	991.	.040	1.59	101.1	4393.	15.37
	063.25	-3.20	104.1	4756. 4582.		= 1436 ·	.058	1.83	99.1	4233.	14.79
		-3.50	102.0			1137.	.045	2.05	.97.2	4077	
_		-3.11 -3.16	100.1	4245.	14.77		:051	2128	95.3		13.66
	066-25		98.1 96.1	4081.			055	2.51	€ 93.4	3772.	
	067.25	-3.17 $-3.41$	94.2	3920.	13.62		068	2.79	91.5	3624.	12.60
	068.25	-2.79	92.5	3763.		1207.		2.99	89.9	3480.	12.16
	069.25 070.25	-3.87	90.2	3608.	12.50		.093	3.33	87.7	3337.	11.57
			88.6	3458.	12.07	629.	.024	3.51	86.2	3199.	11.17
	071•25 072•25	-2.11 -3.46	87.0	3309.	11.62	2157.	.081	3.74	84.6	3062.	10.76
	073.25	-2.49	85.0	3164.		1196.	.045	3.99	82.6	. 2928 .	10:27
_	074.25	-2.91	83.7	3021.	10.77	1700.	-064	4.16	81.4	2797.	9.98
	075.25	-3.20	81.7	2982.	10.25	2088.	.079	4.46	79.4	2668.	9.50
	076.25	-3.09	79.9	2745.	9.81	2040.	.076	4.72	77.7	2543.	9.10
	077.25	-2.56	78.1	2612.	9.38	1531.	.058	4.97	76.0	2420.	8.69
	078.25	-2.80	76.8	2481.	9.06	1844.	.068	5.17	74.7	2299.	8.40
	079.25	-2.86	74.8	2354.	8.60	1975.	.074	5.45	- <b>72.</b> 8	2182.	7.98
-	080.25	-2.97	73.2	2228.	R.24	2155.	.080	5.69	71.3	2066.	7.65
	081.25	-3.02	71.4	2106.	7.84	2270.	.084	5.97	69.5	1953.	7.28
	082.25	-2.83	69.6	1987.	7.44	2137.	.078	6.24	67.8	1844.	6.91
340	083.25	-1.98	68.2	1871.	7.14	1265.	046	6.42	- 66.4	1736.	6.64
340	084.25	-3.06	66.8	1757.	6.86	246 ⁹ •	.095	6.64	65.1	1631.	6.38
340	085.25	-2.54	64.9	1546.	6.47	1980.	.072	6.90	63.2	1529.	6.02 5.78
340	086.25	-2.63	63.6	1537.	6.22	2103.	.07R	7.10	62.0	1428.	5.49
341	087.25	-3:19		1431.	5.90	2755.	.103	7.30	60⊾4 58.4	1330.	5.13
	088.25	-3.52	: 59.9	1329	5.51	3181.	.117	7.68 7.95	56.5	1144.	4.80
	089.25	-2.60		1230.	5.16		.135	8.23	. 54 . 9	1054.	4.53
	090.25	-3.89	56.3	1133.	4.86	3682. 3146.	.117	8.57	52.4	969.	
	091.25	-3.33		1040.	4.43	3115.	.114	8.83	50.8	886.	3.89
	092.25	-3.26		951.	4.16	- 3295.	.119	9.12	48.7	807.	3.57
	093.25	-3.37	49.9	565.	3.54	3377	.125	9.30	-46.9	730.	3.31
	094.25	-3.41	48.0	782.	₹3.22	3383.	.123	9.65	44.8	657.	3.01
	095.25	-3.36	45.8	703. 627.	2.94	4178.	.154	-9-94	42.8	-586 •	2.76
	096.25	-4.06	43.8	555.	2.63	4134.	.152	10.23	40.5	520.	2.46
	097.25	-3.97		488.	2.35	3529	128	10.49	38.3	457.	2.20
	098.25	-3.36		423.	2.12	4257	.155	10.73	36.4	397.	1.99
	099.25	-4.00 -3.85		363.	1.83	4148.	154	10.99	33.8	341.	1.72
	100.25 101.25	-4.19		306.	1.61	4538.	.170	11.23	31.8	288.	1.52
		-4.10		254.	1.37	4507.	.160	11.46	29.3	240.	1.30
	102.25	-5.14	2	205.	1.13	5653.	.210	11.70	26.7	194.	1.07
	103.25 104.25	-4.55		162.	.90	5048.	.193	11.93	23.9	154.	•86
-	104.25	-2.74		124.	.73	3133.	.119	12.06	21.5	118.	.70
	105.32	-2.64		121.	.72	3034.	.113	12.06	21.5	116.	•69
2											

## TEST NO. 35A MARK II ANTISKID/BFG TIRES/WET RUNMAY

STAND WGT	TEST WGT	PRESS ALT	TEMP WIN	O VEL	WIND DIREC
43000.LBS	43350.LBS	27.398 IN HG		8 KTS	192.0 DEG MAG
4000000	,00500000				- 40
		TEST DAY		STA	NDARD DAY
TOD ACCE	L GND-SPD DIST			KTAS	DIST KE
23325.79 -4.8			0.000 0.00	146.7	9061. 40.98
23326.50 -5.0		2. 45.31	0. 0.000 0.00	144.8	8867. 39.90
23327.50 -4.1	and the second s	43.27	0. 0.000 -0.00	141.3	8622. 38.02
23328.50 -2.6		4. 42.55	0.0.000 0.80	140 - 1	8393. 37.36
23329.50 -4.8				137.7	8160. 36.07
23330.50 -4.0	1 143.8 899	39.67 73	4027 -45	135.0	7931. 34.71
23331.50 -3.6		9. 38.47 48	2017 .55	132.9	7708. 33.61
23332.50 -3.7		1. 37.28 - 64	6023 .70	130.7	7489. 32.53
23333.50 -3.5			8020 .84	128.6	7273. 31.47
23334.50 -3.5				126.5	7061. 30.48
23335.50 -3.6				124.4	6852. 29.44
23336.50 -3.5		32.85 101	0034 1.39	122.3	6646. 28.46
23337.50 -3.2		31.93 63	7021 1.53	120.5	6446. 27.62
23338.50 -3.2		_	7029 1.70	118.5	6248. 26.74
23339.50 -3.6		29.90 151	3049 1.99	116.4	6051. 25.78
23340.50 -2.6				114.7	5861. 25.02
23341.50 -3.4		6. 28.22 159	0050 2.36	112.9	5673. 24.24
23342.50 -3.4				110.8	5487. 23.38
23343.50 -2.8		4. 26.42 109	9033 2.96	109.0	5305. 22.61
23344.50 -3.0		7. 25.68 1144	7044 3.19	107.4	5126. 21.94
23345.50 -3.2				105.6	4951. 21.24
23346.50 -3.1		3. 24.02 - 177	5052 3.84	103.6	4777 20 43
23347.50 -3.4		5. 23.16 230	2068 4.25	101.6	4606. 19.66
23348 50 -2.7	5 108.2 519	2. 22.46 146	7	100.0	4441. 19.03
23349.50 -3.7		1. 21.66 285		98.1	4276. 18.30
23350.50 -3.3	1 104.0 "483	3 20.77 240			-4114. 17.51
23351.50 -3.0	7 102.3 465	9. 20.09 216		94.2	3957. 16.89
23352.50 -2.8	9 100 4 448	8. 19.34 200	8057 6.18		
23353.50 -3.2	7 98.9 431	9. 18.76 258		96.8	3652. 15.70
23354.50 -3.2	5 96.9 - 415	5. 18.01 264			3503. 15.02
23355.50 -3.0	9 94.7 399	3. 17.22 253		86.7	3356. 14.31
23356.50 -3.1	0 -93.2 383	4. 15.67 260			3215. 13.82
23357.50 -2.5	6 91.3 367	9. 16.00 196	4056 8.13	83 • 4	3076. 13.22
23358.50 -3.8	5 89.7 352	5. 15.44 379	4108 8.57	81.8	2940. 12.72
23359.50 -2.2	4 87.5 337	7. 14.71 167	6048 8.98	79.6	2866. 12.07
23360.50 -3.3	3 86.2 323	0. 14.27 318		78 . 4	2677. 11.69
23361.50 -3.3	7 84.0 308	6. 13.53 332		76.1	2547. 11.03
23362.50 2.8	0 82.4 294	6. 13.02 -262	1	74.6	
23363.50 -3.0	7 80.4 280	9. 12.40 305	9087 10.62	72.6	2302. 10.03
23364.50 -2.0	8 78.6 267	4. 11.87 180			
23364.95 -1.3	7 78.4 261	4. 11.79 92	7023 10.98	70.6	2133. 9.49
			- 4.1.000 - 1		

		Control of the Control				TENO.	- UTNO	WEL	WIND	DIREC
STAND HGT		TEST WGT	27.	LADZ IN	LT HG 1	7.0 C	6.9	KTS		DEG MA
3000000		1000	HX			THE RESERVE		STA	NDAPD D	AY
The same of			TE			UBR	EBR	KTAS	DIST	KE
TOD	ACCEL	GND-SPD	DIST	KE	FBR		.00	136.3	7847.	31.26
25743.95	-4.07	145.3	8988.	36.04	78.	.904		134.5	7668.	30.42
25744.75	-3.66	143.4	8792.	35.11		0.000	.01	132.4	7449.	29.47
25745.75	-4.14	141.3	8552.	34.05	462.	.020		129.8	7232.	28.34
25746.75	-3.92	138.7	8315.	32.81		.016	.18	127.8	7021.	27.46
25747.75	-3.54	136.6	8083.	31.84	52.	.002	.20	125.5	6812.	26,50
25748.75	-3.80	134.3	7854 .	30.77	545.	.022	.37	123.6	6608.	25.68
25749.75	-3.56	132.3	7629.	29.86	381.	.016		121.4	6407.	24.79
25750.75	-3.49	130.1	7408.	28.88	434.	.017		119.3	6209.	23.96
25751.75	-3.58	128.0	7190 .	27.95	685.	.027	.69	117.4	6015.	23.19
25752.75	-3.25	126.0	6976.	27.09	401.	.016	.86	115.5	5824.	22.44
25753.75	-3.76	124.0	6765.	26.26	1149.	.044		113.4	5637.	21.65
25754.75	-2.65	121.9	6557.	25.38	9.		.97	111.8	5453.	21.04
	-3.42	120.3	6352.	24.70	1025.	.038	1.07	109.9	5272.	
5756.75	-3.46	118.4	6151.	23.91	1224.	.044	1.29		5093.	19.55
5757.75	-3.10	116.2	5953.	23.04	918.	.033	1.53	107.8	4919.	18.9
25758.75	-3.18	114.6	5758.	22.42	1154.		1.69	106.3	4747.	
25759.75	-3.23	112.7	5567 .	21.67	1320.	.046	1.94	104.4		
25760.75	-2.87	110.5	5379.	20.85	1005.		2.19	102.3	4577.	17.1
25761.75	-3.13	109.2	5193.	20.33	1387.	.C48	2.37	100.9	4413.	
25762.75	-3.29	106.3	5011.	19.45	1693.		2.71	98.6		15.8
25763.75	-2.87	105.1	4832.	18.85	1281.	.044	2.96	95.9	4089.	15.3
	-2.41	103.7	4656 .	18.35	805.		3.11	95.6		
25765.75	-3.17	102.0	4482.	17.76	1788.		3.37	93.9	3779.	
	-2.73	100.4	4312.	17.22	1325.		3.50	92.4		
25767.75	-3.34	98.4	4144.	16.52	2149.	.073	3.95	90 • 4	3479.	
25768.75	-2.74	96.6	3979.	15.94	1517.	.051	4.23		3334.	
25769.75	-3.57	94.5	3817.	15.23	2598.	.089	4.64	86.5	3189.	12.6
25770.75	-2.45	4 4 4	3660 .	14.73	1329.	.045	4.90	85.0	3051.	
25771.75	-3.57		3504.	14.11	2751.	.093	5.26	83.1	2913.	
25772.75	-3.16		3353.	13.49	2346.		5.65	81.1	2778.	
25773.75	-2.72	87.2	3204.	12.99	1880.	.054	5.94	79.5	2648.	
25774.75	-3.53	100	3057 .	12.46	2918.	.098	6.29	77.7		The second second second
25775.75	-3.25		2915.	11.87	2665.	.090	6.69	75.7	2394.	
	-3.35		2776 -	11.38	2854.	.094	7.04	74.0	2272.	9.2
25776.75	-3.28		2640 .	10.80	2843.		7.44	71.9	2153.	
25777.75	-3.30		2507.	10.32	2936.		7.81	70.2	2037.	
25778.75	-3.22	4000	2378.	9.76	2912.		8.20	68.1	1924.	
25779.75	The second second	THE ASS. CO. LEWIS AND ADDRESS.	2252.	9.28	2687.		8.55	66.3	1814.	
25780.75	-2.98		2128.	8.83			8.92	64.5	1707.	
25781.75	-3.41		2009.	8.41	2927.		9.26	62.8	1605	6.6
25782.75	-3.08		1892.	7.83			9.72	60.4	1501.	
25783.75	-4.11	37 -27	1779.	7.46	4000		10.03	58.8	1466	
25784.75	-2.34		1559.	7.12			10.31	57.3	1313	
25785.75	-2.95		1561.	6.69	T (12.5%)	170 10 11 2	10.67	55.3	1221	
25786.75	-3.35			/			11.00	53.5	1133	. 4.1
	-2.97	60.8	1458 .					51.6	1047	. 4.1
25787.75		1000	4756	E. 00	3671	127	11.35	21.0	Turi	
25788.75 25789.75	-3.43	58.8	1356.	5.90			11.35	49.8	965	

STAND WGT	TEST WGT				TEMP		VEL	WIND	DIREC
36000.LBS	35400.LBS	27.	403	TN HG	18.0 C		KTS	210.0	DEG MAG
		***			- 011 h				,6
	GND-SPO	DIST		. FBR			KTAS	ANDARO I	KE
27557.11 -3.8		-				.00	130.9	7550	
27558.004.6		8050 .	29.0			•15	128.6	7349.	26.34
27559.00 -3.76		7823.	28.0	_		. 29	126.1	7129.	25.32
27560.00 -3.34	131.7	7599.			0.100	.29	124.0	6914.	24.52
27561.00 -3.67	7 129.6	7378 .	26.3		.018	.34	122.0	6703.	23.71
27562.00 -3.76	5 - 127.3	7162 .	25.4	1 663	.029	.47	119.8	6494.	22.85
27563.00 -3.58	2 125.1			3 - 518		.60	117.5	6290.	22.02
27564.00 -3.59	123.2	6739.			.032		115.6	6090.	21.31
27565.00 -3.47	121.0	6533.	22.9	3 773.		.88	113.4	5892.	20.50
27566.00 -3.59				6 1000.		1.02			
27567.00 -3.14		6131.	21.4		.028	1.21	109.4	5509.	19.08
27568.00 -3.42				1 1136.	-045	1.37	107.7		18.50
27569.00 -2.88		5743.	20.1			1.54	105.8	5141.	17.83
27570.003.57		5553.				1.76	103.9		17.19
27571.002.86 27572.00 -3.52	109.5 2 -107.6		18.7	8 849 6 1657			102.0		16.59
27573.00 -2.88		5184.	47 4	5 979	.063	2.47	100.2	4612.	16.00
	104.1	4827	16.0	9 1181.	.044	2.62	96.7	4441.	15.34 14.91
27575.00 -2.67	102.0	4653.	16.29	9 992.	.037	2.88	94.6	4112.	14.25
27576.00 -3.00		4482		7 1419.		3.05	93.3		13.86
27577.00 -3.00		4314.		1525		3.35	91.1	3795.	13.23
27578.00 -3.08		4149.		8 - 1680				3641.	12.75
	95.0	3987.		1787			87.7	3489.	12.25
27580.00 -2.24		3828.				4.08		3342.	11.80
27581.00 -3.00		3671.	13.3			4.26	84.9	3199.	11.48
27582.00 -3.26	90.1	3517.	12.7		.079	4.59	82.8	3055.	10.93
27583.00 -2.58		3367.	12.2			4.86	81.0	2916.	10.46
27584.00 -2.74		3219.	11.8			5.07	79.7	-2781.	_ ,
27,585.00 -3.19		3074.	11.3			5.38	77.7	2646.	9.63
27586.00 -3.43		2932.	10.8			5.71	76.0	2515.	9.19
27587.00 -2.85		2793 •	10.37			6.02	74.1	2387.	8.75
27588.00 -3.26		2657.	9.9			6.33	72.3	2262.	8.33
27589.00 -2.64		2524.	9.5			6.61	70.8	2142.	7.98
27590.00 -3.01		2395.	9.09			6.90	68.9	2023.	7.58
27591.00 -3.17 27592.00 -3.19		2267.	8.68			7.21	67.2	1908.	7.20
27593.00 -3.19		2144. 2023.	8.23 7.83			7.55 7.87	65.3 63.5	1795.	6.79
27594.00 -3.29		1905.	7.41			8.21	61.6	1686. 1579.	6.43 6.04
27595.00 -3.28		1791.	6.9			8.55	59.5	1475.	5.65
27596.00 -2.46		1680.	6.6			8.82	57.8	1376.	5.32
27597.00 -2.94					.097			1280.	
27598.00 -2.85		1466.	5.97			9.37	54.6	1187.	4.75
27599.00 -2.54		1363.	5.6				53.1	1098.	4.49
27.600.00 -3.34			5.3			9.91	51.3	1010.	4.19
27601.00 -3.54	56.4	1166.	4.99			10.23	49.3	924.	3.88
27602.00 -3.49	54.2	1073.	4.61	3509.	.129		47.1	841.	3.53
27603.00 -3.26		983.	4.29		.120	10.87	45.3	764.	3.27
27.504.00 -3.16		896 .	4.0			11.14	43.5	690.	3.02
27605.00 -3.18		<b>B13</b> .	3.70			11.42	41.6	618.	2.76
27606.00 -3.15		732.	3.39			11.70	39.5	550.	2.49
27607.00 -3.44		655.	3.17			11.95	38.0	487	2.30
27608.00 -3.64		581.	2.83			12.26	35.5	424.	2.01
27609.00 -3.10		511.	2.58			12.50	33.6	367.	1.80
27610.00 -2.33		444.	2.35				31.8	313.	1.61
27610.36 -1.79	38.3	421.	2.30	2032.	.070	12.72	31.4	295.	1.57

TEST NO. 37	Д	MA	ARK II	ANTIS	KID/	BFG T	CRES/OR	Y RUNWAY	Y 1 - 1	127	ing say of
	.6	TEST WGT	4 0	RESS	ALT		TEMP	WE WIND	VEL-		DIREC
STAND HGT.		42700.LBS		. 565		G :	19.8 G	2.4	KTS:	.4 30.0	DEG MAG
43000 • L BS	- "	42700.653		. 702		1		ma fr	7 1		all party.
1 3			TE	ST DA	Y				5		D'AY
7.00 A	CCEL	GND-SPD	DIST	KF		FBR	USR	E BR	KTAS	DIST	KE
, 5.,	4.95	146.6	3646.	40.6		1164.	.047	. 04	147.2	3691.	
	6.71	143.7	3430 .	39.0			.146	-64	14463	3474.	
- 1554 ame	8.07	139.1	3191	36.9		5862.	.224	1.90	139:7	3235	37.17
		134.2	2961 .	34.0		7059.	.255		134.9	3005.	34.64
	8.66	129.0	2739.	.31.4		7557.	.250	5.04	129.8		32.07
4 1	8.62	123.8	2525.	28.9		8597.		6.76	124.6	2570.	29.54
	9.14		2321.	26.3			339	8.69	119.0	2365.	26.97
24558.25 -1		11001	2127 .	23.7		0135.	329	10.66	113.1	2172.	24.34
	9.82		1942	21.3			340	12.54	107.4	1987.	21.94
	9.85		1768	19.1		9762.	.312	14.27	101.8	1813.	19.73
	9.10		1602	17.1		9838.		15:87	96.5	1647.	17.73
	8.97		1446.	15.3		0098.		17.41	91.3	1490.	
	9.00		1298	13.5		0357.		18.90	86.0	1342.	14.08
	9.02	•	1160 .	11.9		9697.		20.25	81.0	1203.	12.48
	8.36		1030 .	10.0		9262.	-	21.45	₹ 76.3	1072.	11.08
×11	7.89			9.			345	22.69	4 71.3	948.	9.67
	9.07		907	7.74		0828		23.91	66.0	834.	8.29
	8.81		794 .	6.		9342.		24.94	61.0	728.	7.09
F 42024 = -	7.56		690 •	5.		9888		25.84	56.7	629.	6.12
_ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-7 - 88	_	593.	- 4.		9226.	_	26.67	52.2	539.	5.18
_ , _ ,	7.28		504.	4.		0343		27.45	47.8	455.	4.35
_ ,	8.04		422.			0259		28.20	43.1	379.	3.53
	-7.89		348 •	3.		0258		28.84	38.7		
	-7.81		283.	1.		9300.		29.40	33.9		
	-7.03		225	1.	-	6436.		29.77	30.6		_
	-4 - 83		174.	1.	-	4305		29.87	28.9		
24576.92	-3.19	26.9	143.	1.	J f	4000			1		

TANO WGT	TEST HGT		PRESS	ALT.		TEMP	MIND	VEL	WI:1D	DEG HA
8000.LBS	38350.LBS	1	27.569	IN HG		22.5 C	1.3	K12	0.0	DEG HA
			TEST D	v				ST	ANDARD	DAY
	GND-SPD	DIET	ESI OF		RP.	UBR	EBR	KTAS	DIST	. KE
		3158	77.	1 1	211.	.062	. 07	130.4	3015.	
6606.50 -5.2				6 . 7		172		-134.8	2792.	30.56
6607.50 -6.9		2923		7 5	124.	.234	1.75	130.3	2575.	
6608.50 -7.9		2695				.288	3.05	125.6	2366.	26.53
6609.50 -8.9		2475			175.		4.67	120.1	2166.	24.28
26610.50 -9.7		2264			194.	749	6.45		1975.	21.94
26611.50 -10.2	5 116.1	2063			566.		8.09	118.6	1794.	
6612.50 -9.4		1872	. 56.					102.9	1621.	10000
26613.50 -10.2		1690		53 9		100	11.27	97.4	1458.	100
26614.50 -8.8	1 98.9	1519			360.		12.81	91.8		
26615.50 -10.3	6 93.1	1356		7.5	447.		14.30		1159.	7.00
26616.50 -9.1	8 87.2	1204			294.		15.61		1023.	1000
26617.50 -9.1	9 81.9		. 11.		531		16.90	75.5	895.	
26618.50 -9.3	8 76.4	928			956					3 3 3 2 2
26619.50 -9.6	4 70.8	803					18.15	64.6	667.	
26620.50 -9.2		689			248		19.31		567.	- THE E- Z
26621.50 -10.3	0 59.4	584	. 5.		613		20.45		476.	1000
26622.50 -10.0	3 53.2	488	. 4.		470		21,53	52.8		
26623.50 -9.0		403			403	and the con-	22.42	47.5		
26524.50 -8.2	3 42.6	328	. 3.		613		23.15	42.4	322.	400
26625.50 -7.4	The second second	260	. 2.		803		23.76	37.8	0.000	
26626.50 -7.8	The second second	199	. 1.	90 9	370		24.28	33.6		
26627.50 -7.5	7	147	. 1.	38 9	083	320	24.76	28.8		
26628.15 -4.8		117	. 1.	15 5	930	292	24.89	26.3	118.	1.16

TEST NO. 38A	MARK II	[ ANTIS	SK TD/BF G	TIRES	WET RUN	WAY (WATE	P ONLY)		
STAND WGT 43000.LBS	TEST WGT 43200.LBS		PRESS AL	_T HG _	TEMP 15.5 C	W1ND 6.5			DIREC DEG MAG
		тс	ST DAY-				ST	ANDARD	)ΑΥ
	L GNU-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	_ KE
23060.55 =4.4		H737.	45.14	,	0.000	0.00	147.0	7994	41.11
23061.50 -4.4		8492	43.71		0.000	0.00	144.5	7763.	39.77
23062.50 -4.2		8239.	42.18		0.000	0.00	141.9	7524	38.33
23063.50 -3.7		7991.	40.92		0.000	0.00	139.7	7290.	37.14
23064.503.5		7746.	39.71		-0.000	0.00	- 137.5	7060.	36.01
23065.50 -3.7		7504.	38.47	324.	.012	.10	135.3	6833.	34.85
23066.50 -3.5		7267.	37.41	272.	.010	• 14	133.4	6611.	33.85
23067.50 -3.4		7033.	36.23	219.	.008	.23	131.2	6391•	32.75
23068.50 -3.9		6802.	35.22	948.	.034	• 35	129.3	6175.	31.80
23069.50 -3.7		5575.	33.83	951.	.033	•65	126.6	5961.	30.50
23070.50 -3.1		6352	32.89	264.	.009	.73	124.8	5754.	29.62
23071.50 -3.5		6132.	31.90	974.	.033	• 88	122.8	5548	28.70
23072.50 -3.6		5916.	30.85	1227.	.041	1.13	120.7	5346	27.72
23073.50 -3.3		5704.	29.90	1023.	.034	1.34	118.7	5149.	26.83
23074.50 -3.3		5495.	28.89	1204.	.037	1.60	~116.6~	4954	25.89
23075.50 -3.9		5289.	27.99	2224.	.067	1.94	114.7	4762	25.05
23076:50 -3.9		5087.	26.74	2409.	.072	2.49	112.0	4572.	23.89
23077.50 -2.7		4989.	26.01	876.	.027	2.71	110.4	4390.	23.20
23078.50 -3.9		4593.	25.06	2645	■078	3.10	108.3	4208	22.33
23079.50 -3.6		4502.	24.20	2393.	.071	3 • 54	106.3	4030.	21.52
23080.50 -3.7		4314.	23.21	2634.	.077	4.04	104.0	3856.	20.60
23081.50 -3.6		4131.	22.32	2577.	.076	4.50	102.0	3686	19.79
23082.50 -4.1	7 105.4	3950.	21.24	3411.	.099	5.11	99.3	3517.	18.78
23083.50 -3.3		3774.	20.43	2370.	.068	5.57	97.3	3355.	18.03
23084.50 -3.3		3502.	19.57	2457.	073	6.03	95.1	3195	17.23
23085.50 -3.6	8 99.5	3432.	18.92	3023.	.088	6.45	93.5	3040.	16.63
23086.50 -3.6	0 96.8	3267.	17.91	3037.	.088	7.02	90.8	2886	15.70
23087.50 -4.1	8 94.8	3104.	17.18	3888.	•115	7.55	88.9	2737.	15.03
23088.50 -2.9	0 92.6	2947.	16.40	2284.	.065	8.02	86.7	2592	14.31
23089.50 -4.4	5 90.6	2792.	15.70	4442.	.128	8.55	84.7	2450.	13.66
23090.50 -4.3	2 87.9	2542.	14.75	4379.	.127	9.23	82.0	2311.	12.81
23091.50 -3.2	7 85.3	2495.	13.93	3068.	.08B	9.78	79.5	2176.	12.04
23092.50 -3.6		2352.	13.41	3584.	.104	10.21	78.0	2047	11.57
23093.50 -3.6		5513	12.64	3693.	.106	10.75	75.5	1920.	10.86
23094.50 -3.6		2078.	12.02	3844.	.113	11.24	73.6	1797	10.30 9.69
23095.50 -3.8		1946.	11.35	4123.	.119	11.77	71.3	1677	
23096.50 -3.4		1917.	10.71	3665	.105	12.26	69.2	1561.	
23097.50 -3.3		1593.	10.18	3577.	.102	12.69	67.3	1449.	8.63 8.10
23098.50 -3.8		1571.	9.60	4410.	126	13.19	65.2	1340.	7.55
23099.50 -3.1		1454.	8.99	3430.	.097	13.65	63.0	1234.	7.37
23099.95 -2.6	2 67.8	1402.	8.79	2793.	•081	13.72	62.2	1188.	1 + 3 1

TEST NO. 38H	MARK III	L ANTISK	ID/BFG	TIRES/W	ET RUNW	AY (WATE	S ONLA)		**
• *	·	m **	mee 41	·	TEMP	WIND	VFI	WIND	DIREC
STAND WGT	TEST WGT		ESS AL 435 IN		8.5 C	6.1	KTS	215.0	DEG MAG
38000.LRS	38200.LBS	~ 1 •	435 14	10 1	303 0				
		TES	T 1) A Y ==				STA	ANDARD D	ΔΥ
TOD : ACCEI	GND-SPD	DIST	KE	FBR "	UHR	EBR	KTAS	DIST	KE
			38.52		0.000	0.00	142.2	7254.	34.04
		7907.	37.24		0.000	.00	139.8	7020•	32.86
		7658	36.24		0.000	.00	137.8	-6792	31.94
		7413.	34.98	211.	.009	.04	135.3	6565	30.78
	7	7172.	34.01	60.	.003 -	⊌04	133.3		29.89
24947.00 =3.86 24948.00 =3.53		6935.	32.82	0.	0.000		130.8	6126	28.80
24949.00 -3.94	•	6701.	31.93	510.	.021	.13	129.0	5912.	27.98
24950.00 -3.2			30.80	0.	0.000	•52	126.6	5701.	26.94
24951.00 -3.50		6245.	30.03	305.	.013	•53	124.9	5495	»26.24.
24952.00 -4.3		<b>6022</b> •	28.90	1390.	.057	• 49	122.4		25.21
24953.00 -4.0		5804.	27.82	1196.	.048	•76	120.0	5090	24.22
24954.00 -4.1		5589.	26.80	1542.	.058	1.07		4893	23.29
24955.00 -3.9		5379	25.83	1620.	.059	1.37	115.4	4701.	22.41
24956.00 =3.9		5172.	24.75	1716.	.063	1.76	112.8	4511.	21.42
24957.00 -3.3		4969.	24.00	1105.	.039	1.98	111.0	4327	20.74
24958.00 -3.8		4770.	23.16	1905.	•067	2.29	109.0	4147.	19.97
24959.00 -4.3		4575.	22.16	2594.	.089	2.76	106.5	3968	19.07
24960.00 -4.1		4384.	21.19	2536.	• 086	3.26	104.0	3793.	18.19
24961.00 -3.6		4197.	20.39	1953.	.067	3.62	101.9	3624.	17.46
24962.00 -4.0		4013.	19.40	2639.	•093	4.12	99.2	3456	16.56
24963.00 -4.0		3635.	18.69	2721.	.093	4.56	97.3	3296	15.92
24964.00 -3.7		3660.	17.70	2486	.084	5.07	94.5	3136.	15.03 14.37
24965.00 -3.7	_	3488.	16.98	2596.	-08B	5.49	92.4	2981.	
24966.00 -3.7		3321.	16.32	2663.	•090	5.90	90.5	2831 •	
24967.00 -3.8		3157.	15.53	2833•	•098	6.37	88.2	2683	12.50
24968.00 -3.8		2997.	14.89	2964	•097	6.81	86.2	2541.	
24969.00 -3.2		2841.	14.16	2361.	.078	7.22	83.9	2401.	
24970.00 -3.7		2587.	13.58	3048.	-102	7.62	82.1	2265. 2131.	
24971.00 -4.0		2538.	12.90	3414.	.114	8.11	79.8	2003.	
24972.00 -3.3	and the second second	2393.	12.26	2769.	.092	8.54	77.7	1877•	
24973.00 -3.8		2251.	11.62	3386.	.115	8.99	75.4	1754	
24974.00 -3.8	5 80.7	2113.	11.01	3476.	.118	9.47	73.3	1637.	
24975.00 -3.3	5 78.5	1980.	10.42	2969.	.099	9.90	71.1 69.1	1522	
24976.00 -3.3	5 76.4	1948.	9.87	3030•	.103	10.29	67.0	1410.	
24977.00 -4.3	5 74.3	1721.	9.34	4295	•143	10.77	64.6	1302.	
24978.00 -3.2	3 71.8	1598•	8.72	3057.	.099	11.22	62.8	- 1199	
24979.00 -3.4	4 70.0	1,	8.28	3342	.113	11:58	60.6	1098	4 - 49
24980.00 -4.2	2 67.7	1361.	7.76	4350.	.144	12.05 12.47	58.2		
24981.00 -3.3	65.3	1249.	7.22	3387.	.115	12.87	56.4	908	E: 0E
24982.00 -4.0		1140.	6.81	4253.	•139		53.9	818.	_
24983.00 -3.9		1036.	6.28	4259.	.144	13.32	51.6	733	
24984.00 -4.2		935.	5.81	4668		13.76 14.18	49.1	651	_
24985.00 -3.6	9 56.0	938.	5.31	4034		14.62	46.8	572	_
24986.00 -4.7		745.	4.87	5344	-181	15.02	44.4	499	
24987.00 -3.6		657.	4.44	4147.		15.44	41.8	429	
24988.00 -4.8		572.	4.00	5623•		15.79	39.2	364	
24989.00 -3.		493.	3.57	3611.		15.79	38.8	352	
24989.20 -2.9	45.6	477.	3.51	3416.	• 1 1 1	10017		<del>-</del>	

TEST NO. 38	3C	MARK II	I ANTIS	KIDZBEG	TIRES/	WET RUN	WAY (WATE	S ONLY)		
, 23, 112						TEMP	wIND		ONTW	DIREC
STAND WGT		TEST WGT		RESS A		25.0 C	7.4		215.0	DEG MAG
34000.LBS	3	4225.LBS	21	.433 IN	כורי	22 • W C	, •			
			тс	ST DAY-				ST	ANDARO D	)AY
		CND-CDD	DIST	KE DAIL	FBR	UHR	EBR	KTAS	DIST	KE
		GND-SPD 140.4	7125.	29.86		0.000	. 0.00	129.8	6096.	25.34
207100.7	-3.73	138.7	6929.	29.13		0.000	0.00	128.1	5921.	
	-3.70		6597	28.23		0.000	0.00	126.0	5714.	23.88
	3.63	136.5 134.1	6469.	27.24	403.	.019	.07	123.6	5508.	23.00
	-3.95	132.1	6244	26.42	131.		.10	121.6	<b>5308</b> •	22.27
		129.8	6023.	25.53	325.	015	.18	119.5	5111.	21.48
	3.63	127.7	5806	24.72	709.	.033	.27	117.4	4918.	20.76
	-3.89	125.3	5593.	23.78	349.	.016	.44	115.0	4726	19.91
	-3.41	123.7	5383.	23.17	87.	.004	.45	113.4	4542	19.37
20,0	-3.05	121.6	5176.	22.40	321.	.014	.53	111.4	4359.	18.69
	-3.12	119.8	4972	21.76	720.	.030	.63	109.7	4180.	18.12
	-3.35		4771.	20.93	972.		.A4	107.5	4002.	17.39
	-3.47	117.5	4574	20.33	1076.	.042	.99		3830.	16.86
	-3.41	115.8	4381.	19.41	1892	.073	1.36	103.2	3657	16.04
	-4.05	113.2	4191.	18.86	1057.		1.55	101.7	3492.	15.56
	-3.19	111.6	4005.		2118.		1.91	99.2	3327.	14.81
	-4.05	109.0	3823.	-17.27	2572		2.32	97.0	3166.	14.16
	-4.38	106.8	3545.	16.34	2963		2.85	94.1	3008.	13.34
	-4.63	103.9	3472.	15.66	1458		3.19	92.0	2856.	12.74
	-3.11	101.7 99.6	3302	15.03	2755		3.55	90.0	2708.	12.18
	-4.24		3136.	14.26	2100.		3.98	87.5	2562	11.51
20,,000	-3.53	95.2	2973.	13.74	2326		4.31	85.7	2422.	11.06
	-3.67 -3.46	93.0	2815.	13.11	2185		4.67	83.6	2285.	10.51
	<b>-4.61</b>	90.4	2559.	12.38	3515.		5.16	81.0	2149.	9.88
	-3.45	88.2	2509	11.78	2358		5.57	78.8	2019.	9.36
	<b>-4.30</b>	85.8	2362.	11.16	3363.		6.00	76.6	1892.	8.82
	-3.63	63.4	2219.	10.53	2756.		6.44	74.2	1769.	8.28
	-3.84	81.4	2080.	10.05	3042.		6.81	72.3	1650.	7.86
	-3.83	79.1	1945.	9.49	3100.	.118	7.23	70.0	1535•	7.38
	-3.90	76.8	1913.	8.93	3267.		7.65	67.7	1423.	6.90
m,	-4.11	74.5	1585.	8.40	3566		8.08 🕏	65.5	-1314.	6.45
	-4.15	72.0	1561.	7.85	3676.		8.53	63.0	1209•	5.98
	-3.78	69.7	1442.	7.36	3355.		8.93	60.8	1109.	5.57
	<b>-4.20</b>	67.3	1327	6.86	3865		9.35	158.5	1013.	5.15
	-4.33	64.7	1215.	6.34	4085		9.81	55.9	919.	4.71
	-2°.90	62.4	1108.	5.91	2615.		10.15	53.B	831.	4.35
	<b>-3.</b> 83	60.9	1003.	5.62	3655		10.46	52.2	<b>7</b> 47 •	4.11
-,	-2.82	58.6	911.	5.20	2647		10.70	50.0	673.	3.76
27013.16	-2.02	30.40	/114	545.0		-				

EST NO. 3	40	MARK	III ANT	IZKIDNO	UNLOP T	TKEOVAC	, i Kolina	•		
E31 404 3						EMP		VEI	WIND D	IREC
TENT CHAT	- 1	EST WGT	PRE	SS ALT		. 0 C	2.6	KTS	325.0	EG MAG
	1. 7	8850.LBS	27.0	571 IN F						
			1					STA	NOARD DA	14
•			0707	KE	FBR	UBR	EBR	KTAS	DIST	40.27
CCT	ACCEL (		DIST	41.88		* 000	0.00	145.5	8162.	
2911.25	-5.63			39.92	• -		10.00	142.3	7928	38 . 39
2912.25	-5.45			38.31		*000	0.00	139.1	7699•	36.85
22913.25	-4.51		<b>-</b>	37.02			0.00	:136·B	7.474	35.61
22914.25	-3.51	138.1	7773.	35.97	488	. 016	.04	134.8	7252.	34.61
22915.25	-3.60	136.1		34.85	0.	*000	. 12	132.1	10070	
22915.25	-3.24	134.0	1979.	33.91	89.	.003	. 12	130.9	6818.	32.64
22917.25		132.2		32.83	943.	. 032		128.5	6606.	31.60
22913.25	-3.77	130.0		31.73	361.	.012	. 42	125.7	6398.	30.55
22919.25		127.9		30.82	251.	.008	. 47	12419	6192.	29.67
22923.25		126.0	6435.	30.01	975.	031	. 58	123.2	5989.	28.90
22921.25	-3.47	124.3		29.00	537.	.017	. 75	121.1	5790	27.93
22922.25		122.2		28.13	4657.	- 052	- 97	119.3	5594.	27.10
22923.25		120.4	5811.	20.13	1400-	.034	1.29	117.0	5401.	26.04
22924.25		118.0		27.03 26.28	1087	.032	1 . 45	115.3	5211.	25.32
22925.25	-3.07	116.4	5412.		1803.	152	1.78	113.3		24.42
22925.25	-3,49	114.3	5218.	25.34	1200.		2.04	111.5	4841.	23.65
22927.25	-2.99	112.4			1409.		2.28	109.7	40014	22.92
22923.25	-3.07	113.7	4838		2241.	.066	2.65	137.7	4483.	22.08
22923.25		108.6	4653.	22.91			3.05	105.6	4309·	21.24
22931.25	-3.41	106.5	4472.	22.02	2032		3.41	103.7		20.45
22931.25	-3.28	194.5	4294	21.21	2798	.081	3 - 84	101.5	3970•	19.66
22932.25	-3.77	132.5	4118.	20.38	2409	770	4.29	99.4		18.83
22933.25	-3.41	130.2.			2468.	068	4.64	97.8	3645.	18.22
22934.25	-3.34	98.0		18.85	2793.	.082	5.10	95.6	3488.	17.39
2207= 25	-3.55	96.3	3615.	18.01	3171.		5.57	93.5		16.63
22935.25	-3.75	94.2		17.22	2896.	.082	6.05	91.3	3182.	
22937.25	-3.47	92.0		16.43	3431.	.097	6.52	89.3	3035.	15.18
22939.25	-3.80	93.0	3144.	15.71	1508.		6.85	57.5	2891.	14.57
22937.25	-2.33	88.1		15.08	3633.	.105	7.22	86.0	2748.	14.08
22941.25	-3.85	86.5		14.57			7.73	83.7	2611.	13.33
22941.25	-3.58	84.3	2702.	13.79	3369		8.23	81.4		12.61
22942.25			2561.	13.04	3450.		8.65	79.6	2344.	12.07
22943.25	-3.33	80.2	2425.	12.48	3202.	002	0.10	77.4	2216.	11.42
22944.25			2292•	11.73	3215.	0.05	9,49	75.8	2091	10.93
22945.25			2161.	11.28	3279.	. 108	9.97		1969.	10.30
22943.25			2035.	10.63	3756					9.76
22947.25			1911.	10.07	3181		10.83	69.8	1735	9.27
22943 25		70.2	1791.	9.55	4360.		11.36	67.1	1623	
22949.25	-3.83		1675.	8 • 5 4	4313.		11.80		1515	
22953.25			1562•	8.53	4007.		12.20	63.3	1410	7.6
22951.25			1454.	7.85	3597.		12.55	61.5	1308	7.1
22952.25			1348.	7.40	3631•		13.02	59.3	1209	6.7
22953.25			1245.	6.89	4941				1114	. 6.2
22954.2			1147.	6.38	4412		13.83	55.0	1023	
22955.2			1052.	5.92	3174		14.17	53.4	933	
22955.2	-		960.							
6622206			871.	5.03	3863					_
22957.2				4.98	3341	094				

5331.

5209.

6120 .

6209.

5446 .

5557.

4589.

.170

. 204

. 201

.179

.181

.150

14.35

14.65

14.94

15.18

15.38

15.47

32.1

29.4

26.5

23.6

21.2

19.3

281.

231.

186.

146.

109.

85.

1.74

1.46

1.18

. 94

.75

• 62

2.12

1.84

1.54

1.25

.99

.79

.66

297

244.

197.

154.

115.

90.

-4.44

-4.30

-5.02

-5.04

-4.38

-4.44

-3.62

25386.00

25387.00

25388.00

25389.00

25390.00

25391.00

25391.73

35.1

32.7

29.9

26.9

24.0

21.5

19.5

STAND HGT.		TEST HGT	F	PRESS	ALT.	TEHP	WIND	VEL	HIND	DIREC
36000.LBS		35200.LBS	27	.678	IN HG	22.6 C	.9	KTS	0.0	DEG MAG
36000 L BS			TF	ST DA				01	AND ADD	
TOD A	CCEL	GND-SPD	DIST	KF	FAR	IIRR	FRD	KING	BICT	741
27345.68 -	4.17	123.2	58543	23.6	7 962	- 041	_ n 1	123.0	5962.	24.12
27346.50 -	3.30	121.4	5685	22.9	5 123		13	121 2	270C+	27 70
27346.50 - 27347.50 -	3.43	119.5	5482	22.2	4 378	.016		440 7	5584.	23435
27348.50 -	3.45	117.4	5282	21.4	8 530	.023	26	117:3	5704	24 00
27349.50 -	3.24		5085	20.7	7 402	.017	34	111.66	5182.	21.90
.27350.50 -:		113.4	4892	20.0	4 953	. 040	4.0	117.3	9102.	21.10
27351.50 -			47.0324	10.3	9 207	000	.56	"T#3" 2		
27352.50 -			4516.	48.6	6 1503	.009	76	400 7	4794. 4604.	19.79
27353.50 -			47771	4.0.0	3 958	04.0				19.04
.27354.50			44 57.1	17 2	5 1488	050	.93	107.5	4419	
27355.50 -			3077 L	15 6	1 1341		1.20		4237	.17.61
27356.50 -			3805		0. 1526		1.42	103.2		16.96
27357.50 -			3636		7 4554	. 060		101.5	3883.	
27358.50 -		07 2	74.78 1	4 1. 7	2 1552		1.94	99.1	3712.	15.66
27359.50 -		97.82	37703	46.0					3543.	15.04
27360.50 -3		970 U		14.0			2.53	95.0		14.39
27361.50 -3	3.77	00.0	3149.º				2.89	92.7	3:218.	13.70
27362.50 -	3.37	90.0		12.8			3.17	90.8		13.14
27767 50 -3	3.01	00.0	28 43.			.092	3.52		2906.	12.53
27363.50 -3	7 77	00.5	26.95				3.86		2756.	11.93
27364.50 -3	3.37	04.5	2551.	11.1			4.17		2609.	
27365.50 -3	3.96	62.4	2410	10.5	9 2924		4.53	82.5	2466.	10.85
27366.50 -4	4.10	79.0	22/35		2 3259		4.98	79.9	2327.	
27367.50 -3	3.24	77.6		9.3	_		5.32	77.7 75.8	2192.	9.63
.27368.504		75.7	2010.	8.9			5.68	75.8		9.16
27369.50 -3				8.4			6.05		1933.	8,62
27370.50 -3			1763	7.9			6.41	71.4	1808.	8.13
27371.50 -3	3. 54		1645.	7,4			6.76	69.1	1688.	7.60
27372.50 -3			1530.	6.9			7.12	67.1	1571.	
27373.50 -3		64.9	1419	6.5			7.47	65.1	1457	
27374.50 -4		62.3	1312	6.0					1348.	
	3.73		1209.	5.5			8.26	60.1	1244.	
27376.50 -3		57.7	1109-	5.1				57.9		
			1013.	4.7			8.99	55 • 4	1045.	4.88
27378.50 -3	3,73	53.2	922.	4:4			9.30	.53.4		4.55
		50.5	8345	3.9			9.67	50.8	862.	4.12
27380-50 -4		48.2	751.	3.6			10-00	48.6	. 7.76.	3.76
27381.50 -4			672	3.2			10.33 10.64 10.94	46.2	695. . 619.	3.40
27382.50 -3	5.81	.43.4	597.	2.9			10.64	-43 ₋₈	. 619.	
	4.26	41.1	525.	2.6			10.94	41.4		2.73
		38.6	458.	2.3			11.22	39. U		2.42
27385.50 -4	+.82	36.3					11.46	36.7	412.	2.15
	.18	33.9	335.	1.7			11.75	.34.3	350.	1.58
	39	31.3	260.	1.5			12.01	31.7	294.	1.60
	+.82	28.8	230-1	1.2			12.26	29.2	242.	1.36
	.39	25.7	184.	1.0		.179	12.50	26.1	194.	1.09
	.01	23.1	142	• B		. 204	12.70	23.6	150.	. 89
	.15	20.2	105	•6			12.85	20.7	113.	. 66
	2.57	18.2	73.	- • 5			13.01	18.7	.79.	. 56
27392.68 -2	2.47	17.9	68.	.5	0 2952.	. 103	13.01	18.4	73.	.54

152: 40. 404	TEST NO. 40A	MARK III	ANTISKID/DUNLOP	TIRES/WET	RUNWAY
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STAND WGT 41000.LBS	TEST WGT 41500.LBS	PRE 27.6	SS AL	T HG	TEMP 16.8 C	WIND •4	VEL KTS		DIREC DEG MAG
	· 	TFS3	T DAY				STA	NDARD (	)ΔΥ
	L GND-SPD		KE	FAR	UBR	EBR	KTAS	DIST	KE
23493.61 -4.0							137.6		
23494.50 -3.6				60.			135.5		33.33
23495.50 -3.4	7 135.3	6958 - 13	33.61	5.	000				
23496.50 -3.9	0 .133.1	6732. 3	32.56	707.	•027	.10	131.4	6480	31.35
23497.50 3.5	7 130.8	"6509 · · · 5	1.45	- 442.	.016	23	129.2	6266	-30-29-
23498.50 -3.3		6290. 3	30.46	279.	.010	•30	127.1	6056.	29.34
23499.50 -3.4	7 126.9	6074 2	9.56	585	.021	- 38	125.2	-5848	-28.47
23500.50 -3.8	1 124.7			1171.		·58	123.1	5644.	
23501.50 -3.9	3 122.3	5653 2				.87	120.8	5444.	26.48
23502.50 -3.5				1032.		1.10	118.7	5247.	25,56
23503.50 3.6					.044	····1 • 34	116.6		
23504.50 -3.3				1065.	•036		114.5		
23505.50 -3.8		4856 - 2				-1.85	112.5	4677	-22.97
23506.50 -3.6	7 111.7	4665. 2	2.92	1772.		2.19	110.3	4494	22.09
23507.50 -3.2						2.46	108.3	4315.	-21.28
23508.50 -3.2	7 107.9	4295. 2	1.38	1473.	.049	2.69	106.6	4138.	20.61
23509:50 -3.5						3.03	104.4	3965	
23510.50 -3.5			9.78		.067	3.36	102.5	3795.	1.9.07
23511.50 -3.3		3765 - 1					100.2		
23512.50 -3.5			8.30			4.04	98.6		17.64
23513.50 -4.0		3428. 1				4.56	96.0	3305	16.72
23514.50 -3.3					.074		94.0		16.04 15.34
23515.50 -3.3			5.90	2391.	•077	- 5.33 5.73	90.0		
23516.50 -3.5			5.23		.088	5.72	88.1		14.69
23517.50 -3.2			4.59	2845.	078	6.52	85.8	2557.	13.38
23518.50 -3.5			3.86 3.30	2561.	•093 •082	6.87		2417	
23519.50 <b>-</b> 3.2 23520.50 <b>-</b> 4.5			2.59	4364	•138	7.39	81.8	2280.	12.15
23521.50 -3.1			1.83	2630.	.082	7.87	79.3	2149.	11.42
23522.50 -3.6			1.35	3302.	.106	8.23	77.7	2019.	10.96
23523.50 -3.6			0.66	3489.	.110	8.71	75.3	1894.	10.29
23524.50 -3.8			0.04	3819.	.120	9.18		1771.	9.70
23525.50 -3.4			9.46	3338.	.103	9.62	71.0	1653.	9.14
23526.50 -3.1			9.01	3023.	•097	9.97		1538.	8.71
23527.50 -4.3			8.39		-146	10.46		1426.	8.10
23528.50 -3.3			7.82	3424.	.106	10.89		1318.	7.56
23529.50 -3.8									
23530.50 -4.1			6.82	4672.	.146	11.77	60.3	1113.	6.59
23531.50 -3.7		1051.	6.27	4150.	131		.57.8	1016.	·· 6.07
23532.50 -4.2		954.	5.80	4868.	.151	12.65	55.6	922.	5.61
23533.50 -4.4		861.	5.26	5219.	.160	13.12	-53.0 -	-833.	5.09
23534.50 -3.9			4.76	4716.	.143	13.56	50.4	748.	4.61
23535.50 -3.9	0 48.8	689.	4.38	4663.	•143	-13.93	48.4	667 <b>•</b>	- 4-24-
23536.50 -4.1	7 46.4	608.	3.95	5069.	<ul><li>156</li></ul>	14.32	45.9	589.	3.83
23537.50 -4.6	0 43.9 -	532.	3.54	5688	175	-14.72	43.5	-515.	3.43
23538.50 -4.1			3.12	5111.		15.11	40.8	446.	3.02
	2 38.8-					-15.47	38.5		2.69
23540.50 -4.5	35.8	330.	2.35	5743.		15.85	35.5	321.	2.29
	33.2								197
23542.50 -5.1			1.68	6607.		16.51	30.1	212.	1.64
	3 27 . 1				227	-16.A4			
23544.50 -4.9			1.03	6520.		17.14	23.6	124.	1.01
23545.16 -2.93	3 22.1	102.	90	3948.	•119	17-22	22.0	100.	

STAND _ WGT	TOOT HOT	D.	DECC 4	1 7	TEMP	. U TNO	VFI	MIND	DIREC
.S.I.ANU NG I	37550.LBS		.670 TH	HG	17.5 C	1.3	KTS	30.0	DEG HA
38000.LBS	01220.FR2	21	OLC IN	חט	4119	703			
		TE	ST DAY-				ST	AND ARD	3AY
T DD 60001	これり こくりり	T27N	KE	FRR	IIAR .	. FBR	KTAS	DIST.	KE
25762-99 -4-21	134.2	6610	29.94	504 •	.021	.01	135.0	6755.	30.65
25762.99 -4.21 25763.75 58	131.9	64231	28.93	1106.	. 047	22	132.7	6566.	29.62
26766 75 <b>- 8</b> 2	120.4	<b>ムフロマン</b>	27.H.S	.5 1475	- 1172	• 3 (	130	00400	
25765.75 -3.49 25766.75 -3.85	127.3	5986et	26.95	92 .	. 004	. 39	128.1	.5124.	27.50
25766-75 -3-65	125.2	5773.	26.06	641.	.026	.48	126.0	5907.	26.70
257.67 - 7.5 3.38	427.4	5554.	25.1H	255.			123.9		··· - 62 P D T
25758.75 -4.12	120.8	5356	24.26	1255.	.049	.74	121.6	5486.	24.88
25750.75 -7.76	118.6	5156.	23,36	. 523.	020	91	119.4	5281.	23. 97
25770.75 -3.67 25771.75 -3.68	116.5	4957	22.57	. 995	.036	1.05	117.3	5080.	23.16
25771.75 -3.68	114.3	4763	21.74	1108.	043	1.25	115-2	4882.	22.32
25772.75 =3.43	117.0	4572.	20.86.	1552	นอย	1.53	112.9	40000	- CT - 43
25773.75 = 3.58	109.8.	4384.	20.05	1262.		1.7.8	110.7	4498.	20.61
25774.75 -3.96	107.7	4201	19.27	1829.	.071	2.07	105.5	4311.	19.81
257.75.753.64	105.3	40 21.	18.43	.1607	.060.	2.39	. 106.2	4129	18.96
25776.75 -3.25	103.4	3845	17.76	1262	.047	2.62	104.2	3950.	18.27
	101.1	3672	16.98		. 896	2.99	102.0	3774.	. 17.49
25778.75 -3.33	98.7	3504.	16.18	1579	.060	3.35	99.5	3603.	16.67
25779-75 -3.28	97.0	3339.	15.64	1617 .		3.5€	97.9	3435.	16.12
25780.75 -3.82	94.7	3177	14.90	2363	.086	3.93	95.6	3270.	15.37
25761.75 -4.12	92.5	3019.	14.22	2811	. 103.	. 4.32	93.4	3109.	1468
25782.75 -3.59	89.9	2865	13.44	2310 .	.085	4.73	90.5	2.953.	13.88
257.63.7.5 = 3.23	86.0	2715	12.87	. 1982	072	5.04	88.9	2800.	13.31
25777.75 -4.29 25778.75 -3.33 25779.75 -3.82 25780.75 -3.82 25781.75 -4.12 25782.75 -3.59 25783.75 -3.77 25785.75 -3.76	86.1	2568	12.32	2687	099	5.37	87.0	2650.	12.75
25785.75 -3.76	.83.6	2425.	.11.61	2782	192	5.80	84.5.	2504	12.02
25786.75 -3.70	81.6	2285	11.07	2802	. 102	6.16	82.6	2361.	11.47
25767.75 -3.22	79.4	2150.	10.48	2345	.083	6.52.	80.4	2.223.	10.55
25788.75 -3.74	77.3	2016	9.95	3037.	. 106	6.87 7.28 7.62	78.3	2067.	10.32
25789.75 -3.87	75.2	1886.	9.41	3256	• 117.		762	1956.	. 9.77
25790.75 -3.19	73.1	1763.	8.87	2558.	090	7.62	74.0	1828.	9.22
25791.75 -5.13	70.7	1641	8.32	4886		8.50 8.86	.71.7.	1703.	6. 66
25792.75 -2.86	68.1 66.2	1525	7.72	2341	083	8.50	69.1	1585.	0.04
25793.75 -4.23		1411.	. 7.29	4022	. 140	. 8.8€	67 2	1465.	
25794.75 -3.66			6.77	3425	. 122	9.27	64.8	1 355.	6.07
25795.75 -4.15	61.5	1195	6.28	4077	143	9.67	. 62.5	1.247	6.58
25796.75 -4.15 25797.75 -3.80	59.0	1894	5.80	4162	148	10.09	60.1	1142.	6.07
25797-753.80	56	9 96	5.31	3.827.	134_	1045	5.7 • .6.	1042.	5. 57
25798.75 -2.77	54.7	902	4.97	26711.		711 4 5 19	774/	7401	2 1 6 6
25799.75 -5.37		811.	4.5.8	5777	200	11.17	53.5		4.002
25800.75 -3.97		726.	4.03			11.60	50.3	764.	4.26
25801.75 -4.12	. 47.1	645	3.69	4457		11.94		680	
25802.75 -4.13		5 67	3.30	4534		12.29	45.7	600.	
25803-75 -4.44			2.96		172			524.	
25804.75 -4.87		425	2.55	5528	• 190	13.00	40.3	452.	
25805.75 -4.76			2.24			13.33	.37 .8.		2 . 40
25806.75 -4.70		302	1.88	5439		13.66	34.6	325.	
25807.75 -5.46		247.		. 6388		_13.98	_31.7.		1.69
25808.75 -5.07		198.		5984		14.27	28.5	216.	
25809-75 -5.21			98	6194		14.54		17.0	
25810.75 -3.41		116.	•79	4135		14.69	23.0	129.	
25810.77 -3.21	21.7	115,1	<b>.</b> 79	. 3913	132	.14.69	22.9	. 125.	5 5

TEST NO - 41A	MARK	III AN	TISKID/S	STANDARD	TIRES	/WET RUN	NAY		
STAND WGT	TEST WGT	ပု	KESS AL .545 IN	HG 1	TEMP	WIND 0.0	VEL	0.0SS	DIREC DEG MAG
7 - 10 /n + water a - 191		T	~* DAY				ST	ANDARD [	)AY
			ST DAY	FBR .	UBR	. EBR	KTAS	DIST	KE
	Q. (12 Q	DIST	42.61	0.0		0.00	150.5	8969.	43.12
24143.40 -4.34		8863.	41.41		0.000	0.00	148.4	8751.	41.90
24144.25 -4.03		8648	40.11	0.		0.00	146.0	8499 •	
24145.25 -4.42	146.3	8399	38.69	٥	0.000		143.4	8252	
24146.253.38	143 m/c ···	7913.	37.75	148.	.007	.01	141.7	8008	38.20
24147.25 -4.07	141.9	7576	36.42	0	0.000	.09	139.1	7.768 • .	36 •.86
-24148,25		7443.	35.41	171.		1.0	137.2	7532 •	35.84
24149.25 -3.67		7213.	34.21	427	-016	-22.	134.8	7299	34.61
24150.25 -3.75				. F A	014	. 22	132.6	7070	.33.49
24151.25 -3.64	132.9	6764	32.05	737.	026	46	130.5	". 6845.•.	32.43
24152.25 3.74	_	6546	- 1 C	- /1	(1) (1) (1) (1)	~ ~ ~	1660	UULT	
24153.25 -3.04		6330 •	30.15	119.	004	54	126.6	6405 • .	30.51
24154.25 = 3.08	100 1	(117	20 35	397.	-014	•58	164.7	OI3∩ •	27010
24155.25 -3.22 24156.25 -3.36	125.1	5207.	28-40-	729	.025	.72_		5978	2B <u>74</u>
								5769.	
24157.25 -3.13 -24158.25 -3.51	121.3	5/02	26-67	1.161-	.039	1.01	119.1	5564.	
								5362.	
24159.25 -3.49 24160.25 -2.97	111.91	5103.	24.89	7.01	.024	1.43	_ 1.150	5164.	
24160-25	113.3	4910.	24.08	1618.	.054	1.67	113.1	4969 •	
24161.25 =3.57 24162.25 =4.19	111 5	4721	23.30	2539.	085	2.01	111.43	4777	
24102-25 4-19								4589.	22.39
24163.25 -1.59	109.1	4350	22.31	790.	.026	2.34.	108.9	4402	
		4170.	21.12	1739.	.058	C. 11	106.0	4220.	
24165.25 -3.36		. 3992	20.42	1882.	063	3.04	104.2	4.040	
24166.25 -3.41 24167.25 -3.23		3818.	19.65	1762.	•057	3.37	102.2	3863.	19.89
C-1701AMO		3646.	18.91	1901.	.062	.3.69	100.3		. 19.13
C 12001-		3479.	18.22	1526.	.050	3.96	98.4	3520.	
		3314.	17.52	2583.	.083		96.5	3353•	
24170.25 -3.63 24171.25 -3.50		3152.	16.72	2512.		4.74	93	3190.	
		2995.	16.05	1838.	059	.5.08	32.4	3030	
		2840.	15.51	5555.	.070	5.36	90.8	2874•	
		2688.	14.80	2287.	.072		88.7	. 2720 •	
24174.25 -3.12 24175.25 -3.12		2539.	14.29	2348.	.075		87.2	2570	
		2394		1529.	•048		85.1		13.78
24176.45 -2.08		2365	13.53	1087.		6.37	84.8	2393•	13.70
24176.45 -2.08	,								

TEST NO. 418	MARK III	ANTISKI	ID/STANDA	RD TIRES	S/WET RUN	IWAY	4-	
STAND WGT 38000.LBS	TEST WGT-	PRESS	AL.T	TEMP	MIND	VEL -	MIND	DIREC
38000.LBS	37700.LBS	27.544	IN HG	20.0 C	0.0	KIS	100.0	DEG MAG
• • •	-	TEST OF		-three				,
-TOD ACCE	L CNO-CDD DIC	- 16.51 DA	E00		500	KTAC	I ANDARD L	)AY
26893.80 -4.3	0 140 2 710	) - NE	· FOR	00K	E.DR	170 E	7074	32 29
26893.89 -4.3 26804.75 -3.7 26895.75 -4.2	0. 177 0 . 600	12 21 7	76 D	0.000	0.6	136 5	10140 607E	31 33
26895 75 =4.2	2 136.0 676	n. 31 F	15 556	0.000	3.0	134 3	44/17	~"3T'•\Z\?"
26896.753.8	2 .133.3653	4 29 6	6 273	011	. 24	171 7	6425	20.16
26897.75 -3.7	4 131.1 631	0. 28.7	0 321		_ 2H	120 E	620E	28 22
26897.75 -3.7 26898.75 -3.6	8. 128.9 609	27.7	2 308	016	- 30	127 3	5080	27 25
26899.75 -3.2	5 126.9 587	5. 26.8	19	001	-40	125.3	5777.	26.43
26900.75 -3.6	0 124.8 566	2. 25.9	8. 576	023	.49	123.2	5568.	25,55
26900.75 -3.6 26901.75 -3.5 26902.75 -4.2	8 122.9 545	3. 25.1	9 647	. 025	59	121.3	5362	24.77
26902.75 4.2	9 120.4 524	8. 24.1	7 1633	062	.87	118.9	5160.	23.77
26903.75 -3.49	9 118.1 504	7. 23.2	9 819 2 - 742	032	1.08	116.7	4963.	22.90
26904.75 -3.3	2 116.2 484	9. 22.5	2 - 742	029.	1.23.	114.7	4768	.22.14
26905.75 -4.0	0 114.2 465	4. 21.7	7 1648	064	1.44	112.8	4577.	21.41
26906.75 -3.5	0 111.8 - 446	4. 20.8	8 . 1216		1.73	.110.5.	4390.	.20.53
26907.75 -3.83	2 109.7 427	7. 20.1	0 1721	- 064	1.99	108-4	4206.	1.977
269.08.75 3.19	9-107-4-409	41.9.2	4 1094	041	2.28	106.0	4026	18.92
26909.75 -3.5		4. 18.6	8 1538	058	2.47	104.5	3849	18.37
26910.75 -3.69		8. 17.7	91908	. 069	2.84.	102.0	.3676	17.49
26911.75 -3.23			6 1463					
26912.75 -3.89	5 - 99.3 - 339	516.4	6 -2282		3.43	98.1.	3339	16.18
26913.75 -3.86	5 97.0 323 5 94.6 306	0. 15.7	1 2416. 3 2404.	• •087	3.82	95.8	3176.	15.45
26914.75 3.79	5 .94.6 306	8. 14.9	3 2404.	• •086	4.22	93.4	3.017.	14.68
26915.75 -3.83	92.4 291	0. 14.2	6 2578.	• 091	4.61	91.3	2862	14.02
26916.75 -3.48	90.4 275	6. 13.6	5 . 2261	083	4.95	89.3	2710.	13.42
26917.75 -4.26	87.8 250	5. 12.8	6 3301 4 997 d	• •119	5.44	86.7		12.64
26918.75 -2.23	86.3 245	9. 12.4	4 997.	• • 035	.5.65	85.3	2418.	12.23
26919.75 -4.30		5. 11.7					2276.	
26920.75 -4.10					. 6.50	80 8	2138.	1099.
26921.75 -3.85	*	9. 10.4			6.97	78.3	2005.	10.31
26922.50 -3.66		0. 10.0			7.35	76.B		9.91
26923.75 -3.59 26925.00 -3.59			6 30 <b>3</b> 7.		7.76 7.97 8.51			9.21
26925.75 -3.19		3. 8.6 3. 8.3	ດ <b>ງປ/4</b> ເ ພ້າວກາ	• 107 • 096	7.97	11.2	1596. 1507.	8.54
26926.75 -3.82			* <i>CIC</i> 1.	135	0.00	67.5	120.	8.20
26927.75 -2.77	66.5 130	7	aaaaa.	. 091	0.22		1370	7 27
26927.75 -2.77 26928.042.09	66 2 136	1. (.)	, 6304.	001 001	7.66	45 A	12/9.	7.10
20720-04 2-05	→ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □ □	7. 1.3	T - 132/	- •·∩⊃⊅ ···	- JOCK	QD.+4	1749	/ 0.17

TEST NO. 42A MARK III ANTISKID/STANDARD TIRES/WET RUNWAY

			5 2	/.565 IN	H6 ·	16.5 C	3.0	KTS	233.0	DEG MAG
•		GND-SPD		EST DAY-				CT	ANDARD C	14 V
2886.04				KL .	TBR .	UBR	EBR	KTAS	DIST	KF_
	=3.84	158.7			U.	0.000	0.00	153.8	9275.	45.06
		156.4		46.80	0.	0.000	0.00.	151.6	9031.	43.75
		154.3	9370.		0.	0.000	0.00	149.5	8781.	42.55
2889.00			9111.				0.00	147.1	8533.	41.19
2890.00	-3.74		B657.	42.95		0.000		145.1		40.09
	-3.92	147.4	8506.	41.52			04		8051.	38.73
2892.00	-3.44	145.1	8359.	40.27		0.000		140.4	7816.	37.54
2893.00		143.1	Allo.	39.15	63.	.002	05 .	138.4	7584.	
2894.00	-3.23	141.0	7876.	38.02	0.	0.000		136.4		35.40
	-2.98	139.2	7540.	37.04	0.	0.000		134.6	7132.	.34.47
	-3.53	137.3	7406.	36.06	329.	.012	.07	132.7	6910-	33.53
2897.00		135.1	7176.	34.89	499	.018	21	130.5	6691	32-43
2898.00		133.3	6950.	34.00	52.	-002	22	128 A	6476	21 57
2899.00		131.3	6727	.32.95	.540 🕳		-33	126.7	6264	30-57
2900.00	-3.74	129.3	6507.	31.99	1148.	.039	• 48	124.9	6055.	29.67
290100		126.8	6290.	√30 •.73 ·	337.	011	73		5849.	28.47
2902.00	-3.35	126.0	6077.	30.35	877			121.5	5649	28.11
2903.00	-4.17	122.8	5867.	28.85	2302.	.072		118.4		26.69
2904.00	-3.32	121.4	5660.	28.16	1257.	.039	1.47	117.0		
2905.00	-4.45	119.0	5450.	.27.10	2912.	.089	1.95		5.06.0	
2906.00	-2.16	116.8	5201	26.08		0.000	2.20	112.4		
2907.00	-2.38	115.7	5064.		320	•010	2.21			24.06
2908.00	-3.67	113.7	4870.	24.71	2191.	.067	2.55	109.4	4689	
2909.00	-3.05	1.11.7	4579	23.85	1496				4505.	22.77
2910.00	-2.93	110.2	4493	23.24	1410.	.042	2.96	106 0	4325	
2911.00	-2.84	108.2	4308	22.41	1392.		3.14	106.0	4150.	
2912.00	-3.20		4126.	21.79	1958.		.3.43			
	-2.89		394d.			•057	3.69	102.5	3805.	20.01
	-2.88		3897.	20.83	1599. 1633.	.049	4.01	100.7	3638. 3589.	19.30

STAND WGT		TEST WGT			ALT		TEMP_	MIND		WIND	DEG MA
38000.LBS		38850.LBS	27	.570	IN HG		50.0 C	3.9	KTS	245.0	DEG MA
			TF	ST DA	Y				ST	ANDARD I	DAY
-T0D	ACCEL	GNU-SPD	DIST	KE	FBR	-	_ UBR	EBR.	KTAS	DIST	KE
	-4.41	160.8	9517.	44.4	6	0.	0.000	0.00	153.0	8458.	39.37
-	-4.46	158.7 -	9304.	43.3	2	0.	0.000	0.00	151.0	8264.	38.34
	-4.32		9039.	41.8	7	0.	0.000	0.00	148.4	8022.	37.03
	-4.38	The state of the s	8777.	40.5	2		0.000 -		145.9 -	7784.	35.81
	-4.10		8520.	39.2	4	0.	0.000	0.00	143.5	7551 •	34.65
- 1 P NO WOLD THE SEC.	-3.96		8268.	37.9	8	0.	0.000		141.1	7322.	33.51
	-4.10		8018.	36.7	8 10	2.	.004	.01	138.8	7096.	32.43
	-4.00		7774.	35.5	5 17	6.	007	.06	136.4	6874.	31.31
	-3.73		7533.	34.5	_	0.	0.000	.06	134.4	6656.	30.37
	-3.68	The second second	7296.	33.3		9.	.003	. 0.9	132.1 .	6441.	The second second second second
THE PROPERTY OF THE PARTY OF TH	-3.38		7062.	32.4	5	0.	0.000	.09	130.2	6231 •	28.52
	-3.41		6832.	31.5	2 1	3.	001 -	.09	128.3-	6023.	
	-3.49		6506.	30.5	3 26	4.	.010	.15	126.2	5819.	26.78
	-3.55		6382.	29.5	8 43	7.	.017	-22-	124.1	.5617.	25.93
	-3.85		6163.	28.6			.036	.38	122.1	5419.	25.07
	-3.29		5947.	27.6	5 40	2.	-015-	53	119.9	5225.	24.19
	-4.01		5734.	26.8	1 138		.053	.71	118.0	5034.	23.43
	-3.26		5474.	25.5	9 67			.94	115.2.	4799.	-22-33
	-3.47		5321.	24.9	7 102	9.	.03A	1.16	113.8	4662.	21.77
	-3.37	-118.4	5119.	24.1	2 . 101	3.	038-	1.36	111.8	4480.	21.01
	-4.13	116.3	4920.	23.2		-	.077	1.69	109.7	4302.	20.25
	-3.43		4727.	22.4			.049	1.98	107.6	4128.	
	-3.73	111.8	4536.	21.5			.068	2.32	105.4	3956.	18.67
	-3.62		4349.	20.8			.064	2.61	103.5	3789.	
	-3.39	107.5	4165.	19.8			.058	2.97	101.2	3624 •	17.22
	-3.13		3985.	19.2			050	3.19	99.6	_3464 .	
	-3.63	103.7	3908.	18.5			.076	3.53	97.4	3306.	15.97
	-3.86	101.6	3535.	17.7				3.92	95.3	_3151.	15.29
	-3.08		3465.	16.9			.059	4.27	93.2	3000.	14.63
	-3.04		3299.	16.4			.061	4.52	91.6	2852.	14.13
24960.86	-2.90		3199.	16.0	3 155	7.	.056	4.63	90.5	2763.	13.76

TEST NO. 42C	MARK	III AN	TISKIDAS	TANDARU	TIRES	WET KUN	YAW		
STAND WGT 34000.LBS	TEST WGT 34550.LBS		RESS AL		TEMP		VEL KTS		DIREC DEG MAG
		TF	ST DAY				ST	ANDARD D	AY
TOD ACC	EL GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
27164.65 -3.		7551.	31.58	0.	0.000	0.00	136.8	6753.	28.15
27165.50 -4.		7346.	30.63	313.	.017	.02	134.6	6566.	27.28
27166.50 -3.		7110	29.58		0.000	.04	132.3	6350 •	26.33
27167.50 -4.		6877.	28.53	157.		.05		6137.	25.37
27168.50 -3.		6548	27.61	80.	.004	.06	127.7	5929.	24.53
27169.50 -3.		6423	26.68	. 0.	0.000	.07	125.5	5724.	23.69
27170.50 -3.		6202.	25.86	56.	.003	.07	123.5	5523.	22.95
27171.50 -3.		5984	25:01	339.	.016	.11	121.4	5325.	22.17
27172.50 -3.		5770.	24.12	298.	.013	.20	119.1	5130.	
	47 123.8	5560.	23.43	319.		.22	117.4	4940.	20.74
27174.50 -3.		5353.	22.53	166.	.007	.28	115.3	4752.	
	37 . 119.8	5149.	21.95	465.	.019	34	113.5		19.39
27176.50 -3.		4948	21.25	665.	.029	.44	111.6	4386.	18.76
27177.50 -3.	45 115.7			760.	.034	61	109.5	:4208	
27178.50 -3.		4558	19.78	986.	.041	.75	107.6	4033.	17.43
27180.00 -3.		4274	18.63	1235.	.050	1.04		3776.	16.38
27180.75 -4.		4136.	18.11	1898.	.077	1.21	102.8	3650.	15.91
27181.50 -4.		3999.	1.7.44	2126.	082	1.75	100.9		15.31
27182.50 -4.		3820.	16.71	5085.	.083	5.05	98.7	3365.	14.65
27183.50 -3.		3546.	16.01	1594 .	. 064	2.33	96.5	3207.	
27184.50 -2.		3475.	15.45	528.	.021	2.49	94.8	3053.	13.52
27185.50 -6.		3305.	.15.01	4960 .	.194	.2.90	93.3	2902.	
27186.50 -4.		3144.	13.55	2887.	.111	3.69	88.5	2751.	11.80
27187.50 -2.		2985.	13.34	717.	.058	3.79	87.8	2611.	
27188.50 -3.		2830.	12.84	5510*	.085	4.05	86.1	2472.	11.16
27189.50 -4.		.2577.	.12.10	3170 .	.120	4.50	83.5	2334.	10.50
27190.50 -3.	35 86.7	2529.	11.49	2181.	.084	4.89	81.3	2201.	9.94
27191.50 -3.		2385.	11.00	2475.	.095	5.21	79.5	2073.	9.50
27192.50 -4.	26 82.2	2243.	10.33	3329.	.127	5.65	76.9	1945.	8.91
27193.50 -3.	45 79.9	2106.	9.75	2554 .	.096	6.05	74.7	1823.	8.39
27194.50 -3.	27 78.2	1973.	9.36	2413.	.092	6.34	73.1	1705.	7.52
27195.50 -4.	21 75.8	1843.	8.79	3509.		6.77	70.7	1588.	
27196.50 -3.		1718.	8.27	5665.	.101	7.15	68.5	1477.	7.06
27197.50 -3.	09 71.7	1595.	7.85	2454.		7.45	66.7	1368.	
27198.50 -3.	53 69.5	1475.	7.40	2983.		7.79	64.6	1263.	6.29
27199.50 -3.		1360.	6.98	3488.		8.15	62.7	1160.	5.91
27200.50 -3.		1248.	6.48	3434.		8.55	60.3	1061.	5.47
27201.50 -2.		1140.	6.08	2487.		8.86	58.3	967.	
27201.90 -2		1098.	5.96	1828.	.069	8.89	57.7	930.	5.01

STAND WGT	4	TEST WG1 +3000.L89		RESS AL •515 IN	HG .	TEMP	WIND 4.1	VEL	0.01S	DIREC DEG MAG
Total Street Str	7 m m m		TF	ST DAY-				ST	ANDARD D	AY
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBR.	EBR	KTAS	DIST	KE'
	-3.63	162.1	10571.	50.02		0.000	0.00	154.9	9785.	45.70
	-4.25	160.5	10462.	49.02	0.	0.000	0.00	153.3	9588	44.76
	-4.06	157.7	10193.	47.36	0.	0.000	0.00	150.6	9334.	43.20
	-3.87	155.5	9929.	46.0 L	0	.0.000.	00.0	.148.4	9086	.41.93.
	-3.64	153.3	9568.	44.76	- 0.	0.000	0.00	146.3	8841.	40.77
	-3.93	150.9	9411.	.43.35	0	0.000	0.00	144.0.	8599.	39.45
	-3.66	148.9	9158.	42.20	0.	0.000	0.00	142.0	8363	38.38
	-3.53		8909	40.87	0.	.0.000	00	139.7	8129	37.13
F - 2 . 2 . 2 . 2	-3.56	144.4	8563.	39.70	. ()	.0.000	.00	137.6	7898	36.05
	-3.78	142.4	8421.	38.61	338.	.013	02	135.6	7672.	35.02
B	-3.37	140.0	8183.	37.32	0.	0.000	.11	133.3	7448.	33.82
23579.00	-3.13	138.3	7948	36.41	0.	0.000		.131.6	.,	_32.97
23580.00	-3.59	136.3	7716.	35.34	522.	.019	.19	129.6	7012.	31.98
	-2.86	134.5.	7488.		0.	0.000	.20	127.9	6800	31.14
23582.00	-3.76	132.5	7262.	33.41	999.	.036	•32	125.9	6590	30.18
23583.00	-3.12		7041.	32.38	2.77 .	.010	.44	123.9	6382	29.21
23584.00	=3.33	128.6	6822	31.48	692.	.024	•53	122.1	6179.	28.38
23585.00	-3.37	126.6	6506.	30.53	860.	.029	•69	120.2	5978	27.50
	-3.47	124.7	6394	29.58	1100.	.038	.90	118.2	5781.	26.61
23586.00	, ,	122.6	6186.	28.59	739.		1.10	116.2	5587	25.70
23587.00	-3.11	120.8	5980	27.78	1145.	:039	1.28	114.5	5396.	24.94
23588.00	-3.31		5778	26.96	0.		1.39	112.7	5209.	24.18
23589.00	-2.33	117.7	5578	26.36	661.		1.43	111.4	5025	23.62
23590.00	-2.78		. 5381.		865			109.6	4842.	22.88
23591.00	-2.86		5187	24.89	1087.		1.76	108.1	4664 .	22.26
23592.00	-2.97		4995.		_1900.			106.0	4485.	21.40
.23593.00	-3.49		4808	23.23	1500.		2.39	104.3	4312.	20.72
23594.00	-3.06		4623.	-	1126.			102.5	4142.	19.99
	2.70		4563 •	22.24	771.		2.67	102.0	4086.	19.81
23595.33	-2.42	108.1	4503.	~~ • ~ ~						,

		ALDO TIESCHET HUNN	AY	
NO 43H MARK	III ANTISKIDISTA	INDARD TIRES/WET RUNI		
TEST NO. 43H MARK		TEMP WIND	VEI WIND UI	REC
STAND WET TEST WET	PRESS ALT	7 6	KTS 228.0 DE	G MAG
DIMITE AT	27.515 IN HO	20.0-0		
3000012			STANDARD DAY	
	TEST DAY		KTAS DIST	NE.
TOD ACCEL GND-SPD	DIST KE	ייביי חמע. אם:	147.7 8844.	36.68
	10379. 43.36	,,	145.7 8649.	35.72
2500111	10162. 42.28	0 0 0 0 0	142.5 8412.	34.62
52000.00	9898. 41.04		141.1 8179.	33.51
20007100 1E3 N	9637 . 39 . 79	V . V	130.9 7950.	32.46
25090.00	9381. 38.60	1130 = 444	136.3 7722.	31.26
25071.00	9129. 37.25	1719	134.4 7502.	30.40
25072.00	8881. 36.28	2.7	132.0 7283.	29.30
25073.00	8636. 35.03	737031 .23	129.8 7068	28.35
25694.00 -4.25 143.6	8396. 33.95	0. 0.000 .27		27.60
25695.00 -3.23-141.4	8159. 33.11	0. 0.000 .27	12041	26.81
25696.00 -3.02 139.0	7925 32.20	230009 .29	17005	25.89
25697.00 -3.52 13(.)		259011 .38	16411	25.26
25628-00 -3.43 135.4		0. 0.000 .38	122.5 6250.	24.36
25699:00 -3.07 133.9		856033 .54	120.3 6050.	23.67
25700.00 -3.72 131.0	7243. 29.42	q. 0.000 .57	11000	22.94
25701.00 -2.71 129.8	7023. 28.64	444 63	11000	20.34
25702.00 -3.21 127.9	6805 - 27 - 80	0.0.000 .64	115.2 5480.	22.34
25703.00 -2.47 126.4	6591. 27.12	912034 .74		21.68
23,000	6378. 26.37	735. 028 91	111.6 5112.	20.94
23107100 000 100 4	6170. 25.52	133	109.8 4932.	20.29
52103000 21-	5965. 24.78	200	108.1 4756.	19.67
23/00.00	5762. 24.06	1210	106.5 4584.	19.07
25/01.00	5563. 23.38	1 65	104.9 4412.	18.50
25100.00	5365. 22.72	1010	103.4 4246.	17.99
2510700	5172. 22.13	7777	101.3 4080.	17.27
23/10/00	4982. 21.32	942	99.9 3919.	16.79
	4794. 20.76	11,700	97.9 3757.	16.11
25/12 - 00	4505. 19.98	2402	95.9 3600.	15.48
23113	4427. 15.24 .	11444	94.3 3447.	14.96
2311700	4249. 18.65	1577053 2.96	92.7 3297	14.44
25/12.00	4074. 18.05	1044035 3.19	91.2 3151.	14.00
25716.00 -2.46 103.1 25717.00 -3.25 101.6		2037 - 069 3-44	89.2 3004.	1.3 • 38.
23111000 300 5		1957056 3.81	87.5 2862	12.89
25718.00 -3.11 99.5	36 36	2156074 4.13	85.7 2723.	12.34
25719.00 -3.22 97.0	35 41	1976066 4.49		11.98
25720.00 -2.99 95.9		705023 4.65		11.80
25721.00 -1.88 94.5	1 0 0	1375045 - 4.70	83.8 2522.	
25721.50 -2.41 93.9	3161. 14.98			

							aren entka	L. A.V		
TEST NO. 4	43C	MARK	III AN	TISK ID/S	TANDARD	TIRES	WET, RUN	WAT	age of a second	
			F3.1	area 11	_	TEMP	WIND	VEL.	WIND (	DIREC
STAND WG		TEST WGT	P:			9.0 C.		KTS	235.0 1	DEG MAG
34000.LBS		34700.LBS	21	.515 IN	m(1 C.	340 C	10	1 7		3 11
					1			STA	NUARO DA	AY
				ST DAY	FBR"	u6P	EBR	KTAS	DIST	ĶΕ
TOD		GND-SPD	DIST	KE		0.000	0.00	130.A	6506.	25.75
27630.54	+3.89	142.4	7519.	31.15		0.000	.01	128.4	6307.	24.83
27631.50	-3.66	139.9	7590 .	30.08	0.	0.000	.01	126.6	6105.	24.13
27632.50	-3.61	138.0	7356.	29.27	311.	ni#	06	124.4	.5905.	.23.31
27633.50	-3.95		7124.	28.32	. 22	001	.11	122.2	5708.	. 22.49
27634.50	-3.53	133.5	6898.	27.36	().	0.000	.11	120.4	5516.	2183
27635.50	-3.04	131.6	6674.	26.59	341.	.015	.14	118.5	5327	21.15
27636.50	-3.61	129.6	6453.	25.81	341.	0.000	17	116.6	5141	20.47.
27637.50	-3.08		6237 •	25.01	305.	.013	.22	114.6	4957	19.77
27638.50	-3.33		5023.	24.20	404	.018	.27	113.0	4778.	19.21.
27639.50	-3.36		5812.	23.54		.029	.43	110.7	4599	18.45
27640.50	-3.43		5505	22.66	645•	.026	.51	109.1	4426	17.91
27641.50	-3.29		5402.	22.02	57.1 • •	.050	.72	106.9		.17.21
27642.50	-3.71	117.5	5201.	21.21	1166.	.048	94	104.9	4086.	16.57
27643.50	-3.53		5005.	20.46	1127.	.041	1.14	103.0	3921.	15.96
27644.50	-3.27	113.4	4812.	19.75	1020.		1.35	101.1	3760.	15.38.
27645.50	-3.33		4522.	19.07	1205.	.048	1.63	99.1	3601	14.79
27646.50	-3.72	169.4	4435.	18.37	1730.		1.90	97.2		14.21
27647.50	-3.18		4253.	17.69	1278	.052	2.12	95.5	3294 •	13.71
27648.50	-3.21		4073.	17.11	1409		2.41	93.5		13.15.
27649.50	-3.40	103.5	3895.	16.45	1699	.063	2.73	91.7	2998.	12.65
27650.50	-3.74	101.6	3724 •	15.35	2145	. 057	3.06	89.4	2854	.12.03
27651.50	-3.04		3554	15.12	1499•		3.31	37.8	2715.	11.61
27652.50	-3.22	97.6	3386	14.62	1759	.067	3.55	86.1	2579	11.16
27653.50	-2.70	95.8	3225.	14.09	1.278	• U4.9	3.86	84.4	2445.	10.72
27654.50	-3.80		3064 •	13.58	2537.	•097	4.32			.10.11
27655.50	-4.07	91.5	2903.	12.85	2926	SLL	4.68	80.1	2184.	9.65
27656.50	-3.44	69.5	2755.	12.30	2323.	.091	5.05	77.9	2059	9.12
27657.50	-3.3	67.2	2606.	11.67		•085	5.35	76.3	1939.	8.75
27658.50	-3.2		2461.	11.23	2233•	.084	5.72	74-1	1820.	8.27
27659.50	-3.59		2313.	10.66	2715.	104	6.09	72.1	1704.	7.83
27660.50	-3.3		2179.	10.13	2555•	.1)48	6.37	70.6	1594.	7.51
27661.50	-2.97	79.6	2044.	9.74	2125	.080		68.5	1484	7.06
27662.50	-3.6		1911.	9.20	2971.		6.75	66.8	1378	6.71
27663.50	-2.9		1782.	8.79	2302.		7.06	65.0	1276	6.35
27664.50	-3.5		1556.	8.35	2962.		7.40 7.75	62.9	1176.	5.96
27665.50	-3.2		1533.	7.88	2713.		7.73	61.3	1080.	5.65
27666.50	-2.4		1414.	7.50	1891.		7.97	61.2	1076.	5.64
27666.54	-2.3		1409.	7.44	1327.	.069	1.91	01.	1010	
_10000										

TEST NO. 44A	MARK	TII ANT	ISKID/S	TANDARD	TIRESA	WET RUN	AY		
		0.	ŒSS AL	т	TEMP	WIND	VEL	WIND	DIREC
STAND WGT	TEST WGT	27.	ESS AL		2.5 C	4.3	KTS	240.0	DEG MAG
43000.LRS	43200.LBS	410	1400 111	-					
ł .		TES	T DAY				STAI		KE
**** ***	CEL GND-SPD	DIST	KE	FBR	USP	CON	KTAS	DIST	39.40
	3.48 151.5	9114.	43.91	0.	0.000	0.00	143.9	8211.	38.30
	13 149.5	3392.	42.72	426.	.017	.05	141.8	8005	37.17
23457.75 -4	3.27 147.3	3542.	41.49	0 4	0.000	* 0 b	139.7	-7775•	36.13.
	3.42 145.3	8395	40.36	0. •	0.000		137.8	7547	35.14
	3.53 143.3	8152.	39.30	12.	• 000	.06	135.9	7322 • 7101 •	_
	3.44 141.1	7912.	38.07	75.	.003	.10	133.7	6883.	33.06
	3.63 139.2	7575.	37.04	464.	.017	.14	131.8	6668	31.90
L.D. WELL	3.93 136.8	7442.	35.77	1006.	•036	• 36	129.5	6456	30.83
	3.27 134.5	7213.	34.61	283.	.010	-50	127.3	6249	30.00.
	3.71 -132.8	6987 ·	33.71	990.	.034	.61	125.5	6045	28.95
	3.04 130.5	6766.	32.56	253.	.008	.79	123.3	5845	
	2.74 129.0	6547.	31.65	0.		.79	121.9 119.9	5646	27.38
	3.74 127.0	<b>6330</b> .	30.85	1382.	. ()47	1.01	118.0	5451	
	2.88 125.0	6118.	29.88	388.	.013	1.18	116.2	5.30.	25.72
( ) ( ) ( ) ( )	3.27 123.2	5903.	29.03	1005.	.035	1.35	114.4.	5071.	7.7.
	3.04 121.3	5702.	28.13	800.	•029	1.50.	112.9	4887.	
	2.64 119.8	5495.	27.43	529	1017	1.64	110.4	4701 .	- 1
	4.88 117.2	5295	26.27	3720.	114	2.20	108.6	4523.	
23474.75 -	2.25 115.4	5102.	25.46	287.	.009		106.8	4346.	_
	4.09 113.6	4909.	.24.67	2864.	•086 630	3.17	104.7	4174.	
23476.75 -	2.80 111.4	4720.	23.75	1246.	.038	3.52	102.8	4003.	
	3.37 109.5	4532.	22.91	2102.		3.81	101.3	3837.	
	2.96 108.0	4344.	22.29	1632.	,040 .048	4.12	99.5	3673.	
23479.75 -	2.86 106.1	4169.	21.52	1580.		4.47	97.6	3512.	_
23480.75 -	3.16 164.1	3991.	20./3	2090	• 056 • 056	4.79	96.0	3354	
	2.96 102.5	3017.	26.09	1894.	• 025 • 077	5.23	93.9	3198	
23482.75	3.41 100.4	3545.	19.27	2598 • 2035 •		5.56	92.4	3047	
23483.75 -	2.93 98.8	3470.	18.00	_		6.00	90.3	2897	15.51
23484.75 -	3.24 96.6	3312.	17.65	2534		6.10	89.3	2806	
23485.38 -	2.02 95.7	3211.	17.50	941.	* V L O	0.10			

TEST NO.	44ਰੋ	MARK	III A	NTISKID/	STANDAR	DITIRES	WET KUN	MAY		
STAND WG	Т	TEST WOT		PEESS A	I T	TEMP	UNIW	VEL	WIND	DIREC
38000 LAS		38200.LBS		7.459 IN		25.0 C	4.2	1.6%	, ,,	DEG MAG
,		7	_				18.	- 4		
			T	EST DAY-				ST	ANDARD I	DAY
TOD	ACCEL	GND-SPD	DIST	KE	FAR	UBR	EBR 🌷	KTAS.	DIST	KE.
25996.92	-3.65	148.2	8463.	37.16	0.	0.000	0.00	139.9	7534.	32.94
25997.75	-3.99	146.4	8256.	36.22	- D.	.0.000	0.00	138.1	7.345	.32.08
25998.75	-3.85	144.1	8011.	35.09	0.	0.000	0.00	135.9	7120.	31.05
25999.75	-3.72	141.8	7770.	34.00	0.	0.000	. 0.00	133.7	6900.	30.05
26000.75	-3.54	139.7	7533.	33.01	0.	0.000	0.00	131.6	6683.	29.15
26001.75	-3.92	137.5	7299.	31.95	316.	.014	04	129.4	6470.	28.19
26002.75	-3.53		7069.	30.97	0.	0.000	.05	127.4	6260.	27.30
26003.75	-3.65	133.1	6842.	29.96	288.	.013	10	125.2	6053.	26.38
26004.75	-3.61	131.0	6519.	29.04	382.	.016	.16	123.2	5850	25.54
26005.75	-3.37		6400.	28.16	247.	.010	.22	121.3	5651.	24.75
26006.75	-3.24		6184.	27.25	199.	.00A	.28	119.2	5455.	23.92
26007.75	-3.50		5971.	26.45	. 615.	.025	36	117.4	5262.	23.19
26008.75	-3.41	122.9	5762.	25.55	638	.026	•51	115.3	5072.	22.37
26009.75	-3.21	121.0	5556.	24.75	523.	.021	- 62	113.5	4886.	21.65
26010.75	-3,63		5353.	23.94	1149.	.047	.80	111.5	4703.	20.92
26011.75	-3.66		5154.	23.04	1348.	.052	1.07	109.3	4522.	20.10
26012.75	-3.60	114.6	4959.	15.55	1380.	.054	1.33	107.2	4345.	19.35
26013.75	-3.57		4767.	21.45	1445.	057	1.58	105.3	4171.	18.66
26014.75	-3.46		4579.	20.67	1441.	.056	1.84	103.3	4002.	17.96
26015:75	-3.81	108.4	4394.	19.86	1956.	.078		101.2	3834.	17.23
26016.75	-2.91	106.3	4213.	19.09	1008.	.039	2.43	99.2	3671.	16.54
26017.75	-3.54	104.6	4035.	18.50	1842.	.071	2.66	97.5	3512.	16.00
26018.75	-3.39		3861.	17.73	1783.	066	2.99	95.4	3354.	15.31
26019.75	-3.74		3689.	17.02	2292.	.086	3.34	93.4	3200.	14.67
26020.75	-3.13		3522.	16.39	1661.	.062	3.64	91.6	3050.	14.10
26021.75	-3.31	96.3	3357.	15.68	1975.	.074	3.97	89.5	2902.	13.46
26022.75	-2.92		3196.	15.15	1589.	.059	4.21	87.9	2759.	12.99
26023.75	-3.43	52.6	3033.	14.49	2300 .	084	4.56	.85.8	2618.	12,39
26024.75	-3.25	90.8	2884.	13.93	2156.	.080	4.88	84.1	2480.	11.69
26025.75	-3.33	88.5	2732.	13.26	2335.	.088	5.26	81.9	2345.	11.29
26026.75	-3.24		2584.	12.74	2313.	.085	5.58	80.2	2214.	10.83
26027.75	-2.89		2439.	12.12	1986.	.073	5.94	78.2	2084.	10.28
26028.47	-1.63		2344.	11.91	539.	.019	5.99	77.5	2001.	10.09

TOOT NO /	. <i>i</i> . c	MARK	TIT AN	TISKI	INSTANDARE	TIRES/	WET KUN	MAY		
TEST NO. 4	140	//AIS-1	74.4.4		,					DIDEC
STAND WG	r	TEST WGT	p	RESS	ALT	TEMP	WIND			DIREC
<b>—</b> • • • • • • • • • • • • • • • • • • •	1	34550 LBS		456 1	IN 1115 2	27.6 C	5.2	KTS	195.0	DEG MAG
34000.L35		343349600								
			TF:	ST DAY	/				NDARD D	AY
TOD	ACCEL	GND-SPD	DIST		FBR ·	UBP	EBR	KTAS	DIST	KE 25.22
28054.35	-3.80	139,2	7345.	29.67	9 0.	0.000	0.00	129.4	6285	24.50
28055.25	-3.81	137.2	7135.	28.80	0 . 0 .	0.000	0.00	127.6	6100.	23.64
	-3.45	134.9	6906.	27.8	2 0.	0.000	0.00	125.3	5898	22.98
28056.25	-3.54	133.0	6579.	27.0	7 - 0.	0.000	0.00	123.6	5699.	22.21
28057.25	-3.71	130.9	6457.	26.19	9 0.	0 = 0 0 0	0.00	121.5	5503.	21.38
28058.25	-3.84	124.5	6238.	25.20		.013	. 05	119.2	5310.	20.84
28059.25	-3.59	126.9	6070.	24.6		.005	• 07	117.7	5168	
28060.00	-3.09		5564.	23.8		0.000	.07	115.7	4982	20.14
28061.00		_	5654	23.1		:017	.09	114.0	4799	19.55
28062.00	-3.59		5449	22.2		•018	.21	111.7	4618.	18.78
28063.00	-3.46		5246	21.0		.021	.25	110.0	4441.	18.20
28064.00	-3.42		5048	20.8		033	•39.	107.8	4267.	17.50
28065.00	-3.55		4852	20.1		.030	•52	105.9	4097	16.87
28066.00	-3.37		4561.	19.4		.039	.66	103.9	3929 •	16.26
28067.00	-3.43		4472.	18.7		.068	.86	102.0	3765.	15.66
28068.00	-3.91		4288.	17.8		.066	1.17	99.5	3603.	14.92
28069.00	-3.76		4107.	17.2		.047	1.35	97.8	3446.	14.39
28070.00	-3.29		3929	16.5		.063	1.58	95.7	3291.	13.79
28071.00	-3.54		3756	15.8			1.87	93.5	3140.	13.16
28072.00	-3.72			15.2			2.06	91.5	2992.	
28073.00	-2.13		3585	15.1			2.14	91.2	2852	
28074.00	-3.61		3419. 3253.	13.6			2.91	86.4	2701.	
28075.00	-5.46		3095	13.5			3.01	86.0	2568.	
28076.00	-2.17		2938	12.8	-	-	3.26	83.7	2433.	
28077.00	-3.06		2785.	12.3			3.55	82.1	2301.	
28078.00	-3.92			11.6			3.95	79.6	2172	
28079.00	-3.84		2635 • 2490 •	11.1			4.26	77.6	2046.	
28080.00	-3.19		2347.	10.6	_		4.55	75.9	1925	
28081.00	-3.58			10.1			4.87	73.9	1806.	
28082.00	-3.1		2203.	9.6			5.21	71.9	1690•	
28083.00	-3.8		2072	9.0			5.58	69.6	1577.	
28084.00	-3.4		1941.	8.6			5.89	67.8	1468.	6.92
28085.00	-3.3		1812.	8.1			6.22	65.9	1362	6.53
28086.00	-3.4		1587	7.7			6.57	63.9	1260.	
28087.00	-3.6		1566.	7.2			6.95	61.6	1160.	5.72
28088.00	-3.9		1448.	6.7			7.28	59.6	1064	
28089.00	-3.0		1334.				7.58	57.8	972	
28090.00	-3.4		1223.	6 • 4 6 • (			7.75	56.2	891	4.76
28090.90	-2.0	8 63.0	1126.		000	• • • • • • • • • • • • • • • • • • • •	,			

				o intabil	ADD TIDE	C/WFT S	RUNWAYZ	O FLAPS		
TEST NO. 4	45A M	ARK III	ANTISKI							T.DEC
STAND WG	1	EST WGT	PF	RESS AL	T	EWH.		VEL KTS	312.0	OFG MAG
43000 LBS		3200.LBS	27	502 IN	HG I	0 C	•.5	J =		2.1
			TES	T DAY					NOARO DA	\Y
		-ND-COD	DIST	KE	FBR	UPR	EBR	KTAS	DIST	KE 20
TOD	ACCEL (	170.0	15065.	55.30	2312.	.078		167.3	14522	53.30 52.99
23040.82	-3.67		14799.	54.97	0.0	0.000	.50	166 H	14265	51.64
23041.75	-1.86		14515.	53.57	1617.	.054	.65	164.7	13991•	50.85
23042.75	-3.09		14233.	52.75	0. (	0.000		163.4	13720	50.35
23043.75	-1.32		13953.	52.24	798.	.026	-82	162.6	13450 •	49.20
23044.75	-2.42 -2.77		13676.	51.04	1336.	.043	1.25	100	13182. 12919.	48.75
23045.75			13402.	50.57	0.		1.27	160.0	12655	
23046.75	-1.36 -2.46		13128.	49.57	974	.032	1.48	158.4	12394	47.17
23047.75	-2.26		12857.	48.94	738.	.024	1.64	157.4	12135	46.26
23048.75	-2.22		12589	47.99		.024	1.90	155.9	11878	45.46
23049.75	-2.29		12322.	47.16	878.	.028	2.12	154.5°	11623	44.78
23050.75 23051.75	-1.60	155.9	12058.		· · · · · · · · · · · · · · · · · · ·	0.000	2.21	152.3	11370.	44-15
23052.75	-2.49		11796		1224.	.038	2.39	151.0	11120.	43.38
23053.75	-2.17		11536.	,		026	2.63	149.4	10871.	42.51
23054.75	-2.12		11278.	44.10	807.	025	2.92 3.05	148.6	10626.	42.04
23055.75	-2.21	151.0	11023.	43901	956.	.029	3.50	146.6	10381.	40.89
23056.75	-2.42		10770.	42.42	1304.	.040	3.68	145.5	10139.	40.30
23057.75	-1.90		10518.	41.81	637.	.019		144.7	9899.	39.87
23058.75	-2.17	147.1	10270.	41.37	1021.	.030	3.83 4.21	143.2	9661	39.01
23059.75	-2.60	145.5	10023.	40.47	1620.	.046	4.54	141.8	9426.	38.26
23060.75	-2.24	144.1,	9779•	39.69	1177.	032	4.77	140.5	9193.	37.58 A.
23061.75	-1.96	142.8	9537•	38.99	828.	.022	4.81	139.9	9084.	37.25
23062.22	-1.91	142.2	9424.	38.65	778.	150.		J.		
	/. E u	MARK 111	LANTISH	1D/STAN	DARD TIR	ES/WET	RUNWAY	NO FLAP	S ····	
TEST NO.	400	PARTY III	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	•						DIDEC
STAND W	C.T.	TEST WGT	T F			TEMP	WIN	VEL		DIREC DEG MAG
38000 LB		38550 LBS	5 27	7.505 IN	HG 8	20.5 C		5 KTS.	100.0	שבט וואס
3000002									ANDARD I	) A Y
			TE	ST DAY-		Han	EBR	KTAS	DIST	KE
TOD	ACCEL	GNU-SPD	OIST	KE	FBR	UBR	.06	156.8	12227	
25280.80	-2.91	161.1	13097.	44.30	1099•	•04B	.30	155.1	11986.	40.46
25281.75	-2.36	159.4	12840.	43.36	501.	.021 .039	•44	153.9	11735.	39.84
25282.75	-2.72	158.2	12572.	42.70	829.	.061	.70	152.1	11487.	38.92
25283.75	-3.18	156.3	12306.	41.71	991. 207.	.011	.83	150.5	11242.	38.09
25284.75	-2.29	154.7	12044	40.82	956	•043	.97	149.2	10998.	37.42
25285.75	-2.66	153.3	11784.	40.11 39.25	1104.	043	1.26	147.5	10758.	36.62
25286.75	-2.64	151.7	11527.	38.44	962.	.038	1.54	146.0	10520.	35.86
25287.75		150.1	11272.	37.74	77.	.003	1.67	144.7	10284.	35.20
25288.75		148.7	11020	37.27	1012.	.037	1.77	143.8	10050.	34.77
25289.75		147.8	10769	36.40	1242.	.047	2.11	142.1	9818.	33.95
25290.75		146.0	10521. 10276.	35.74	700.	.027	2.31	140.8	-9588 •	. 33.34
25291.75		144.7	105104					139.3	9361.	32.65
				36 (1)	1321.	*11.211	2.00	10,00		22 12
25292.75	-2.61	143.2	10033.	35.01	1321.	•050 •015	2.60 2.75	138.2	9137.	32.12
25293.75	-2.61 -1.82	143.2 142.1	10033. 9793.	34.44	405.	•015	2.75	138.2	8913.	31.49
25293.75 25294.75	-2.61 -1.82 -2.40	143.2 142.1 140.7	10033. 9793. 9553.	34.44 33.77	405. 1147.	.015 .042	2.75 2.98		8913. 8692.	31.49 31.00
25293•75 25294•75 25295•75	-2.61 -1.82 -2.40 -1.86	143.2 142.1 140.7 139.6	10033. 9793. 9553. 9317.	34.44 33.77 33.25	405. 1147. 538.	.015 .042 .019	2.75 2.98 3.15	138.2	8913. 8692. 8473.	31.49 31.00 30.43
25293.75 25294.75 25295.75 25296.75	-2.61 -1.82 -2.40 -1.86 -2.37	143.2 142.1 140.7 139.6 138.3	10033. 9793. 9553. 9317. 9083.	34.44 33.77 33.25 32.63	405. 1147. 538. 1166.	.015 .042 .019 .043	2.75 2.98 3.15 3.36	138.2 136.8 135.8	8913. 8692. 8473. 8256.	31.49 31.00 30.43 29.82
25293.75 25294.75 25295.75 25296.75 25297.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09	143.2 142.1 140.7 139.6 138.3	9793. 9793. 9553. 9317. 9083. 8850.	34.44 33.77 33.25 32.63 31.98	405. 1147. 538. 1166. 868.	.015 .042 .019 .043	2.75 2.98 3.15	138.2 136.8 135.8 134.5	8913. 8692. 8473. 8256. 8041.	31.49 31.00 30.43 29.82 29.25
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35	143.2 142.1 140.7 139.6 138.3 136.9	9793. 9793. 9553. 9317. 9083. 8850. 8620.	34.44 33.77 33.25 32.63 31.98 31.37	405. 1147. 538. 1166. 868. 1234.	.015 .042 .019 .043 .032	2.75 2.98 3.15 3.36	138.2 136.8 135.8 134.5 133.1	8913 8692 8473 8256 8041	31.49 31.00 30.43 29.82 29.25 28.71
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75 25299.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35 -1.82	143.2 142.1 140.7 139.6 138.3 136.9 135.6 134.3	9793. 9793. 9553. 9317. 9083. 8850. 8620. 8393.	34.44 33.77 33.25 32.63 31.98 31.37 30.79	405. 1147. 538. 1166. 868. 1234.	.015 .042 .019 .043 .032 .044	2.75 2.98 3.15 3.36 3.61 3.86	138.2 136.8 135.8 134.5 133.1 131.9 130.6 129.5	8913. 8692. 8473. 8256. 8041. 7828. 7617.	31.49 31.00 30.43 29.82 29.25 28.71 28.22
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75 25299.75 25300.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35 -1.82 -2.11	143.2 142.1 140.7 139.6 138.3 136.9 135.6 134.3 133.2	10033. 9793. 9553. 9317. 9083. 8850. 8620. 8393. 8167.	34.44 33.77 33.25 32.63 31.98 31.37 30.79	405. 1147. 538. 1166. 868. 1234. 634. 1016.	.015 .042 .019 .043 .032	2.75 2.98 3.15 3.36 3.61 3.86 4.06	138.2 136.8 135.8 134.5 133.1 131.9 130.6 129.5 128.3	8913 8692 8473 8256 8041 7828 7617	31.49 31.00 30.43 29.82 29.25 28.71 28.22
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75 25299.75 25300.75 25301.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35 -1.82 -2.11 -2.07	143.2 142.1 140.7 139.6 138.3 136.9 135.6 134.3 133.2 132.0	10033. 9793. 9553. 9317. 9083. 8850. 8620. 8393. 8167. 7943.	34.44 33.77 33.25 32.63 31.98 31.37 30.79 30.27 29.72	405. 1147. 538. 1166. 868. 1234. 634. 1016. 989.	.015 .042 .019 .043 .032 .044 .023 .036	2.75 2.98 3.15 3.36 3.61 3.86 4.06 4.25	138.2 136.8 135.8 134.5 133.1 131.9 130.6 129.5 128.3	8913 8692 8473 8256 8041 7828 7617 7408	31.49 31.00 30.43 29.82 29.25 28.71 28.22 27.71 27.24
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75 25299.75 25300.75 25301.75 25302.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35 -1.82 -2.11 -2.07 -1.99	143.2 142.1 140.7 139.6 138.3 -136.9 135.6 134.3 133.2 132.0 130.9	10033. 9793. 9553. 9317. 9083. 8850. 8620. 8393. 8167. 7943.	34.44 33.77 33.25 32.63 31.98 31.37 30.79 30.27 29.72 29.72	405. 1147. 538. 1166. 868. 1234. 634. 1016.	.015 .042 .019 .043 .032 .044 .023 .036	2.75 2.98 3.15 3.36 3.61 3.86 4.06 4.25 4.47	138.2 136.8 135.8 134.5 133.1 131.9 130.6 129.5 128.3 127.3	8913. 8692. 8473. 8256. 8041. 7828. 7617. 7408. 7201. 6996.	31.49 31.00 30.43 29.82 29.25 28.71 28.22 27.71 27.24 26.66
25293.75 25294.75 25295.75 25296.75 25297.75 25298.75 25299.75 25300.75 25301.75	-2.61 -1.82 -2.40 -1.86 -2.37 -2.09 -2.35 -1.82 -2.11 -2.07 -1.99 -2.23	143.2 142.1 140.7 139.6 138.3 136.9 135.6 134.3 133.2 132.0 130.9 129.5	10033. 9793. 9553. 9317. 9083. 8850. 8620. 8393. 8167. 7943.	34.44 33.77 33.25 32.63 31.98 31.37 30.79 30.27 29.72 29.22 28.60	405. 1147. 538. 1166. 868. 1234. 634. 1016. 989. 925.	.015 .042 .019 .043 .032 .044 .023 .036 .035	2.75 2.98 3.15 3.30 3.61 3.86 4.06 4.25 4.47	138.2 136.8 135.8 134.5 133.1 131.9 130.6 129.5 128.3	8913 8692 8473 8256 8041 7828 7617 7408	31.49 31.00 30.43 29.82 29.25 28.71 28.22 27.71 27.24 26.66

		MARK III	1101521	DISTANCE	1420 TIR	ES/WFT	HUNWAY/	NO FLAPS	1	
TEST NO. 4	5C	MARK III	ANTIBAL	DY 31 MM				uri	WIND	DIREC
			5.	CSS AL		TEMP	ONLA		210.0	DEG MAG
STAND WGT	1	TEST WOT	1.000		HG 2	2.0 C	4.0	KTS	2100	
34000.L55	14	470%.Las	2.0				4.7	CTA	NUARD D	AY
		- 1	TES	T DAY-				KTAS	DIST	KE
		4.0.000	DIST	KE	FAR	HHB.	FHH	147.4	10050.	32.72
TOD	ACCEL		11420.	37.34	005.	.031	.04		9825.	31.94
27312.55	-2.54	155.9	11176.	36.48	1585.	.071	• 30	145.7	9594.	31.36
27313.50	-3.32	154.1	10918.	35.83	595.	. 437	.59		9364.	30.62
27314.50	-2.47	152.7	10562.	35.00	923.	.046	.44	142.6	9137.	30.07
27315.50	-2.72	150.9	10408.	34.34	533.	.650	.47	141.3	8911.	29.31
27316.50	-2.44	149.6	10400.	33.54	1115.	.079	1.19	139.5	8688.	28.53
27317.50	-3.56	147.6	10157.	32.07	379.	.025	1.36	137.7	the second second second	27.93
27318.50	-2.69	145.8	9909.	32.00	485.	.024	1.43	136.2	8469.	27.44
27319.50	-2.22	144.3	9565.	31.45	1244.	.053	1.64	135.0	8252.	26.81
27320.50	-2.72	143.1	+422.	30.75	652.	.028	1.86	133.5	B037.	26.23
27321.50	-2.15	141.5	9182.		1816.	.077	2.16	132.0	7824.	25.61
27322.50	-3.18		A943.	30.10	1525.	.055	2.52	130.4	7614.	24.95
27323.50	-2.87	137.4	A709.	29.41	1388.	.056	2.85	128.8	7406.	
27324.50	-2.68		4477.	28.6H	390.		3.07	127.5	7202.	23.90
27325.50	-2.20		4247.	28.14	1682.	.070	3.38	156.0	6999.	
27326.50	-2.90	133.8	4020 ·	27.01	39%	Land Control	3.69	124.4	-6799	E CANADA
27327.50	-2.12	132.1	7796.	20.62	1477.	324779458	3.91	123.3	6602.	
27328.50	-2.64	131.1	7574.	25.35	2109.	THE R. LEWIS CO., LANSING	4.37	121.4	6405	100000000000000000000000000000000000000
27329.50	-3.17		7354.	25.57	1231.		4.69	119.9	6515.	
.27330.50	-2.34		7137.	24.97			5.02	118.4	6021	
27331.50	-2.6		2953.	24.38	1644.		5.25	117.2	5834	
27332.50			9712.	23.40		1.75.00	5.57	115.7	5648	
27333.50			02055	23.31	1890.	574 300	5.91	114.2		
27334.50			- 024h.	22.73			-	112.9	5283	
27334.50			6691.	35.53	1739.	4.70	4 10 6	111.3	5104	
27335.50			5590.	21.63			200	110.3		. 18.32
27336.50			5701.	21.26	754	· · · ·				
27337.45	-1.0									

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TEST NO. 46A MARK III ANTISKID/STANDARD TIRES/WET RUNWAY/HALF FLAPS

STAND WG	7	TEST WG	r P	RESS AL	T	TEMP	WIND	VEI.		DIREC
43000 LBS	•	3200 LB		.578 IN	HG : I	17.8 C	3.0	KTS	550.0	DFG MAG
					5.3		a = 18		VIII. VIII.	
			TE	ST DAY					ANDARD D	
TOD	ACCEL	GND-SPD	DIST	KE -	FBR 🖘	URR	EBR	KTAS	DIST	KF
23226.05	-2.85	158.6	11221.	48.08	1567.	.054	• 08	153.4	10478.	44.77
23227.00	-3.62	156.4	10968.	46.80	2704.	.088	76	151.3	10237.	43.55
23228.00	-2.59	154.8	10706.	45.80	1372.	.045	1.22	149.6	9988.	42.61
23229.00	-3.01	153.1	10446.	44.80	1990.	.064	1.68	147.9	9742.	41.45
23230.00	-2.75	151.3	10189.	43.78	1569.	.055	2.15	146.2	9498.	40.69
23231.00	-2.88	149.8	9935.	42.89	1546.	.060	~ 2.52	144.7	9258.	39.95
23232.00	-3.09	147.8	9684.	41.75	1859.	.073	3.00	142.7	9019.	38.77
23233.00	-2.87	146.2	9436.	40.86	2011.	.062	3.47	141.2	8785.	37.93
23234.00	-3.00	144.4	9191.	39.85	2240.	.069	4.01	139.4	H557.	36.47
23235.00	-2.82	142.7	8949.	38.92	2064.	.061	4.50	137.7	8323.	36.09
23236.00	-2.84	140.8	8709.	37.93	2123.	.064	5.03	135.9	8096.	35.15
23237.00	-2.74	139.5	8473.	37.20	2030.	.061	5.46	134.5	7873.	34.46
23238.00	-3.05	137.6	8239.	36.22	2493.	.075	6.02	132.7	7652	33.53
23239.00	-2.76	135.9	8008.	35.33	2149.	.064	6.54	131.0	7433.	32.60
23240.00	-3.12	134.3	7780.	34.48	2679.	.079	7.09	129.4	7219.	31.88
23241.00	-3.32	132.4	7555.	33.55	2997.	<b>~088</b>	7.72	127.6	7005.	31.00
23242.00	-2.31	130.4	7334.	32.54	1684.	.050	8.25	125.6	6796 •	30.05
23243.00	-2.92	129.3	7114.	31.96	2544.	074	8.66	124.5	6589.	29.50
23244.00	-2.65	127.5	6898.	31.08	2223.	.064	9.20	122.7	6385.	28.67
23245.00	-3.02	125.8	-6684.	30.27	2760.	.080	9.73	121.1	6183.	27.90
23246.00	-2.79	124.1	6473.	29.44	2505.	.071	10.29	119.4	5985.	27.12
23247.00	-3.00	122.4	6265.	28.64	2821.	080	10.84	117.7	5789.	.26.37
23248.00	-2.69	120.6	6060.	27.79	2454.	.069	11.40	115.9	5596.	25.57
23249.00	-2.62	118.9	5858.	27.05	2392.	.068	11.89	114.3	5405.	24.87
23250.00	-2.86	117.4	5658.	26.36	2746.	.078	12.40	112.8	5219.	24.22
23251.00	-2.42	115.7	5461.	25.62	2204.	.061	12.89	111.1	5033.	23.52
23251.70	-1.21	114.9	5325.	25.23	598.	.017	13.04	110.3	4905.	23.15

TEST NO. 468 MARK III ANTISKID/STANDARD TIRES/WET RUNWAY/HALF FLAPS

TEST NO. 46B	WARK 111	MINITONION.	31207						
		PRE	SS ALT	1	TEMP		VEL .	MIND	DIRFC
STAND WGT	TEST WGT			19	9.4 C	•4	KTS	225.0	DEG MAG
38000.LBS	38375.LBS	21.00	00 114 110				4		
		TEST	DAV					ANDARD D	AY
		(E)	KE F	BR :	UBP	EBR	KTAS	DIST	KF
	L GND-SPD		I k has	652	.061	.07	152.2	10634.	38.95
25699.10 -3.2				599.	.060	.48	150.5	10411.	-38.10
25700.00 -3.1				146.	.078	1.00	148.5	10165.	37.10
25701.00 -3.5		10,000		889.	.033	1.33	146.8"	9923•	36.27
25702.00 -2.4				640.	.061	1.65	145.3	9684•	35.53
25703.00 -3.0				688	.061	2.05	143.7	9447.	34.72
25704.00 -3.0			-	772.	.063	2.51	141.7	9213.	33.79
25705.00 -3.0				388	.050	2.84	140.3	8983.	- 33 · 1.0 ·
25706.002.6				452	.050	3.22	138.5	8754.	32.27
25707.00 -2.6				981.	.071	3.64	136.9	8528	31.52
25708.00 -3.1		, , , , ,		450.	.051	4.04	135.2	8306.	30.75
25709.00 -2.6	2 138.3		L V		.061	4.44	133.5	8085.	29.98
25710.00 -2.8	12 136.5	050.4	A	728.	.062	4.84	131.9	7868 •	29.28
25711.00 -2.8	3 134.9			794.	.047	5.21	130.3	7653.	28.56
25712.00 -2.4		-		411.	.057	5.54	128.9	7440 .	27.95
25713.00 -2.6	8 131.8			706.		6.00	127.3	7231.	27.27
25714.00 -3.1				249	.077	6.28	125.7	7024.	26.59
25715.00 -1.		1 76. 4 4 -	8.10	635.	.021	6.68	124.2	6818.	25.96
25716.00 -3.3				638.	.087	7.14	122.5	6616.	25.25
25717.00 -2.5				756.	.059	7.45	121.2	6417.	24.70
25718.00 -2.3		6779. 2		447.	.04A	7.78	119.9	6550	24.16
25719.00 -2.5				1743.	•057		118.3	6025	23.54
		6366.		1639.	•055	8.14	116.9	5832	55.09
25720.00 -2.0 25721.00 -2.0				1557.	.050	8.46	115.5	5641	22.43
42,44,4		5962.		1892.	•061	8.82	114.1	5454	21.90
				1536.	.050	9.15	112.7	5268	21.36
2012000				2006.	.066	9.51	111.3	5103.	20.83
25724.00 -2.		5394	22.03	1735.	.057	9.77	11143	21030	1

MARK III ANTISKID/STANDARD TIRES/WET RUNWAY/HALF FLAPS TEST NO. 46C WIND DIREC WIND VEL TEMP PRESS ALT STAND WGT TEST WGT 250.0 DEG MAG •4 KTS 27.580 IN KG 22.5 C 34700.LBS 34000.LBS ----STANDARD DAY---------TEST DAY-----... .KF ... -DIST-KE - FBR ----UBR -- EBR -KTAS ACCEL GND-SPD DIST TOD .07 29.65 8222. 32.30 140.4 1849. .077 8953. 145.0 27551.35 -3.438021 ... 28.91 *067 138.6 .51 8734. 31.49 1679. -3:21 143.2 27552.25 7800. 28.16 30.68 .91 136.B 1842. .074 8494. 27553.25 141.3 -3.32 1.35 7582. 27.29 .059 134.7 1495. 8257. 29.74 139.1 -2,94 27554.25 26.75 7367. 1.72 133.3 2261. .093 B023. 29.15 27555.25 -3.63 137.8 130.7 2.34 7155. 25.69 .086 28.00 2184. 7794. 27556.25 -3.48 135.0 2.64 6946. 25.17 129.3 .052 1323. 7566. 27.43 -2.65 133.6 27557.25 6740. 24.52 127.6 26.73 .072 3.01 1841. -3.09 131.9 7343. 27558.25 3.41 6537. 23.81 125.8 25.95 1673. .065 7122. 130.0 27559.25 -2.89 23.19 6336. 1986. 3.80 124.1 .075 25.28 6904. -3.13128.3 27560.25 6139. 22.52 4.20 122.3 24.55 .062 6689. 1652. 27561.25 -2.78 126.4 21.94 5943. .078 4.59 120.7 23.91 2096. 6476. -3.15 124.8 27562.25 119.1 4.97 5751. -21.33 1778. .066 6268. 23.26 123.1 27563.25 -2.82 20.67 ..095 5561. 5.43 117.2 2507. 6061. 22.54 -3.46 121.1 27564.25 5375. 20.02 .075 5.89 115.3 5858. 2007. 21.83 27565.25 -2.95 119.2 .095 19.43 6.33 113.6 5191. 2491. 5659. 21.19 -3.37 117.4 27566.25 5011. 18.76 .070 20:46 6.77 111.6 1908. -2.77 5462. 27567.25 115.4 7.21 110.0 4832. 18.20 19.85 2759. **.**105 113.7 5268. 27568.25 -3.54 17.62 4657. 108.2 .082 7.66 19.23 2246. -3.01 5078. 27569.25 111.9 106.4 4485. 17.05 8.10 .095 4891. 2582. 18.60 27570.25 -3.29 110.0 16.45 104.5 4316. 2555. .094 8.56 17.95 4707. -3.23 108.1 27571.25 4150. 15.82 9.09 102.5 4526. 17.26 3114. .112 106.0 27572.25 -3.7115.30 .058 9.48 100.B 3987. 1667. 27573.25 4349. 16.70 -2.32 104.3 99.4 9.84 3826. 14.89 2675. 4174. 16.25 .096 102.8 27574.25 -3.24 14.23 15.53 10.40 97.2 3668. 3497. .124 -3.96 100.6 4002. 2757.5 • 25 3514. 13.63 95.2 10.89 2609. .093 3834. 14.88 98.4 27576.25 -3.1013.17 3362. 93.6 2901. .103 11.32 -3.34 96.8 3669. 14.38 27577.25 91.7 3214. 12.65 2374. .084 11.74 13.81 3509. 27578.25 -2.82 94.8 .104 89.8 3068. 12.15 12.16 3350. 13.27 2894. 92.9 -3.27 27579.25 11.68 88.1 2926. .090 12.58 2582. 3195. 12.76 27580.25 -2.94 91.1 86.4 2786. 11.25 12.95 12.29 2416. .087 3042. 89.4 -2.77 27581.25 10.86 84.9 2648. 13.26 1866. .067 87.9 2892. 11.87 -2.23 27582.25 10.80 84.7 2622. 11.80 1477. .053 13.26 2863. 27582.45 -1.8787.6

TEST NO. 47A	MARI	C III A	MTISKIO	JBFG TI	RES/DRY	RUNWAY			
STAND VGT	TEST WGT	р	RESS A	LT	TEMP	MIND	VEL	WIND	DIREC
43000 LBS	42400.LBS	27	.567 IN	HG	20.0 C	3.7	KTS	253.0	DEG MAG
+500074455									
· · · · · · · · · · · · · · · · · · ·		TE	ST DAY-				ST	ANDARD [	DAY
TOD ACCEL	GND-SPD	DIST	kΕ	FBR	UBR	EBR	KTAS	DIST	KE
23091.29 -4.76		3388.		288.	.012	02	155.5	3731.	46.05
23092.25 -8.84		3530.	45.94	6051.	.246	•95	151.9	3481.	
23093.25 -10.32		3371.	42.46	8689.	.308	3.03	145.9	3228.	40.52
23094.25 -10.52		3123.	39.07	9427.	•324	5.27	139.8	2985.	37.22
23095.25 -10.62		2885.	35.73	9952.	.340	7.58	133.6	. 2752	33.97
23096.25 -10.20		2557.	32.56	9754.	*335	9.80	127:4	2530.	30.88
23097.25 -10.19		2440.	29.68	10111.	.334	11.94	121.5	2317.	28.08
23098.25 -9.60		2233.	26.95	9657.	.317	13.96	115.6	2116.	25.43
23099.25 -9.63		2035.	24.49	9989.	•326	15.87	110.0	1923.	23.05
23100.25 -9.58	108.4	1847.	22.07	10213.	•333	17.77	104.3	~ 1741 •	20.71
23101.25 -9.55		1669.	19.85	10394.		19.58	98.8	1568.	18.56
23102.25 -9.72	97.0	1506.	17.05	10923.	• 353	21.38	92.9	1405.	16.45
23103.25 -9.17	7	1341.	15.65	10436.	.340	23.04	87.3	1251.	14.52
23104.25 -9.19		1191.	13.95	10674.	.341	24.57	82.3	1106.	12.89
23105.25 -9.69		1050.	12.16	11547.	366	26.14	76.6	971.	11.17
23106.25 -8.92	74.9	920.	10.52	10729.	.341	27.58	71.0	845.	9.60
23107:25 -8:77		797.	~9.11	10703.	343	28.85	65.9	- 728 ·	
23108.25 -8.15	64.7	684.	7.85	10048.	315	30.00	60.9	621.	7.06
23109.25 -8.68	59.7	579.	6.69	10885.	342-	31.09	56.0		
23110.25 -8.79	54.6	483.	5.59	11167.	•352	32.13	50, 9	430.	4.93
23111.25 -8.57	49.2	395.	4.53	11010.	.346	33.09	45.5	348.	3.95
23112.25 -8.39		316.	3.69	10085.	.337	33.92	40.8	274.	
23113.25 -7.76	-39.3	245.	2.90	10150.	.318	34.66	35.8	209.	2.44.
23113.94 -5.09		202.	2.50	6688.	.208	34.89	33.0	170.	2.07

EST NO. 4	6A	HAM	K 11 48	HISKIDA	STANDARD	11.Car				01050
TAND UCT		TEST VET	P	A C Sec. Mr.	the t	TEMP	WIND	VEL	238.0	DIREC DEG MAG
TAND HGT		43025.645		.446 I	1 HG 2	1.5 0	4.6	KTS	230.0	100 1914 1991
+3000.L3S						200		ST	ANDARD I	DAY
-			TF	ST DAY		000	EBR	KTAS	DIST	KE
TOD	ACCEL	GNU-SPD .	DIST		FHR	0.560	0.00	154.4	10627.	45.41
23202.44	-4.08	161.8	11522.	49.84		0.000	0.00	152.6	10421.	44.32
23203.25	-3.84		11462.	48.00		0.000	0.00	150.4	10168.	43.04
23204.25	-3.75		11134+	47.31		0.000	0.00	148.3	9921 .	41.89
23205.25	-3.39		10570.			0.000	-02	146.1	9675.	40.65
23206.25	-4.24		10504.	44.75	295.		.06	143.8	9434 .	39.34
23207.25	-3.85	10 mm 1 mm	10353.		0.	0.000	.00	141.5	9197 .	38.13
23208.25	-3.29		10100.				.06	139.€	8964.	
23209.25	-3.48	146.8	9550.		0.	.010	.10	137.7	8733.	36.08
23210.25	-3.76		95114.		4 7 75	.019	15.	135.4	8506°	34.91
23211.25	-3.80		9362.				.24	133.3	8282.	
23212.25	-3.00		9124.	37.44			.24	131.8	8063.	33.08
23213.25	-3.17	10.00	8585°	36.63	0.		.28	129.7	7846.	32.04
23214.25	-3.22		8550.				.32	128.0	7633.	
23215.25	-3.48		8427 .				.45	125.9	7422	30.17
23216.25	-3.2	A Marie Contract	#505.				.46	124.2	7215	29.34
23217.25	-2.6	2 2 2 2 2	7974.				.49	122.4	7010.	
23218.25	-2.9	- N 100 M	7760.			.007	.50	120.9	6810	
23219.25	-2.5	0.46.74	7543.	30.49			.50	119.5		
	-2.6		7329.	36.25				117.8	6416	
23220.25	-3.0		7116	29.49			.61	116.0		
23221.25	-3.1		0909	25.59			.95	114.2	6032	
23222.25	-2.5		0704		311.		7	113.9		
23223.25	-2.2		6545	27.0	0.	0.000	.95	113.7	2,,0	

TEST NO. 4	88	MAR	K II AN	TISKID/S	STANDAR	O TIRES	/WET RUN	WAY		100
STANO WGT		TEST WGT	. 0	FESS AL	T	TEMP	WIND	VEL	MIND	DIREC
38000 L95		39300.LB5		.453 IN	HG	23.0 C	6.5	KTS	225.0	DEG MAG
	121		20		The same				ANDARD D	NAV
			the second second second second	ST DAY-			Cub	KTAS	DIST	KE
TOD	ACCEL		0151	KE	FBR	URR	EBR	145.1	9091.	35.43
25699.00	-3.97	155.6	10466.	41.05	- P	0.000	0.00		8854.	34.29
25700.00	-4.11	153.2	10509.	39.79	0.		0.00	142.8	And the second second	33.21
25701.00	-4.30	150.9	4949.		150.		.01	140.5	8620.	31.96
25702.00	-4.25		9596.	37.19			.15	137.8	8389.	17 7 7 10 0
25703.00	-3.61		9448.	36.06	1000000	0.000	.13	135.6	8163.	30.95
25704.00	-3.88	143.7	9204.	35.01	203.		-14	133.5	7942.	30.00
25705.00	-3.99	141.3	8963.	33.85	473.		.25	131.2	7723.	28.96
25705.00	-3.46	139.0	3727.	32.77		0.000	.30	129.0	7508	27.99
25707.00	-3.61	137.1	H494.	31.86	590.		.33	127.1	7298 •	27.18
5708.00	-3.51	134.8	8265.	30.82	290.	.012	.42	124.9	7090.	26.24
5709.00	-3.70	134.7	8639.	29.85	664.	.027	.53	122.8	6886.	25.38
5710.00	-3.33	130.6	7516.	28.90	368.	.014-	.65	120.8	6685.	24.53
5711.00	-2.70	128.9	7596.	28.16	0.	0.000	.66	119.1	6490 .	23.87
	-3.72		7381.	27.39	1028.	.040	.77	117.4	6297	23.18
5713.00	-2.90	124.9		- 26.44	182.	.007	. 92	115.2	6105.	22.33
5714.00	-2.95	123.3	6959.	25.7H	336.		:04	113.7	5918.	21.75
25715.00	-3.29	121.4	6753.	25.00	875.	.033	1.09	111.9	5734.	21.05
5716.00	-2.96	119.5	6550.	24.21	586.	.022	1.25	110.0	5552.	-20.35
25717.00	-2.56		6350.	73.59	166.		1.29	108.5	5375.	19.80
25718.00	-2.95		6152.	22.92	763.		1.41	106.8	5199.	19.20
25719.00	-2.79	114.6	5957.	22.28	655.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.53	105.3	5027.	18.64
25720.00	-2.89		5765.	21.60	870.		1.70	103.5	- 4856 -	18.03
25720.75	-2.36		5623.	21.15	310.		3.77	102.4	4731.	17.63

TEST NO.	48C	MAR	K II ao	115810/	STANDAR	O TIMES	WET HUN	нАУ		
STAND 46	T	TEST WGT	i i	HESS &	LT	TEND	WIND	VEL	WIND	DIREC -
34000.LBS		34550.Las	5.1	.450 IN	rir;	25.5 C	8.5	KTS	225.0	DEG MAG
			TF	ST DAY-				ST	ANDARD I	DAY
TOD	ACCEL		0157	KE	FAR	HHR	EBR	KTAS	DIST	KE
27733.29	-4.30	147.3	9325.	33.1A	-89.	.004	.00	134.0	7662.	27.02
27734.25	-4.10		9088.	32.03	21.	.001	.06	131.5	7452.	26.02
27735.25	-3.75		H946.	31.10	0.	0.000	.06	129.4	7241.	25.22
27736.25	-3.94		8508.	30.04	180.	.009	.09	127.1	7032.	24.31
27737.25	-4.18	7.33.57	8373.	29.06	565.	.027	.17	124.9	6826.	23.47
27738.25	-3.66		6142.	28.04	188.	.009	.27	122.5	6624.	22.59
27739.25	-3.29		7915.	27.24	0.	0.000	.27	120.6	6428 .	21.90
27740.25	-3.62		7592.	26.41	384.	.017	. 32	118.6	6234.	21.19
27741.25	-3.54		7472.	25.56	405.	.019	.41	116.6	6043.	20.46
27742.25	-3.10	PR. PT	7256.	24.77	72.	.003	.46	114.6	5856 .	19.78
27743.25	-3.62		7042.	24.03	742.	.033	.54	112.8	5672.	19.15
27744.25	-3.26		6833.	23.19	495.	.021	.70	110.7	5490 .	18.43
27745.25	-3.08		6520.	22.55	406.	.01p	.77	109.0	5314.	17.89
27746.25	-3.12		6423.	21.81	577.	.024	.91	107.1	5139.	17.26
27747.25	-3.09		6223.	21.15	656.	.027	1.02	105.4	4968.	16.71
27748.25	-2.94	115.8	5026.	20.50	578.	.024	1.16	103.6	4800.	16.14
27749.25	-3.04	114.1	5932.	19.90	794.	.033	1.29	101.9	4635.	15.64
27750.25	-2.65	112.4	5541.	19.31	455	.019	1.41	100.3	4473.	15.13
27751.25	-3.00	110.7	5453.	18.75	905.	.038	1.54	98.7	4314.	14.66
27752.25	-3.24	168.6	5267.	18.04	1325.	.050	1.79	96.6	4155.	14.05
27753.25	-2.77	107.0	5085.	17.52	880.	.035	1.95	95.1	4002.	13.62
27754.25	-2.99		4905.	16.96	+142.	-048	-2.15	93.4	3851.	-13.14
27755.25	-2.31	103.7	4730.	16.45	538.	.021	2.28	91.9	3703.	12.72
27756.25	-2.69	162.5	4555.	16.06	1010.	.039	2.39	90.7	3560.	12.39
27757.25	-2.88	100.6	4384.	15.48	1296.	.050	2.63	88.9	3415.	11.90
27758.25	-2.31	99.3	4415.	15.09	745.	.029	2.76	87.7	3277.	11.57
27759.25	-2.06	97.8	4650.	14.62	536.	150.	2.88	86.2	3139.	11.18
27759.44	-1.97	97.0	4014.	14.56	457.	.017	2.88	86.0	3114.	11.13

TEST NO. 4	49A	MARK	II a	TTS <iu< th=""><th>/STANDAH</th><th>TIRES</th><th>WET KUN</th><th>WAY</th><th>3</th><th></th></iu<>	/STANDAH	TIRES	WET KUN	WAY	3	
STAND #GT		TEST WGT		oarss.	AL T	TEAP	MIND	VEL	WIND	DIREC
43000 LBS		43200 . LSS		7.615 1		15.0 C		NTS	270.0	DEG MAG
43000.003		-24.00		-						
31114			T	ST Oak				ST	ANDARD I	
T00	ACCEL	6ND-5PD	DIST	R.F.	FAR	UEP	ERR	KTAS	DIST	KE
23313.12	-5.14		4973.	30.08	0.	0.000	0.00	141.6	8777.	38.16
23314.00	-4.97		4763.	37.54	0.	0.000	0.00	139.1	8571.	36.81
23315.00	-3.85		4529.	35.14	0.	0.000	0.00	136.3	8342.	35.35
23316.00	-3.15	The state of the s	4509°	35.22	n.	0.000	0.00	134.5	8117.	34.45
23317.00	-3.67		H071.	34.09	584.	.050	- 14	132.3	7894.	33.34
23319.00	-3.44		7447.	33.07	410.	4	15.	130.4	7676	32.35
23319.00	-3.50		7527.	31.96	549.	.022	. 36	1.821	7460.	31.26
23320.00	-3.47		7411.	30.40	714.	.024	.52	156.5	7248 .	30.32
23321.00	-2.69		7194.	30.11		0.000	- 55	124.4	7041.	29.45
23322.00	-3.41		h947.	29.14	357.	650.	•68	122.4	6834 .	28.52
23323.00	-3.08		6781.	24.20	559.	.615	. 45	120.4	6632.	27.60
23324.00	-2.94		4577.	27.50	475.	.015	.43	118.9	6433.	26-89
23325.00	-3.05		4374.	26.63	729.	.1153	1.08	117.0	6237.	26.05
23326.00	-3.36		5178.	25.77	1263.	.041	1.29	115.1	6043.	25.20
23327.00	-2.87		saha.	24.9	795.	.025	1.45	113.3	5853.	24.43
23328.00	-2.68		5793.	24.20	547.	050	1.63	111.5	5666.	23.67
23329.00	-2.71		5504.	23.60		.025	1.75	110.1	5481 .	23.09
23330.00	-2.73		541d.	22.67	933.	.022	1.94	108.4	5299.	22.37
23331.00	-3.20		5235.			.051	2.17	106.A	5120.	21.70
23332.00	-2.43		5055.	21.3			5.41	104.8	4944.	50.60
23333.00	-2.88		4377.	20.75			2.57	103.4	4771.	20.33
23334.00	-1.90		4703.	20.1		.606	2.81	101.8	4600.	19.73
23335.00	-3.02	101.7	4530.	19.78			2.44	100.8	4431.	19.35
	-3.07		4361	18.95			3.32	98.7	4265.	18.54
23336.00	-2.25		4194.	15.4			3.50	97.2	4102.	18.00
23337.00	-3.01		4030.				3.79	95.6	3941.	17.38
23338.00	-2.34		3864.	17.0			4.00	94.2	3784.	16.90
23339.00			3710.				4.25	92.6	3628.	16.31
23340.00	-2.34		3557.				4.25	92.2	3587.	16.20
23340.21	1 . 50									

STAND WG		TEST WGT 38700.LBS		RESS A		TEMP 19.5 C	WIND 0.0	VEL KTS	0.0EE	DEG MA
	_ '		TF	ST: DAY-				STA	NDARD D	AY
	ARCEL	GND-SPD		KE	FBR	OBR	EBR	KTAS	DIST	KE
TOD			7745.	31.40		0.000	0.00	132.3	7260.	29.44
25451.57	-3.61	133.2	7534	30.70	620		.08	130.2	7062	28.50
25452.50	-4.13		7311.	29.34	0.	0.000	.15	127.9	6853.	27.50
25453.50	-3.49		7092	25.46	742.	010	-18-	125.9	6648	
25454.50	-3.61		1.00	27-51	487.	.020	.26	123.8	6446.	
25455.50	-3.67	4 41 77 4 1		26.52	487. 378.	015	. 36		6247.	24.86
25456.50	-3.46	4.64	5455.	25 74	892	.036	.47	119.8	6051.	24.13
25457.50	-3.80		6251.	24 95	892.	013	59	117.7	5860.	23.30
25458.50	-3.20			23.92	904.	0.35	.75	115.4	5670.	22.42
25459.50	-3.57		6049.	23.23				113:8 -		21 .77.
25460.50	-3.13	THE STATE OF THE S	5851.		1007.	.039	1.01	11177	5302.	21.00
25461.50	-3.47		5657.	22.41	1228		1.22		5123	-20.29
25462.50	-3.55		5465.	21.64		.023	1.40	107.7	4947.	19.52
25463.50	-2.95		5277.	20.82	605	~ "•02.5 ~ "•046		106.4		19.03
25464.50	-3,37		5092.	20.31	-1206.		1.75	104.3	4603.	18.29
25465.50	-3.04		4911.	19.51	931.	035	1.94	102.5		17.68
25466.50	-3.29		4732.		1325	.050		100.7		17.06
25467.50	-2.44		4557.	18.20	403.		2.08	99.1	6-1-NO	16.51
25468.50	-4.11	101.4		17.62	2501.			96.8	3951.	15.76
25469.50	-2.81	99.1	4215.	16.81	1068.	.039	2.65			
25470.50	-3.23	97.5	4049.	16.28	1642		2.84	95.2		15.26
25471.50	-2.71		3886.	15.66		.041	3.07	93.4	3643.	14.68
25472.50	-3.31		3726.	15.10	1919	······• (r = 9 ~		91.7		14.15
25473.50	-2.80		3569.	14.54	1396.	1050	3.56	90.0	3345	13.63
25474.50	-3.15		3415.	14.01	1871.	.070	3.79	.88.3		13.13
25475.50	-3.20		3264.	13.46	2047 -	.072	4.09	86.6	3059.	12.62
25476.50	-2.88			12.90	1733.	.062	4.36	84.8		12.09
25410.50	-2.67		2971.	12.46	1545.	.055	4.58	83.3	2785.	11.68
25477.50	-3.10		2829.				4.88	81.3		11-11
25478.50	-2:88		2589.	11.45	1945.		5.12	79.9	2520.	
25479.50				10.93	2373		-5,43	78.0	2393.	
25480.50			2419.	10.44	2875		5.76	76.3	2268.	9.78
25481.50	-3.52	The state of the s		9.91		–	··· 6 - 05 ···		- 2146.	
25482.50	-2.3		2230.	9.80	707		6.08	73.9	2090.	9.19
25482.97	-1.64	75.6	2530.	2.00				- 1		

1531 1100 170						
STAND WGT 34000.LBS	TEST WGT	PRESS ALT 27.625 IN HG	TEMP 20.2 C	W1N0 1.1	VEL KTS	WIND DIREC 255.0 DEG MAG
TOD ACCEL 27309.85 -4.90	GND-SPD 138.9 136.2	7510. 28.67 18	UGR 00030 1010	EBR •02 •14 •14	134.1 131.5 129.2	6918. 26.04

TEST NO. 49C

MARK 11 ANTISKID/STANDARU TIRES/WET RUNWAY

34000.655	٠,-	+400 100		•						
- 18 ALF INCOME TO 1	. ,		Tr	ST DAY				STA	O GHADINA	AY
				KE	FBR	UBR	EBR	KTAS	DIST	KE
TOD		SND-SPD	DIST	29.80	490.	.030	50.	134.1	7110.	27.07
27309.85	-4.90	138.9	7819.	~28.67	181.	010	.14	131.5	6918.	26.04
27310.75	-4.39	136.2	7510.	27.69		0.000	.14	129.2	6710.	25.14
27311.75	-3.53	133.9	7383.	.54.95		-0.000-	14	127.2	6504.	24.35
27312.75	-3.84	131.8	7158	25.92	79.	.004	.15	125.0	6303.	23.52
27313.75	-3.87	129.5	593å•	\$2.00	721.	038	1.5.	122.8	6104.	22.68
27314.75	-4.34	127.2	6721 •	23.97	57.	.003	.35	120.2	5910.	21.73
27315;75	-3.53	124.5	6509.	-		- 023	• 38	118.3	5719.	21-07
27316.75	-3.84	122.6	6300.	23.24	0.	0.000	.44	116.1	5532.	20.30
.27317:75	-3.07	120.4	6096•	22.39	1534 •-	.025	.49	114.2	5347.	19.63
27318.75	-3.64	118.4	539 <b>→•</b>	21.66	614.	.029	.61	112.2	5166.	18.94
27319.75	-3.61	116.3	5596	20.91		.028	.76	109.9	4988.	18-19
27320.75	-3.43	114.0	5501.	20.08	135.	.006	.78	108.5	4814.	17.73
27321.75	-2.91	112.6	5310.	19.58			1.04	-106.0	4642.	16-92
27322.75	-4.07	110.0	5122.	18.69	1638•	.021	1.19	104.3	4474.	16.37
27323.75	-2.52	108.2	4934.	18.09	504. 774.	.033	1.29	102.8	4309.	15.89
27324.75	-3.10	106.6	4757	17.57		• 033 • 054.	1.55	100.5	4146.	15.19
27325.75	-3.67	104.3	4579.	16.80	1546.		1.70	98.7	3987.	14.65
27326.75	-2.58	102.4	4404.	16.21	454		1.74	97.5	3831.	14.31
27327.75	-2.81	101.2	4233.	15.84	766.	.031	2.19	94.9	3676.	13.54
27328.75	-4.87	98.5	4063.	14.99	3213.	.124	2.42	93.0	3526.	13.01
27329.75	-2.32	96.6	3900.	14.41	535	.021	2.55	91.4	3379.	12.58
27330.75	-2.53	95.0	3738.	13.94	**************************************	.033	2.73	90.0	3234.	12.19
27331.75	-3.12	93.5	3578.	13.51	1545.	.060	-	87.8	3092.	
27332.75	-3.53	91.3	3422.	12.87	2095	.079	3.29	86.1	2953.	11.17
27333.75	-2.83	84.5	3270.	12.38	1407.	.054		84.1	2816.	10.64
27334.75	-3-98	87.4	3150.	11.80	2733.	105	3.64	62.4	2683.	10.21
27335.75	-2.62	85.7	2974.	11.34	1342.	.051		80.7	2553.	9.80
27336.75	-3.00	84-0	2631.	10.89	-1822.	÷069	4.13	79.2	2426.	9.45
27337.75	-2.55	82.4	2591.	10.50	1394.	.053	4.33		2300.	9.03
27338.75	-3.00	80.6	2553.	10.04	1951.	.075	4.58	77.4	2178.	8.67
27339.75	-2.69	79.0	2416.	9.64	1663.	.053	4.81	74.3	2059.	- 8.31
27340.75	-3.10	77.4	2287.	9.25	5195	085	5.07		1941.	7.87
27341.75	-2.87	75.3	2158.	8.76	2019.	.075	5.30	.72.3	1827.	7.58
27342.75	-2.47	73.9	2031.	8.44	1616		5.57	71.0	1715.	7.28
27343.75	-2.66	72.5	1908.	8.11	1888.	•070	5.79	69.5	1660.	7.11
27344.25	-2.54	71.6	1847.	7.92	17⊌3∓	.067	5.84	68.7	1000+	

TAND WGT		TEST WGT		PRESS	ALT		TEMP		KTS.	197.0	DEG MAG
3000.LBS		+3500.L69		27.541	IN	10 6	1.0		1777	Same Same	
				TEST DA	Y					ANDARD I	DAY
T00		GNU-SPD	DIST	KE	100 10	FBR	UBR	EBH	KTAS	DIST	KE KE
3294.89	-3.43	153.8	10591	45.5	Si	0.	0.000	0.00	148.2	9837.	41.80
3295.75	-4.07	152.0	10469			44.	.002	•00.	146.4	9630	
3296.75	-3.75	149.3	10215		5	0.	0.000	.06	143.9	9392.	39.41
3297.75	-3.66	147.3	9965		19		0.000	-06	141.9	9158.	
3298.75	-3.51	145.1	9716.	. 40.5	Ó		0.000	.06	139.8	8928.	37.19
3299.75	-3.80	143.1	9475	. 39.4	12		.011	.08	137.8	8702	36.12
3300.75	-3.72	140.8	4235	. 38.1	.7	349.	.013	.17	135.5	8478.	
23301.75	-3.31	138.6	8999	. 37.0	00		0.000	.55		8258	The PAST 200
3302.75	-3.62	130.8	5767	. 36.0	15		.017	.25	131.6	8042.	
3303.75	-3.17		8538	. 34.			- 005	35	129.4	7829	
3304.75	-3.40		8312		36	459.	.016	.41	127.5	7618.	30.97
3305.75	-3.17		8690	. 32.	75	292.	.010	.46	125.8	7412.	CONTRACTOR OF THE
3306.75	-3.31	128.8	7571	. 31.5	75	617.	.021	.59	123.8	7208.	
3307.75	-2.77		7556	. 31.	15.		0.000	.60	122.2	7008.	
3308.75	-3.53		7442	. 30.	18	1124.	.037	.80	150.1	6809.	
3309.75	-2.60	The second second	7233	. 29.	25	100	0.000	.87	118.4		
3310.75	-3.24		7026	. 28.	57	960.	.031	.95	117.0	6423.	
23311.75	-3.00		6522			745.	.024	1.18	114.9		The second secon
23312.75	-3.23		6522	. 26.	33	1181.	.038	1.33	113.5	6048.	
23313.75	-1.59		6425	. 26.			0.000		111.8	5866.	
23314.75	-3.56		6250		35	1876.	.059	1.64	110.1	5683.	
23315.75	-1.47		6036		84		0.000	1.72	109.0		22.60
23316.75	-4.02		5946	. 24.	19	2719.	.082	2.01	107.3	5330.	
23317.75	-2.02		5559	. 23.	20 -	120:			105.2	5157.	
23318.75	-2.46		5474		71	767.	.023	2.32	104.1	4986.	
23319.75	-2.74		5293		12	1218.	•037			4819.	20.08
23320.75	-2.83		5114	. 21.	31	1437.		2.79	100.8	4653.	19.34
23321.29	-2.48		5018			1007.	.030	2.84	100.1	4564	19.07
SULTIE!			1.0	200							10.75
										7	Section 1
									11 118		
									11 (20)		
											1975

TEST NO. 508		MARH	TIMATI	TSKIDYS	TANUARU	IRES/	WEI KON			4 4
		TEST WGT		PESS	-	TEMP	WIND	VEL	WIND	DIREC DEG MAG
STAND WGT		TEST WET	27	545 IN	HG 2	3.2 C	3.6	KTS	222.0	DEG MAG
38000.LBS	3	8700.L35	L 1 .	The section of the se	a last new of the property and the	with the same constitution.	and the second	STA	NDAPD I	AV
- co at an indian			TES	ST DAY-				KTAS	DIST	KE-
		GND-SPD	DIST	KE	FBR	UBR	EBR	133.3	7934.	29.89
		141.1	9016.	34.10	0.	0.000	0.00		7741.	28.92-
	-4.04		8903.	33.02	- 0.	0.000	.00	131.1	7530 .	28.04
25527.25	-3.84	138.8	8570.	32.04	0.	0.000	.00	129.1	7323.	27.07
	-3.80	136.8	8342.	30.96	0.	0.000	.00	126.9	7120.	26.22
25529:25	-3.51	134.4	8116.	30.02	73.	.004	.01	124.9		25.34
25530.25	-3.71	132.4	200=	29.04	77.	.004	.03	122.7	6919.	24.55
25531.25	-3.58	130.2	7895.	28.15		0.000	.03	120.8	6723.	
25532.25	-3.27	128.2	7577.	27.27	0.	0.000	.03	118.8	6529 •	23.15
25533.25	-3.21	159.5	7462.	26.52	0.	0.000	.03	117.1	6339.	23.08
25534.25	-3.16	124.4	7250.	25.70	- 628.	02A	10	115.3		- 22.35
25535.25	-3.62	122.5	7042.		0.	0.000	.16	113.2	5967.	The Land of the Artist
25536.25	-2.71	120.4	6537.	24.83	68.	.003	.16	111.9	5787	
25537.25	-2.96	119.0	6535.	24.28	431.	.019	.25	110.0	5607 •	
25538.25	-3.12	117.0	6430.	23.47	489.		.30	108.4	5432.	
25539.25	-3.08	115.4	6240.	55.83			.43	106.4	5259	19.06
25540.25	-2.94		6047.	25.05	463.				5089	- 18.53
25541.25	-2.59		5857.	21.43	482.		.62	103.4	4921.	17.98
	-2.76		5569.	20.81	782.	.027	-76	-102:0-	4757	-17:49
25542.25	-2.76		-5484	20.27	864.			100.3	4595	
25543.25	-3.09		5303.	19.62	1335.		.97	98.6	4435	and the second second
25544.25	-3.07		5124.	19.00	147		1.10	97.5	4279	
25545.25	-2.02	104.1	4947.	18.58	1184.	.040	1.20	05-7-	-4123	15.40
25546.25	-6.00	102.3	4773.	17:92	1032	.035	-1.43	94.5	3972	15.02
25547.25	-2.63		4501.	17.49	938	032	1.56	94.5		
25548.25	-2.49	the second secon	4432	1000	1468		-1.81	92.7	3674	
	-2.85		4266.	16.39	1046	. 036	1.99	91.4	3674	1-3-56
25550.25	-2.45	97.8	4102.	15.88		039		89.8"	3306	13.10
25551-25	-2.47		3941.	15.34		051	2.42	88.3	3386	-12.70
25552:25	-2.71		37910	14.89	1227			86.9		
25553-25	-2.41	93.2		14.34	1878	002	2.89	85.2	3108	11 75
25554.25	-2.88		3627.	13.84			3.13	83.7-	2913	11.43
25555.25	-2.20		3474.			048	3.32	82.4	2841	
25556.25	-2.4		3323.			056	-3.56		2710	-11.0
25557.25	-2.5	9 87.1	3175 -			The same and		79.4	2582	. 10.6
25558 - 25	-2.6	0 85.5	3029.	12.53	1699			78.0	2456	10.24
25559.25	-2.4		2985.		1084			76.9	2352	. 9.94
25560.10	-1.9	4 82.9	2766.	11.77	1004					* 1

TEST NO. 5	0 C	HAR					/HET RUN	k.		
STAND WET		TEST WGT	··· p	RESS A	LT	TEMP:	WEND	-AET	····MIND··	DIREC
34000 LBS		34700. LBS	27	.545 IN	HG 2	6.5 C	4.4	KTS	220.0	DEG MAC
								CT	ANDARD T	AV
				ST DAY-					DIST	KE
TOD	ACCEL	GND-SPD	DIST	KE	FBR		EBR		7338.	25.75
	-3.88		8563.	30.19		0.000			7140	
27276.75	-4.07	137.9	<b>6339</b> •	29.23			0.00	126.3	6935	24.02
27277:75	-4.08	135.6	8109.	28,23	148.	.008	.02	124.0	6734	
	-3.72		7882 .	27.25		0.000	.03		6537	
27279.75	-3.75	" 131.0	7659		107.	.005			6343.	21.62
27280.75	-3.70	128.8	7440.	25.49	177.	.009	0.7		6152.	20.85
27.281.75	-3.54	126.6	7224.	24.61.	161.	.008	• 11	117.7		
27282.75	-3.34	124.6	7012.			603.		115.8	5781.	
27283.75	-3.47		6804.	23.14	318 👓		. 15	114.0	5600.	18.81
	-3.51	120.5	6598	22.29	514.		. 27	111.8	5422	
27285.75	-3.21	118.6	6396 •		284.	.013	33			
27286.75	-3.11	116.7	6198 .	20.92	293.	.013		108.2.	5248	
27287.75	-3.22		6003.	20.27	5500	024	18 147 c.		5077• 4907•	
	-3:17		5811.	19.48	<b>590</b> €		*63			15.94
27289.75	-2.73		5622.	19.81	195.		• 65		4743.	15.39
27290.75	-2.92		5436.	18.38	-510.		.75	101.1.	4581.	
27291.75	-3-08		5252.	17.82	7.61			99.5	4420.	14.37
27292.75	-3.25	105.8	5072.	17.21	1052.		1.03	97.7		
27293.75	-2.84		4895 .	16.62		.031	1.17	96.0	4109.	13.86
27294.75			4721 .	16.11	241.			94.4	3957	13042
27295.75	-2.59		4550 .	15.76	552.		1.29	93.3	3810.	13.11
27296.75	-2.74		4381 .	15.11	945.		1.49	91.3	3662	
27297.75			4214 .	14.69	1027:	042	1.62		3518.	
27298.75	-2.9		4050 .	14.14	. 1391 •	.054	1.84	88.2	3376.	
27299.75	-2.75	_	3890 .	13.71	1182.	.048	2.02	86 . 8	3238.	
27300.75		92.8		13.23	837			85.2		10:92
27301.75	-2.8	91.5	3576.		1384.		2.35	83.9	2968.	
27302.75	-2.2	-	3423 .	12.35	835.	•033	2.55	82.1	2836.	
27303.75	-2-4			- 12:09	1163.	.046	2 000	81.2	2708	
27304.75	-2.8	- 4-4-1	3124.	11.59	1613.	.063		79.4	2580.	
27305.75	-2.2		2979.	11.23	980.			78.1	2456.	
27305.75			2836.	10.87	1480 .	:058		76.8		
27300.75	-2.4	_	2696.	10.48	1323.		3 • 45	75.3	.2215	
27308.75	-2.8	_	2557.	10.03	1915.			73.6	2096.	8,15
27309.70	-1.2		2429	9.74	139.		3.80	72.5	1988	7.90
26309.10	-102	T 130'O	4				, , ,			. ,

TEST NO.	51A		I ANTIS						=1.	
STANO-HG	Tarana in a	TEST - HG1	:  -	RESS A	at and a	TEMP	- WIND	VEL	CHIM	DIREC
43000 LBS		43200. LBS	27	.513 IN	HG 1	19.0 C	6.1	KTS	. S30 • U	DEG MAG
:			TE	ST DAY-					ANDARD (	
TOD	ACCEL	GND-SPD	DIST	KE	FBR		EBR	KTAS	DIST	KE
23262.33	-4.78	160.1	11635 .	49.02		0.000	0.00	151.4	10413.	43.62
3263.25	-5.12	157: 2	11389: "	-47.27	0 -	-0.000	0.00		10179	42.00
23264.25	-4.79	154.4	11126:	45.58	Ü •	0.000	0.00		9930.	40.44
		454 5	10868.	43.91	G.	0.000	0.00	142.9	9686	38.90
23265.25 2 <b>3</b> 266.25	3:42	-148-9	10614	~42,42	O 🖟	0.000	0.00	140.4	9447	37:53
23267.25	-3.32	147.5	10364.	41.50	- U +	0.000	U + U U	73002	25100	3001
23268.25	-3.54	145.0	10117.	40.19	0.	0.000	: a U 5	136.5	8986	35.47
3269.25	-4:03	443.0	9874	39.13	811	030	.11	134.5		~34.49
23270.25	-3.30		9635.	37.85	0.	0.000	. 24	132.5	8537.	3,3.31
23274.25	-3-06	139.0	9399.		0.	0.300	. 24	130.7	8319.	32.50
23272:25	3:57	136-9	9166	-35.84	627	0.22	.36		8102	31.47
23273.25	-3.09		8937 .	34.85	-82.	-013	• 40	120.1		30.56
23274.25	-3.17			33.82	330.	.012	• 48	124.7	7680	
23275.25			8487	32.96	340	-C12	•53	123-1	7475	
23276.25	-2.92		8267 •	32.05	214.	.007	59	121.3	7272	
23277.25	-2.77		8050.	31.22	119.	.004	.62	119.6	7073.	
	3-34		7836.		1016	. 034	*76		6875	26.44
	-2.54	- 4	7625 .	29.52	24.	.001	. 85			25.68
		122.6	7416	28.74	803.	.026	. 95	114.5	5491.	24.96
23281.25			7211	27.92	825	.026	-1.12	112.8	6302	24.21
23282.25	-2.99		7008.	27.16	1105.		1.31	111.2		
23283.25	-2.86		5809.	26.35	1060.	.032	1.54	109.4	5933.	
23284-25				25.68	199.		1 65		5755.	
23285.25	-2.57		6418	25.16	833.		1.73	106 . 8	5579.	
23286.25	-2.78		6225	24.29	1234.		2.01	104.8	5403.	20.91
23287.25		11114	-6036.	23.74	689.		2.14	1.03.5	5232.	-20-41
23288.25	-3.19		5849	23.04	1928.		2.43	101.9	5062.	
23289.25	-2.64		5666	22.27	1287.		2.73	100.1	4894.	19,07
	-2.62			21.67	1351.		2:96	98:7	4730%	
23290 25	-1.91	- 1	5307	21.12	452.	_		97.3	4570.	
23291.25	-3.10		5130	20.53	2118.		3.36	95.9	4411.	17.49
23292.25			4957		1030.		7.63	~ 94.2	4254.	16.88
23293.25	=2 6-25		4786	19.38	1367		3.82	93.0	4101.	
23294.25	-2.43		4617.	18.85	1279.		100	.91.6	3950.	15.98
23295.25	-2.38		4451 .	18.28	2075.		4.33	90.1		
mou potati		-	4288 •	17.57	1669.		4.67			
23297.25	-2.5!			17.33	601.		4.73	87.6		
23297.83	-1.68	8 95.2	4194.	T. + 2.2	001	4011				

TE	ST NO. 5	18 .	MARK II	ANTIS	KID/STA	NOARO T	IRES (WOR	N) / WET	RUNMAY		4 2 1 1 1 1 1 1
				1. 1	4 49 - 4	14- 3	TEMP	MIND		HIND	DIREC
-51	AND WGT		TEST WGT			LT .	23.0 C	HIND	KTS	205.0	DEG MAG
38	000.EBS	3	8350.LBS	27	. 515 IN	MG (	23.0 0	* .			A . Land
			000000000	7.5	CT DAY-				STA	NDARD D	AY
				DICE	KE -	# FBR -	UBR	EBR	KTAS	DIST	KE
			GND-SPO	9570	36.93	. 0.	3.000	0.00	143.3	8950.	34.52
	463.18	-4.01	147.5.	9367	35.89		0.000	0.00	141.2	8759.	33.54
	464.00	-4.10	145.4		34.81	0.	0.700	0.00	139.1	8531.	32.53
	465.00	-3.57	143.2	9124. 8884.	33.81	B •	0.000	0.00	137.1	8306.	31.60
	466.00	-3.73	141.1:	8648	32.59		.010	.05	134.5	8085.	30.45
	467.00	-4.07	138.5 136.5	8416.	31.63		0.300	.05	132.5	7867.	29.55
	468.00	-3.59	134.1	8187	30.55	474.	.050	.11	130.3	7653.	28.54
	469.00	-4.03		7963.	29.52	187.		.18	128.0		27.58
	470.00	-3.67	131.9	7742.	28.67	1.04	.384	.19	126.2	7235.	25.78
	471.00	-3.48	129.9. 127.7	7525	27.69	142.	.006	.24	124.0	7031.	25.87
	472.00	-3.41	125.7	7311	26.84			.28	122.1	6831.	25.07
	,,	-3.39		7100.	25.99	321	.013	. 34	120.1	6633.	
	5474.00	-3.33	121.8	5893	25.19	654.	.026	.43	118.2	6439.	23.52
	475.00	-3.50	11977	6689	24.33	489.	.020	. 55	116.2	6248.	22.72
	-	-3.28		6489.	23.61	383.		.61	114.5	6061.	
	5477.00	-3.09	117.9 115.8	6291 •	22.77	1164.		. 81	112.4		21.25
	5478.00	-3.64		6097	22.17	43.		. 86	110.9	5694.	20.69
		-2.63		5906	21.32	1530 .		1.08	108.8	5515.	19.90
	5480.00	-3.75	_		20.62	320.	.012	1.22	107.0	5339.	19,24
	5481.00	-2.65		5534	20.10	428		1.27	105.6	5166.	18.75
	5482.00	-2.69		5352.	19.42	1005.	A 100 C	1.43	103.8	4995.	18.12
	5483.00	-3.08 -2.06		5173.	18.81	957		1.59	102.1		17.55
	5484.00	-2.96		4996	18.17	785.	2 14 14	1.75	100.4		16.95
	5485.00	-2.74 -3.07		4823	17.61	1255.		1.93	98.8	4501.	16.42
	5486.00	-2.69		4653	17.01	887.		2.10	97.1	4341.	15.86
	5487.00	-3.94			16.40				95.3		
-	5488.00	-2.59		4321.	15.88	929	.035	2.49	93.8	4030.	14.81
_	5489.00 5489.00	-2.87		4159.	15.37	1369		2.68	92.3	3879.	
_	5490.00	-2.18	_	4000	14.85	610	.022	2.83			
-	5491.00 5492.00	-3.22		3843.	14.37	1915	.069	3.04	89.2	3583.	
	5493.00	-2.78		3689.	13.83	1485	.053	3.30	87.5	3439.	
-	5494.00	-2.67	_	3538 .	13:33	1.425	.051	3.51	85.9	3298.	
	5495.00	-3.07		3390.	12.84	1960		3.76	84.3	3160.	A TOTAL CONTRACTOR
	5496.00	-2.90		3245.	12.31	1841		4.05	82.6	3024.	
	5497.00	-2.56		3103.	11.82	1507	.054	4.29	80.9	2891.	
	5498.00	-2.92		2963.	11.44	1994	.070	4.51	79.6		A
	5499.00	-2.73		2826.	10.86			7.00	77.5	2632.	
	5500.00	-2.74		-2692.	10.53	1904		3 . 0 3	76.3	2507.	
***	5501.00	-3.16		2561 .	10.02			5.35	74.5	2364.	
_	5502.00	-3.16		2433.	9.53	2568		5.67	72.6	2264.	
_	5503.00	-2.23		2308.	9.14	1511		5.91	71.1	2148.	120000000000000000000000000000000000000
_	5504.00	-2.95		2185.	8.81	2424		6.14	69.8	2033.	
_	5505.00	-3.21		2065 .	8.33			6.48	67.8	1921	The second second
9	5506.00			1949.	7.92			6.74	100. 5	1812	100
	5516.27	-1.83		1922.	7.84	1239	.043	6.73	65.8	7100	
						- ,					

,									
TEST NO. 510	MARK II	ANTIS	KID/STA	NDARD T	IRES (WO	RID /WET-	RUNWAY		
STAND WGT	TEST WGT	Р	RESS A	! T	TEMP	- WIND	VEL	MIND	DIREC
	34475.LBS		.515 IN		25.8 C		KTS		DEG MAG
* * * * * * * * * * * * * * * * * * *	4 1=								
		TE	ST DAY-					ANDARD (	) AY
TOD ACCEL	GND-SPD	DIST	KΞ	FBR	tine.	EBR	KTAS	DIST	KF
27583.80 -3.56	145.5	9983.	32.30		0.300	0.00	135.8	7849.	27.77
27584.75 -3.77	141.1	8855 .	30.39	Đ.	0.000	0.00	131.6	7636.	26.07
27585.75 -4.10	138.7	8618.	29.35	187.	.010	. 03	129.3	7424.	25.14
27586.75 -3.72	136.3	8387.		0.	0.300	.05	127.0	7215.	24.26
27587.75 -3.52	134,2	8158.		11.	11 - 11 12 11	• 05	124.9		23.47
27588.75 -3.33	132.1	7934.		0.	0.969	• 05	122.9	6810.	
27589.75 -4.15	129.9	7712.	25.77	806.	.037	. 14	120.8	6612.	
27590.75 -3.50	127.6	7495.	24.86	242.	.011	• 25	118.6		21.16
27591.75 -3.22	125.5	7281.	24.05	242 • 47 • 298 •	.002	•29	116.5	6226.	
27592.75 -7.34	123.8	7070 •	23.37	298.	.013		114.8		19.84
27593.75 =3.28	121.8	6863.		007		<b>38</b>	112.9	5855.	
27594.75 -3.21	119.9	6660.	21.95 21.25	385.	.01,7	. 45 . 52	111.1	5674.	
27595.75 -3.04	118.0	6459	21.25	319.	•014	•52	109.2	5496.	
27596.75 3.39		6261.		797.	* 0.2 P.	. pp.	107.3		17.34
27597.75 -3.18	114.0	6067.	19.84	693.		.80	105.4	5147.	
27598.75 -3.11	112.3	5876.	19.23	726.		• 92	103.7	4979.	16.19
27599.75 -3.15	110.4	5688			.036		101.9	4812.	
27600.75 -2.94	138.6	5533.	18.01	720.		1.21	100.2		
27601.75 -2.92	107.0	5321.	17.47	788•		1.34	98.6	4489.	
27602.75 -2.71	105.2	5142.	16.89	661 a			96.9	4332	
27603.75 -2.78	103.7	4965	16.40	0.20		1.60	95.4	4177.	
27604.75 -3.03	101.9	4792						4025	
27605.75 =2.78 27606.75 =2.85	100.2 98.4	4621 •	15.31 14.78	960. 1131.			92.0	3875. 3728.	12.74 12.27
27607.75 -2.67	95.8	4289.	14.29		•046 •041	2.33	88.7	3584.	
27608.75 -2.64		4127	13.82	1060.		2.50	87.2	3443.	
27609.75 = 3.02	93.5	3967	13.35	1535.		2.71	85.6	3304.	11.03
27610.75 -2.75	91.9	3811.		1310.		2.92	84. D	3168.	10.63
27611.75 -2.41	90*3	3657.		- 1008.			82.5	3034.	10.24
27612.75 -3.08	88.8	3506	12.04	1787.		3.31	81.0	2903.	9.89
27613.75 -2.77	87.1	3358	11.58	1522.				2775.	9.48
27614.75 -2.71	85.3	3213.	11.19	1545.		3.56 3.80	77.6	2648	9.07
27615.75 -2.63	83.9	3070.	10.74	1509.		3.99	76.3	2526.	8.76
27616.75 -3.70	81.8	2931	10.21	2745.		4.34	74.2	2403.	8.30
27617.75 -2.62	79.9		9.75	1642.		4.61	72.4		7.90
27618.75 -2.80	78.4	2660 .	9.37	1895.		4 . 85	70.9	2170.	7.57
27619.75 -3.09	75.8		8.99	2280.		5.12	69.4	2058.	7.25
27620.75 -3.07	74.8	2401.	8.53	2320.	.090	5.42	67.4	1947.	6.84
27621.75 -2.34	73.1	2276.	8.16	1601.	.061	5.66	65.9	1840.	6.53
27622.75 -2.72	72.0	2154.	7.91	2036.	.089	5.85	64.8	1738.	6.31
27623.75 -3.31	69.9	2034.	7.45	2736.	108	6.13	62.7	1634.	5 • 92
27624.75 -3.10	68.1	1918.	7.08	2581.	.099	6.47	61.0	1535.	5.60
27625.75 -3.15	66.1	1804.	6.67	2680.	.106	6.78	59.1	1438.	5.26
27626.75 -2.86	64.4	1694.	6.33	2431.	.094	7.05	57.4	1345.	4:96
27627.75 -2.83	62.8	1587.	6.02	2451.	.194	7.30	55.9	1255.	4.70
27628.75 -3.79	60.7	1482.	5.62	3536.	.137	7.64	53.8	1165.	4.36
27629.75 -2.51	58.9	1382.	5.30	2172.	.094	7.90	52.1	1061.	4.09
27630.75 -2.93	57.2	1284.	4.98	2714.	.104	8.16	50.4	999.	3 • 82
27631.10 -2.28	56.5	1253.	4.88	2036.	.078	8.18	49.8	971.	3.74

TEST NO. 52A	MARK III ANTI	SKID/STAN	DARD TI	IRES (WOR	N)/WEI	YUMMAY		
	TOT NOT	PRESS AL	т	TEMP	WIND	VEL	WIND	DIREC
O 171.100		7.483 IN		9.8 C	4.9	KTS	235.0	DEG MAG
43000.LBS	43200.603	1 4 405 211	,,,,					
	T	FST DAY				STA		ΑΥ
TOD ACCEL	GND-SPD DIST	KE	FBR	UBR	EBR	KTAS	DIST	KF
TOD ACCEL 22947.28 -4.02	160.3 10093.			0.000	0.00	152.6	9136.	44.30
	158.3 9833.		0.	0.000	0.00	150.5	8894	43.12
22948.25 <b>-3.67</b> 22949.25 <b>-4.18</b>			0.	0.000	0.00	148.1	8646	41.74
22950.25 -3.29			0.	0.000	0-00	146.1	8403.	40.62
22951.25 -4.02	151.5 9048.		80.	.003	. 0,1	143.9	8163.	39.43
22952.25 -3.64			` D.	0.000	.02		7927.	38.19
22953.25 -3.22			0.	0.000	.02	139.6	7695	37.11
22954.25 -3.65			97.	•004	.02	137.7	7467.	36.11
22955.25 -3.55			114.		.08	135.5	7241.	34.97
22956.25 -3.18	141.1 7815.		0.	0.000	• 08	133.7	7019.	34.03
22957.25 -3.82			782.		-20	131.6	6800.	32.94
22958.25 -2.62			0.	0.000	•22	129.7	6585	32.03
22959.25 -3.67			785.	.028	• 29	128.0	6373.	31.19
22960.25 -2.83			0.	0.000	.40	125.8	6164.	30.14
22961.25 -3.68	131.6 6666.		1082.	.037	.48	124.4	5959.	29.47
22962.25 -3.65			1183.	.040	.81	121.9	5755.	28.30
22963.25 -3.21			766.	•026	97	120.1	5556.	27.44
22964.25 -3.66			1569.	.051	1.24	118.1	5359	26.55
22965.25 -2.94			755.	.024	1.48	116.1	5167.	25.65
22966.25 -3.16			1175.	.037	1.68	114.3	4977.	24.89
22967.25 -3.08			1166.	.036	1.91	112.5	4791.	24.09
22968.25 -3.51			1890.	• 058	5.55	110.7	4608	23.32
22969.25 -3.69			2242.	•069	2.64	108.6	4427.	72.44
22970.25 -2.69			1017.	.031	2.94	106.6	4250.	21.62
22971.25 -3.70			2484.	.074	3.29	104.9	4076.	20.43
22972.25 -2.76		22.96	1331.	•039	3.66	102.8	3906.	20.10
22973.25 -3.51			2418.	.071	3.97	101.2	3739.	19.51
22974.25 -3.53			2558.		4.47	98.9	3573	18.63
22975.25 -3.77			2970.		4.95	96.9	3412.	17.87
22976.25 -2.98			2008.		5.36	94.9	3254.	
22977.25 -3.71			3068.		5.80	93.0	3100.	16.48
22978.25 -2.28			1226.		6.14	91.2	2950.	15.85
22978.53 -2.15			1082.	.032	6.14	90.9	2908	15.74
25210422 -5472								

					DAGD II	BECTUNE	NIZWET I	RUNWÁÝ		
TEST NO. 5	5 <b>2</b> B	MARK II	ANTISK	TDZSTAN		A. A.			MTNID' (	DIREC
STAND WG		TEST. WGT		ESS AL	,	TEMP	WIND 4.2		250.0 [	OFG HAG
38000.LBS	38	350.LBS	27.	485 IN	HG Z	107 (/	, • •			
	10		TF9	ST DAY-				STA		KF KF
700		SND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	31.58
T00 25132.23	-2.80	144.6	8267.	35.50	. 0.	0.000	0.00	137.0	7388 <b>.</b> 7217 •	30.95
25133.00	-3.61	143.2	8080.	34.81		0.000	0.00	135.6 133.2	6996	29.86
25134.00	-4.04	140.7	7840.	33.62	559.	.022	•14 •15	131.3	6780	50 US
25135.00	-3.18	138.8	7605.	32.70		.000	.16	129.4	6568	28.16
25136.00	-3.55	136.8	7372.	31.76	112. 345.	.014	.25	127.1	6357.	27.18
25137.00	-3.65	134.4	7143.	30.69 29.90	0. J47.	0.000	.25	125.4	6152.	26.46
25138.00	-2.83	132.7	6918. 6695.	29.02	372.	.015	.30	123.5	5949	
25139.00	-3.46	130.7	6477	28.20		0.000	.32	121.7	5749	24.01
25140.00	-2.73	128.9	6260.	27.43	651.	.025	•37	4 0		24.21
25141.00	÷3.50	127.1 124.9	6048.	26.47	963.	.037	•58	117.8	5358	23.33
25142.00	-3.66	122.8	5839.	25.61	534.	.020	.73	115.8		22.54
25143.00	-3.20 -2.96	121.1	5633.	24.89	358.	.014	:81	114.1	4980	21.89
25144.00	-3.49	119.1	5430.	24.10	1112.	.042	.98	112.2	4796.	21.17
25145.00	-3.69	117.0	5231.	23.23	1,475.	.055	1.26	110.1	4436.	19.63
25146.00 25147.00	-2.92	114.9	5035.	22.41	689	.025	1.47	108.0	4262	19.12
25148.00	-3.13	113.4	4842.	21.84	991.	.037	1.60	106.6	4090	18.40
25149.00	-3.65	111.4	4553.	21.05	1734.	.065	1.89	104.6 102.3	3921.	17.59
25150.00	-3,51	109.0	4467.	20.16	1692	.062	2.25	100.5	3756.	16.98
25151.00	-2.94	107.2	4285.	19.49	1092.	.040	2.47	98.2	3593.	16.23
25152.00	-3.79	104.8	4106.	18.66	2226.	.083 .055	3.11	96.6	3435.	15.69
25153.00	-3.12	103.2	3931.	18.07	1517.	.062	3.43	94.5	3279.	15.01
25154.00	-3.19	101.0	3758.	17.31	1718. 2620.	.093	3.78	92.7	3127.	14.45
25155.00	-3.87	99.2	3589.	16.69 15.93	1876.	.067	4.17	90.4	2977.	13.76
25156.00	-3.17	96.9	3424 • 3262 •	15.31	2798	.101	4.53	88.6	2831.	13.80
25157.00	-3.87	95.0 92.4	3104.	14.48	3128.		5.04	86.0	2688	12.45
25158.00	-4.03 -3.07	90.3	2950	13.85	2082.	.073	5.41	84.1	2549.	11.99
25159.00	-3.07 -3.11	88.4	2799.	13.27	2218.	.077	5.75	82.2	2414.	11.36
25160.00 25161.00	-3.52	86.7	2651.	12.76	2756.		6.10	80.5	2282*	10.90
25162.00	-3.84	84.2	2507.	12.04	3251.		6.57	78.1	2152	9.71
25163.00	-3.89	82.1	2366.	11.43	3394.		7.02	76.0	2026. 1904.	9.19
25164.00	-3.52	79.9	2229.	10.85	3027		7.45	73.9 71.8	1785	8.46
25165.00	-4.24	77.7	2096.	10.26	3951.		7.91 8.41	69.1	1669.	8.14
25166.00	-3.69	75.0	1967.	9.56	3400.		8.85	66.9	1531.	7.94
25167.25	-3.72	72.8	1811.	9.00	3518.		9,31	64.7	1424.	7.04
25168.25	-3.95	70.5	1690.	8.44	3870 • 2967 •		-		1321.	6.59
25169.25	-3.14	68.3		7.93	3992		10.09	60.6	1221.	6.18
25170.25	-3.95	66.3	1460.	7.47 6.95	3899		10.54	58.3	1124.	5.72
25171.25		64.0	1350.	6.45	4023		10.95	56.0	1031.	5.28
25172.25		61.6	1244. 1142.	5.95	3915		11.37	53.7	941.	4.85
25173.25		59.2 57.3	1043.	5.58	4149		11.74	51.9	856.	4.53
25174.25		54.7	949.	5.09	4517		12.17	49.3	773.	4.09
25175.25		52.5	859.	4.68	3742		12.53	47.1	695•	3.74
25176.25			771.	4.29	5327	178	12.92	45.0	620 •	3.40
25177•25 25178•25			689.	3.80	5130.		13.36	42.1	548.	2.98
25179.25			612.	3.42	- 4817 ·		13.73	39.7	48]. 419.	2.36
25180.25			538•	3.08	3103		14.02	37.4	403.	2.32
25180.53			518.	3.03	2212	072	14.03	37.1	7030	

STAND KG 34000.les		TEST WGT 34550.LBS			ALT N HG	TEMP 21.4 C	WIND	VEL KTS	UNIW. 220.0	DIREC DEG MAG
			T	EST DAY				-1		
TOD .		GND-SPD		- KE		UBR		KTAS		KE
27023,25	-4.23		7297.	30.04		0.000	0.03		6421.	
27024.25	-4.30		7863.	28.89			.05	129.6		25.28
27825.25	-3.73		6833.	27.94		0.000	.09	127.4	6000	24.42
27026.25	-3.51		6637.			0.000	.03	125.1	5795.	23.56
27027.25	-3.65		6334.	26.21			.13	123.2		22.86
7028.25	-3.59			25.29			.15	121.0	5397	
27029.25	-3.5'2		5950.	24.46			.22	118.9	5203.	21.28
27030.25	-3.12	_	5738.	23.66		0.000	.25	116.3		20.56
27031.25	-3.27		5529.	23.02			.28	115.2		19.99
7032.25	-3.7.5		5324.	22.26			.39	113.3		
7033.25	-2.87		5123.	21.44	10 -	. 000	49	111.1		18.57
7034.25	-3.45		4924	20.90		.532	53	109.6		18.08
7035.25	-4.10	114.3	47.28	19.98	1543			107.1		17.26
7036.25	-3.14		4537.	19.41				105.5	3937.	16.75
7037.25	-3.73	110.2	435G.	18.56						15.99
7038.25	-3.6'6		4165	17.91			1.43	101.2	36û4.	15.40
7039.25	-3.02		3985	17.16			1.67		3442.	
7640.25	- 3.91	134.1	3807.				1.92	97.1		14.75
7041.25	-3.52	101.8	3634	15.85						14.20
7042.25	-3.57	99.7	3464.					94.9	3129. 2978.	13.57
7043.25	-3.95	97.5	3297	14.53	T ( 43 e	± 07.4		92.9		12.98
7044.25	-2.71	95.5	3135.			.096	2.85	94.7	2829.	12.38
7045.25	-3.96	93.9	2974.	13.96		. 643	3.09	88.8		11 . 87
7046.25	-4.41	91.2					3.34	87.2	2544.	11.45
7047.25	-3.43	83.8	2619. 2667.	12.73		. 125	3.80	84.7	2405	10.79
7048.25	= 3.62	86.7		11.56			4 • 1 4	82.3	2270.	10.18
7049.25	-3.95	34.5		11.00	2368	4.4	4.51		2139.	9.69
7050.25	-4.02	82.1	2374. 2233.	10.93		•113	4.83	78.1	2011.	9.19
7051.25	-272	70 0		10.31			5.31	75.8	1886.	8.64
	-3.76	79.8	2097	9.75			5.69	73.6	1767	
7052.25 7053.25	-3.52	77.7	1964.	9.24		. 104	6.04	71.5	1650.	7.69
7054.25	-3.70	75.4 73.3	1635.	8.70		-118	6.41	69.3	1536.	7.23
7055.25			1769.	8.21		• 131	6.79	67.2	1427.	6.79
7056.25	-3.81 -4.74	71.0 68.5	1588.	7.71		. 128	7.17	65.0	1320.	6.35
7057.25		65.6	1470.	7.17			7.62	62.5	1217.	5.89
	- 4. 45		1356.	6.58		. 158	8.13	59.7	1117.	5.37
7058.25	-3.89		1248.	6.14	3529 .		6.48	57.5		4.98
7059.25	-4.63			5.66			8.93		932.	4.57
	-4.34		1042.	5.15		. 163	9.33	52.4	845.	4.13
7061.25	-4.52	55.8	947.	4.77			9.73	50.2	763.	3.80
7062.25	-4.09	52.8	855.	4.26			16.13	47.2	683.	3.36
7063.25			768.	3.91			10.47	45.1	609.	3.06
7064.25	-4,58	47.7	685.	3.47			16.87	42.3	538.	2.69
7065.25	-3.73		607.	3.11		. 146	11.26	39.8	471.	2.38
7066.25	-4.86		532.	2.79			11.53	37.5	409.	2.11
7067.25	-5.31	39.7	463.	2.41		. 221	11.91	34.6	350.	1.80
7668.25	-4.89		398.	2.04			12.25	31.4	296.	1.49
7069.25	-4.34	33.8	339.	1.75			12.54	28.8	247.	1.25
7070.25	-5.42	31. 3	284.	1.50	5915.	. 228	12.82	26.4	202.	1.05
7071.25	-5.49		234.	1.16	6056.	. 558	13.12	22.7	161.	.78
7072.25	-2.68	25.3	190.	.98	3070.	.114	13.35	20.5	127.	.63
7672.76	-2.33	24.6	171.	.93	2348.	. 689	17.32	19.9	113.	.59

TEST NO.	53 A	MARK	TIT AN	NTISKID/	SOMMERS	TIRES/	IET RUNW	AY :		- 5.4
		TEST NOT		PRESS A	LT .	TEMP	WIND	VEL ST		DIREC
• , ,		TEST WGT		7.484 IN	-	16.5 C	3.9		195.0	DEG MAG
43000 L BS	3	43200.L9S	2.6	1 m 3 m 1 m	*		4			
1.			T	EST DAY-				STA	NOARD	DAY
4 2 1			DIST			UBR	ERR	KTAS	DIST	KE,
T 00		GND-SPD	7714	47.96		0.000	0.03	152.8	7172.	44.44
22977.72	- 4.26		75 07	46.71		.009	.05	150.7	6975.	43.26
22978.50	-4.45	A11701 4 W	7246	45.31		0.000	.05	148.4	6.728.	
22979.50	-3.60		6987.		1027 •		.17	145.9	6484.	
22980.50	-4.79		6734	42.32	537		.35	143.3	5244.	39.10
22981.50	- 4. 26		6485		931 •		.55	140.8	5.008.	37.72
22982.50	-4.40		6241	39.60	786		.69	138.5	5778.	36.53
229,83.50	-4.19		6000	37.93	1685		1.09	135.5	5550.	34.95
22984.50	-4.72		5765	36.68	1460.		1.39	133.2	5328.	33.77
22985.50	- 4. 4.2		5533.	35.09	1674 •		1.84	130.2	5109.	32.28
22986.50	-4.40		5367.	34.02	604	10.00	2.01	128.1	4896.	31.26
22987.50	-3.53		5083	32.79	1883	- 1 -	2.34	125.8	4685.	30.10
22988.50	-4.39		4864			. 066	2.77	123.2	4479.	28.90
22989.50		128.4	4650.		2795		3.25	120.9	4277.	27 . 81
22950.50	40 00 0	126.0	4439.	40 12 West Mann h	3173.	tobic to one and a territoria	3.94	117.9	4079.	26.45
22991.50			4234	<del>-</del> :	2100		4.44	115.4	3885.	25.34
22992.50			4832.	NAME AND ADDRESS OF TAXABLE PARTY.	3705.	4	5.01	113.2	3697.	
22993.50			3837.		2200		5.63	110.2	3:512	23.10
22994.50			3643.	1 1 1 1 1	4365		6.23	107.8	3331.	22.14
22995.50			3455		2777		6.86	105.2	3155.	21.06
22996.50			3272		3749		7.44	102.8	2983.	20.13
22997.50			3092		3136		8.05	100.1	2815.	19.06
22998,50			2917.		3411		8.56	98.3	2652.	18.38
22999.50			2746		5084	_	9.41	94.9	2491.	17.15
23000.50			2579.	-	3574		10.04	92.5	2336.	16.29
23001.50			2417		4383		10.72	89.8	2185.	15.35
23002.50			2260.				11.33	87.3	2039.	14.52
23003.50		•	2107.				12.11	84.4	1897.	13.57
23004.50							12.67	81.9	1759.	12.76
23005.50			1959		2551		12.67	81.6	1737.	12.67
23005.67	-2.3	5 86.2	1935	14.20	2221		24,0			

TEST NO. 539	MARK III ANT	ISKID/SOM	ERS TIRES/	WET RUNWA	ΥY		
	51	SERO ALT	TEMP	MIND	VEI	WIND	DIREC
		RESS ALT	19.0 C	4.2	KTS		DEG MAG
38000.LES 3820	00.LBS 27	485 IN HG	1.9.0 Å	702	N, I J		7.7
	TE	T 384			STAN	IDARD D	AY
		KE F	R UBR	EBR	KTAS	DIST	KE
TOD ACCEL GN		36.92	0.0.000	0.03	142.0	5693.	33.94
	,		373	•13	139.3	5461.	32.64
4,000,00			342016	.15	136.8	5234.	31.46
			345	.25	134.4	5011.	30.39
			250 . 011	.33	132.1	4792.	29.34
	37.6 5211. 35.2 4981.		37, 051	.53	129.7	4577.	28.29
	* · · ·		357	.85	126.8	4365.	27.06
			267 . 089	1.25	124.2	4159.	25 • 97
	29.6 4534.		715	1.72	121.2	3956.	24.71
	26.5 4318.		239	2.12	118.6	3759.	23.68
	23.9 4107.	24.80 2	963111	2.68	115.9	3566.	22.59
	21.1 3900.		861 . 138	3.29	112.6	3377.	21.33
	17.8 3699.		655061	3.68	110.2	3194.	20. 43
	15.3 3502.		412128	4.20	187.7	3015.	19.51
	12.8 3309.		504129	4.89		2840.	18.33
C 2 4.300 C	09.4 3122.		997 144	5.57	101.5	2669.	17.33
	06.4 2939.		176151	6.29	98.4	2505.	
	03.3 2762.		397119	6.95	95.3	2345.	
	00.2 2591.		282 .115	7.49	92.8	2191.	14.49
	97.6 2424.		782167	8.19	89.9	2949.	13.59
	94.6 2261.		703 166	8.95	86.6	1894.	12.61
	91.3 2155.		232 . 150		83.3	1753.	11.68
			741 164	10.26	80.9	1619.	11.01
	85.5 1806.		816 . 159		77.7	1485.	10.14
25505.00 -5.14	82.2 1655. 79.3 1529.		903. ,174		74.8	1362.	9.42
			652 203		71.5	1242.	8.62
25507.06 -5.66			210214		68.0	1126.	778
	72.3 1272. 69.3 1152.		223. 134		65.0	1016.	7.10
25509.00 -5.11			657198		62.1	912.	
25510.00 -5.39			383 185		58.9	813.	5.84
25511.00 -5.07			947 241		55.6	718.	
25512.00 -6.31			030206	-	51.9	629.	
25513.00 -5.45			761 234		48.9	546.	4.01
25514.00 -6.00	52.8 636. 49.4 550.		568 . 229		45.5	468.	
25515.0C -5.77			543 223		41.8	396.	2.95
25516.00 -5.67	45.7 470. 42.5 395.		953 238		38.7	330.	
25517.00 -5.95	38.8 .327.		951 241		35.0	269.	
25518.00 -5.90	34.9 264.		332 252	_	31.3	213.	
25519.00 -6.16	31.6 258.		102278		28.9	165.	
25520.00 -6.76	27. 1 158.		986 . 277		23.5	121.	
25521.00 -6.61	24.1 115.		381 . 147		20.7	86.	.72
25522.00 +3.53	た ユキエ エアンチ	•					

TEST NO. 530			MEOS TIE	FS/WET	RUNHA'	Y	4	
TEST NO. 530	HACK III ANTI	2KI 11/20m	MEK2 IT	(1,0)				
1531 101			TE!	4P			MIND 0	IKE U
STAND HGT TEST	WGTPRE	SS ALI	21.	0.0	€.1	KTS	220.0 0	EG MAG
34000.LES 34550	.L95 27.4	85 IN HG	, 210	, 0				
34000125			= -			STAN	DARD DA	Y-55
	TES	DAY	9R	UBR	EBR	KTAS	DIST	KE
TOD ACCEL GND-	-SPO DIST .		3 . C.	00 (	0.00	138.7	,	28.95
	4.6 6529 1	33.79	J . U.		.01	136.7	5448.	28.11
2164(*1)	6.5 6323	32.83	152	000	.23	133.7	5229.	.26 . 89
2105000	7.4 6677 ·	31.47	932 .	901	.27	131.2	5014.	25.92
2/02300	n. 9 5838.	30.38		001	2.2	128.9	4805.	.25.00
2100000	a. 5 5602 ·	29.35			34	126.5	4599.	24.10
C. LOGITA O.	c 4 5370 .	28.33	539	053	.57	1 23 . 9	4396.	23.09
5/035-01	7. L 5142				64	1 21 . 7	4199.	22.29
2/00000	4920	26.30	0. 0.	200	.74	119.5	4005.	21.50
5/404400	8.9 4700.		847	037	96	117.1	3815.	20.62
2100000	6.4 4485.		1000	046	1.19	114.7	3629.	19.80
2100000	3.9 4274.	C U # - V		055	1.47	112.2	3446.	18.94.
2100110	1.4 4067.	22.53	7	.061		109.6	3267.	18.08
21030800	8.7 3864.	21.55		087	1.84	107.2	3093.	17.31
27639.00 -4.67 11		20.68		.081	2.1	104.2	2021.	16.34
27640.0C -4.37 11		19.58		.132	2.74	101.3	2755.	15.45
C/041000		18.57	2709 .	.107	3.23	98.5	2593.	14.61
2,042		17.61			3.81	95.5	2436.	13.76
			3493 .	.135	4 4 4	92.9	2285	13.00
27644.005.09 1		15.78		.092	4.89	89.9	2135	12.18
27645.66 -4.83 1	01.6 2748. 98.5 2578.	14.84	4907 .		,	36.9		11.37
2/640=0.6		13.92	2843 .	.110		84.4	1855.	
27647.00 -4.23	J J U T	13.17	4455 .	.175	6.73	80.8	1720	9.83
27648.30 -5.50		12.15	4322 .	.178	7.44		1591.	9.18
27610.00 +5.34	V 7 4 -	11.40	3914 •	. 147	8.01	78.1	1468.	8.56
27650.00 -4.84		10.68	4234 .	. 164	8.54	75.4	1347	
27651.00 -5.10	00.4	9.83	4771 .	.134	9.24	72.1	1234	
27652.00 -5.44	30.0	9.28	3953.	.148	9.75	69.6	1123	
27653.00 -4.58	77.6 1540.	8.42	5529 .	.239	19.4	66.3	4 9 4 8 2	6.00
27654.86 -5.95	74.2 1412.	7.71	4941 .	.189	11.02	63.2	917	
27655.00 -5.31	71.0 1290.	6.98	5786	. 220	11.55	59.8	823.	
27656.00 -6.00	67.5 1172.	5.29	5148 .	.193	12.25	56.5	774.	4.32
27657.00 -5.31	64.2 1061.	5.72	5383.	.203	12.79	53.6	649.	3.60
27658.00 -5.45	61.1 956.	5.10	5239 •	.201	13.31	50.3	570	3.38
27659.00 -5.24	57.7 955.		5241	.199	13 . 81	47 • 4	495	2.97
27660.00 -5.17	54. 8 760	4.09	5488	.212	14.29	44.4		
27661.00 -5.34	51.7 670.		5610	.212	14.75	41.3	426	
27662.00 -5.38	48.5 586.		4752	. 160	15.18	38.3		
27663.00 -4.52	45.4 507.		2075	.077	15.39	36.3		
27664.00 -1.98	43.4 432.		1531	.056	15.39		293	1,90
27664.22 -1.47	43.2 416.	2.85	1931				•	
21004022								

STAND WGT	TEST WG1		PRESS	ALT				HIND	VEL	WIND	DIREC
43000.Les	43200.LBS		27.527	IN H	G	17	7.2 C	€.6	KTS	217.0	DEG MAG
		**********	FST D		- ,		,-" ;	43. 0	STA	ND ADD	, , , , , , , , , , , , , , , , , , ,
TOD ACC	EL GND-SPD		KE.						KTAS		KE
23022.68 -4:		7933.	50.9				0.000		154.5	7114.	
23023.50 -4.	37 161-1	7709	4,9.8				0.000		152.4	6.906	
23024.50 -4.		7439.		7			0.00			6656	
23025.56 -5.	78 155.1		46.	0.0	ā		000	0.00	146.4	6407	40.82
3026.50 -5.0	151.9	6915.	44.1	11			0.000	0.00	143.3	6165	39.07
3027.50 -5.5		6662.					000	0.00		5927	37.12
3028.50 -4.5	7 145.3	6414.					. 000	0.69	136.7	5697	35.59
3029.50 -3.	142.9		39.0	18	565		. 021	0 3	134.5	5473.	34.42
3030.50 -4.1	16 140.6	5932.					. 048	.33	132.2	5253.	33.26
3831.56 -4.6	1 138.0		36.4	1	1982		.071	.7.4			31.96
3032.50 -4.0	16 135.3	5466.	35.0		1471		.050	1.14	126.9	4824.	30.67
3033.50 -4.4	5 132,9				2173		.072	1.54	124-6	W616-	20.55
3034.50 -4.4	4 138.2	5017.	32.4	4	2353	•	. 077	2.06	121.9	4411.	28.30
3035.50 -4.7	1 127.6	4850.	31.1	2	3050		.096	2.65	119.3		
3036.50 -4.6	5 124.8	45 87.	29.7	7	3149		.097	3.32	116.5	4 C16.	25.85
3037.50 -4.5	122.1	4379.			31.33	Ι.	095	3.97	113.9		24.68
3038.50 -4.5	5 119.4	4175.	27.2	7	3319	- 3	. 100	4.62	111.3	3638.	23.56
3039.50 -4.1	5 116.8	3976.	26,1	0	2912		.087	5.24			22.49
3040.50 -4.4	9 114.2	3781.		4	3510	•	-104	5.88	106.1	3278.	21.44
3041.50 -4.0	8 111,7	3590.	23.8	4 3	3091		. 091		103.6	3105.	20.43
3042.50 -4.4	7 109.2	3404.	22.8		3734		.109	7.14	101.2		19.4B
3843.50 -4.3	6 106.4	3222.	21.6				. 112		98.4		18.44
3044.50 -4.3	5 104.0	3044.	20.7	0 -3	3806	•	. 113	8.47			17.58
3045.50 -4.7	8 101.1	2871,					. 133	9.24		2453	16.53
3046.50 -4.3	5 98.5	27 03.			1849	•	. 122	9.93	90.7	2302.	15.64
3047.50 -5.3	2 95.7	2538.	17.5				. 165			2153.	
3048.50 -4.9		2380.	16.3		124		. 152	11.61	84.6	2009.	13.63
3049.50 -4.1		2226.			114		.120	12.25		1.872	12.86
3050.50 -4.1	9 87.4	2076.			275		.129	12.88		1739.	12.10
3051-50 -4-7	3 84.7	1931.	13.7		119	-	. 152	13.58		1609.	11.29
3052.50 -2.9		1790.	12.9		2820	-	. 084	14.05	74.7	1485.	10.62
3052.58 -2.8	3 82.21	1779.	12.9		2663		.077	14.05		1476.	

TEST NO. 548 MARK	III ANTIS	KID/SOMME	RS TIRES/W	ET RUNWA	lΥ		3+
			TEMP 18.5 C	MITAIO	VEL	WIND	DIREC
STAND WGT TEST WGT	PRES	S ALT	TEMP	E.E.	KTS	210.0	DEG MAG
38000.LBS 38550.LBS	27.53	O IN HG	18.5 0				
·			and the second of		CTAL	IN COADS	ΛΥ
TOD ACCEL GNO-SPO	TESI	DAY	e HAR	FBR	KTAS	DIST	KE
TOD_ ACCEL GNO-SPO	DIST K	(EEÞ:	0.0.000	0.06	143.5	6048.	34.66
25161.07 -3.33 153.0	6923. 39	1.92	0 - 0 - 0 0 0	0.00	141.9	5834.	33,07
25162.00 -3.53 151.2	5554	70	0.000	0.00	4 30 . 5	5605.	32.72
25163.00 -3.36 148.8	6431. 37	* # / C	0. 0.000	0.04	138.0	5383.	32.02
25161.07 -3.33 153.0 25162.00 -3.53 151.2 25163.00 -3.36 148.8 25164.00 -3.33 147.3	6101. 01	5.60 19	54. 080	.27	135.2	5160.	30.75
25165.00 -5.39 144.4	5935. 35	. 64 . 48	30 - 1.080	.27	132.0	4941.	29.31
	5094 · 34	2.44 28		1.33	128.8	4726.	27.89
25167.00 -5.38 137.9	5457. 38	1.01 22	44	.1 . 87	125.8	4518.	26.60
25168.C0 -5.17 134.8	5228. 31	25	75 103	2.45	122.5	4314.	25.24
25169.00 -5.28 131.4		8.36 7	37. 029	2.73	120.0	4117	24.22
25170.00 -3.58 128.9	47.84. 2	7.48 13	82053	2.93	118.0	3925.	23.44
25171.80 -4.04 125.9		6.48 25	42098	3.32	115.7	3736.	22.54
25172.00 -4.86 124.6	4356. 2°	5.00 26	94	3.97	112.3	3548	21.21
25173.00 -4.77 121.0	3946. 2	4 11 21	19075	4.36	110.2	3369.	20.41
25174.00 -4.11 118.9		2.89 34	88121	5.00	167.2	3190.	
25175.C0 -5.11 115.8	3747. 2	4 87 3	56 . 107	5.58	104.5	3018.	18.38
25176.00 -4.64 113.1	32221 6	0.79 33	81118	6.18	101.9	2850-	
25177.00 -4.80 110.4			309134			2687.	16.50
25178.00 -5.93 107.5	, ,		100 .444	7 - 5 !	99.0 96.1	2527.	
25179.00 -5.08 104.5	3003. 1	7.58 31	125	8 2 2 3	93.2	2373.	14.60
25180.00 -4.66 101.5	2829. 1	6.65 4	332141	8 . 85	90.5	2223.	13.77
25181.00 -4.88 98.8			525 . 122	9.46	87 . B	2078.	
25182.00 -4.36 96.0 25183.00 -4.38 93.5			671123	10.02	93.2 90.5 87.8 85.3	1938.	
25183.00 -4.38 93.5			901 . 167	10.72	82.4 79.7	1801.	
25184.00 -5.31 90.5 25185.00 -4.34 87.8	2031. 1	3.14 3	847 136	11.34	79.7	1670.	
	1885. 1		172 176	12.03	76 • 8 74 • 0	1542.	9.93
25186.CC -5.37 84.8	1745. 1	1.46 4	265142	12.66	74.0	1420.	9.21
25187.06 -4.46 81.9			426 186	13.32	71.2	1302.	
25188.00 -5.40 79.0			306183	14.04	71.2 68.0	1168.	7.77
25188.00 -5.40 79.0 25189.00 -5.21 75.8	4757	9.04 5	189 176	14.68	65.1	1680.	7.12
25198.00 -5.03 /2.00	1232.	8.28 5	297179	15.32	62.0	976.	6.46
25191.00 -5.03 69.7		7.58 5	760 . 195	15.95	59 <b>.</b> 0	877•	5.87
25192.00 -5.35 56.7 25193.00 -5.29 63.5	1117.		785196	16.58	56.0	783	5.27
CAT 208 0 0	903.		020202	17.18	52.9	694	4.70
25194.00 -5.41 60.4 25195.00 -5.67 57.1	803.	5.56 6	413 217	17.80	49.7	610.	4.15
	903. 803. 710. 621. 538.	4.97 5	659 189	18.34	68.0 65.0 62.0 56.0 52.0 52.0 7 463.6 43.6 43.8	532	3.66
	6.21	4.42	624 224	18.88	43.6	459.	3.20
	538.	3.83 6	735 228	19.43	40.2	390.	2.72
	461.	3.29 7	159 239	19.98	36.8	327.	2.28
	461. 390.	2.78	074289	19.96 20.43	33.3	269	1.87
	349	2.57	1002 134	20.55	31.8	237.	1.70
25200.62 -3.33 38.8							

TEST NO. 5	4.G	MARK								
STAND WGT	•	TEST WGT	Р	RESS	ALT	TE MP	MIND	VEL	WIND	DIREC
6000.LBS		35050.LBS	27	.531	IN HG	21.3 C	7 * 4	KIS	225.0	DEG MAG
			TE	ST DA	Ÿ	andria di marca di Part		ST	AND ARD	
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UBR	FBR	KTAS	_DIST_	
	- 3.52	149-6	6609.	34.7	5 )	0.000	0.03	141.5	# 6114.	31.90
6896.25	-4.82	147.2	6358	33.6	1 652	c33		139.0	5872	30.80
6897.25	-3,23	144.7	6113.	32.5	0 0,	. 0.000	.10	136.6	5637.	29.73
6898.25	-4.97		5870.	31.4	3 1129	053		134.2	5404.	28.70
6899.25	-4.24	139.4	5632.	30.1	5 514	. 024	.42	131.3	5173.	27,47
	-5.39		5398.	29.0	9 1926		•63	128.8	4949	26.45
6901.25	-5.00	133.6	5170.	27.7	1 1624	078	1.14	125.6	4728	25.13
6902.25	-4.28	131.0	4947.	26.6	3 1073	048	1,39	122.9	4514	24.09
	-4.73		4728.	25.5			1.70	120.4	4304.	23.09
6904.25	-4.01	125.6	4514.	24.4	9 1665 9 1123	050	2.01	117.6	4099.	22.04
6905.25	-4.18	123.3	4303.	23.5	7 1464	061	2.28	115.2		21.16
6966.25	-4. 6	120.9	4097.	22.6	8 1890	080	2.61	112.9	3704	20.31
6907.25	11		3896.	21.4	9 2740	120	3.14	109.7		19.17
6968.25	-4.33	115.1	3699.	20.5	5 2074	087	3.57	107.1		18.28
6909.25	-4.39	112.7	3507.	19.7	2 2252	• • 095	3.93	104.8		17.49
6910.25	-4.76		3320.	18.7	0 2798	. 119	4.47	101.8	2965.	16.52
	-4.72		3136.	17.7	9 2899	120		99.1	2791.	15.66
6912.25	-4.47		2959.	16.8	9 2762	114	5.49	96.4		14.81
6913.25	-5.47		2784.	15.8	9 3996	163	6.13	93.3	2459.	
	-5.24		2616.	14.9	2 3882	. 150	6.78	90.2	2299.	12.96
6915.25	-5.08	94.7	2453.	13.9	2 3860	157	7.44	86.9	2144.	12.02
6916.25	-4.40		2296	13.2	5 3202	131	7.93	86.9 84.6 81.5	1999.	
6917.25	-4.86	89.3	2142.	12.3	7 3851	157	B.52	81.5	1855.	10.57
	-4.59		1994.	11.6	6 3659	. 146	9.05	78.9	1717.	9.91
	-4.84		1850.	10.9	3 4639	151	9.61	76.1	1585.	9.24
26920.25	-4.51	81.1	1711.	18.2	0 3774	146	10.15		1456.	8,56
26921.25	-5.36	78.2	1576.	9.4	9 4816		10.74	70 - 4	1332.	7.90
26922.25	-5.44	74.9	1447.	8.7	0 5015	195	11.33	67.1	1213.	7.18
6923.25	-4.55	71.8	1323.	7.9	9 4246	167	11.95	64.0	1.099.	
26924.25	-5.08		1204.	7.4	1 4808	. 187	12.49	61.4	992•	
6925.25	-4.8	66.6	10.90.	6.7	6 4614	1//	13.02	58.3	889.	
	-5.6	63.1	961.	6.1	8 5650		13.57	55.4		
	-5.4	59.5	0/0	5.5	C 5440		14.15	51.9	698.	4.29
6928.25	-5.3	56.6	779.	4.9	8 5411	209	14.6€	49.0	611.	
26929.25	-4.96	53.4	687.	4.4	3 5128		15.15	45.8	530.	3.34
26930.25	-5.2		599.	3.9	6 5463	202	15.60	42.9	454.	THE RESERVE
26931.25	-4.8	47.5	516.	3,5	0 5092	190	16.02	39.9	384.	2.53
26932,25	-5.3		439.	3.0	9 5719		16.44	37.0	319.	2.19
	-5.5	5 41.3	366.	2.6		227	16.87	33.8	258.	1.82
26934.25	-6.33	3 38.0	299.	2.2	4 6602	255	17.25	30.4	204.	
26935.25	-6.3		238.	1.8	6989		17.65	26.7	154.	
26936.25	-6.1		184.	1.4		259	18.0€	23.0	112.	
26937.25	-5.8	26.9	135.	11.1	2 6573		18.37	19.4	76.	
26938.25	- 4, 2	9 23.6	92.	. 8	7 4919		18.61	16.1		.42
26938.60	-3.0	22.9	79.		1 3581		18.63	15.4	39.	.38

5TAND 43000 .1	WGT .BS	TEST WST 43200.LAS		7.528		TEMP 17.0 C		KIS		DIREC DEG MAG
				EST 04	y			ST	ANDARD I	DAY
TOD	ACCEL	GND-SPD	DIST	KE	FBR	UHR	EBR	KTAS	DIST	KE
23028.	34 -3.97	155.5	7225.	40.0	7 (1.	0.000	0.00	148.3	6570 .	41.86
22969.			698a.	44.8	218.	.011	.03	145.8	6348	40.49
22970.			5732.	43.2	982.	.039	.19	143.2	6108.	39.04
22971.			6451.	41.6	5 1042.	.040	.48	140.4	5872.	37.54
22972.			6234.	40.2	7 1272.	.040	.73	138.0	5642.	36.25
22973.		142.3	5991.	38.7	1462.		1.10	135.2	5415.	34.80
22974.2			5754.	37.2	1104.	.041	1.41	132.5	5193.	33.44
22975.2			5520.	36.0	3 1777.	.064	1.72	130.2	4976.	32.29
22976.			5291.	34.4	3 2184.	.076	2.25	127.2	4762.	30.81
22977.2		131.7	5066.	33.1	5 2390.	-DH2	2.72	124.7	4553.	29.62
22978		129.0	4947.	31.8	4 1844.	.063	3.18	155.1	4349.	28.40
22979		126.7	4531.	30.7	2104.	.069	3.58	119.8	4149.	-27.34
22980.2			4419.	29.4		.081	4.10	117.3	3954.	26.18
22981.			4212.	23.2	3 2893.	.090	4.65	114.7	3761	25.04
22982.2		118.6	4009.	26.9	3471.	.107	5.36	111.8	3573.	23.81
22983.7			3911.	25.77		.089	5.97	109.3	3390.	22:73
22984.2			3518.	24.5	3106.	.096	6.55	106.9	3212.	21.74
22985.2	A STATE OF THE STA	110.8	3428.	23.4	3894.	.117	7.25	104.1	3037.	20.64
22986 .2			3243.	22.3	3399.	.101	7.89	101.6	2867.	19.65
22987.		105.6	3063.	21.3	3867.	-114	8.54	99.1	-2701.	18.68
22988.2			2987.	20.38	3849.	.113	9.20	96.6	2540.	17.75
22989.2	The state of the s		2715.	19.2		-156	9.98	93.8	-2382.	16.74
22990.2			2549.	18.05	The state of the s	.133	10.80	90.7	2229.	15.66
22991.2			2387.	17.0		.125	11:49	88.1	2082.	14.77
22992.2			2230.	16.0		.136	12.21	85.3	1938.	13.87
2993.7			2077.	-15.Ta		-141	.12.94	82.6	1799.	12.98
22994.2			1929.	14.2	5126.	.153	13.66	80.0	1665.	12.17
22995.2			1726.	13.2		.166	14.43	77.1	1536.	11.30
22996.2			1544.	12.20		.168	15.24	73.8	1409.	10.36
22997.2	The second secon		1515.	11.5		.161	15.92	71.3	1291.	9.69
22998.2			1387.	10.45		.175	16.72	67.8	1174.	8.76
22999.2			1264.	9.8		.156	17.34	65.5	1065.	8.18
23000.2			1140.	8.9	A Company of the Comp	.165	18.06	62.3	959.	7.39
23001.2			1033.	8.2		.159	18.70	59.7	859.	6.78
23052.0			947.	7.7		.100	18.98	57.6	783.	6.31

TEST NO.	554	MARK	111 4	ITISK 10	/SOMMERS	TIRES	WET PUNM	AY		
STAND +6		TEST WGT 34350.Las		PHFSS 7.530 1	ALT N HG	22.0 C	VIND 7.2	VEL KTS		DIREC DEG MAG
			T	ST DAY				ST	ANDARD I	DAY
TOD	ACCEL	GMU-SP0	DIST	KE		Unip		KTAS	DIST	KE
25105.86	-4.04	149.7	6575.	38.03		0.000	0.00	139.8	5720.	32.87
25106.75	-3.89	147.9	6352.	37.15		0.000	0.00	138.1	5521.	32.08
25107.75	-5.12	144.9	6105.	35.56		4.5	.30	135.2	5297.	30.73
25108.75	-4.90	142.0	5563.	34.24			65	132.3	5078.	29.45
25109.75	-6.02	138.7	5525.	32.66			1.24	129.1	4862.	28.03
25110.75	-4.80	135.5	5394.	31.15			1.78	125.9	4652.	26.67
25111.75	-4.06	133.0	5167.	30.04			2.02	123.5	4449.	25.67
25112.75	-3:33	130.7	4945	29:01			2.17	121.3	4251.	24.75
25113.75	-4.46	128.7	4726.	28.13	1778.	.072	2.38	119.3	4056.	23.96
25114.75	-3.82		4511.		1238:	_	2.75	116.6	3864.	-22.87
25115.75	-4.91	123.9	4300.	26.05	2670.	.102	3.11	114.6	3677.	22.10
25116.75	-3.85	120.5	4095	- 24-66				.111.4	3492.	20.86
25117.75	-5.23	115.5	3592.	23.85	3310.	.129	4.05	109.4	3313.	20.13
25118.75	-4-41		3595	72.55	2550.	.094	4-72	106.0	3136.	18.91
25119.75	-4.39	113.0	3503.	21.65	2658.	.098	5.12	104.0	2966.	18.18
25120.75	-5.12	109.9	33147	20.49	~ 3688;	136	5.78	100:9	2798.	17.14
25121.75	-4.60	167.2	3131.	19.53	13182.	.117	6.35	98.4	2636.	16.28
25122.75	÷5.05	164.3	2953.	"18.49	3945	.142	-7:00	95.6	2477.	15.36
25123.75	-4.89	101.5	2779.	17.48	3807.	.142	7.65	92.8	2324.	14.47
25124.75	-4.75	98.4	2511.	16.45	3752	- 139	8 - 30	89.8	2175.	13.57
25125.75	-4.36	.95.7	2447.	15.55	3408.	.127	8.89	87.1	2031.	12.77
25126.75	-4.55	93.2	2287.	14.76	3311.	137	9.44	**84.7	1892.	12.08
25127.75	-4.79	90.3	2133.	13.84	4190.	. 149	10.09	81.8	1756.	11.27
25128.75	-4.94	87.6	1982.	13.02	4475.	-160	10.72	79:2	1625	10.55
25129.75	-5.09	84.6	1936.	12.15	476h.	.170	11.40	76.3	1499.	9.79
25130.75	-5.02	~ 81.5	1598	11.28	4805	168	~12.07 "	73.3	1376.	9.03
25131.75	-5.21	78.3	1562.	10.40	5156.	.179	12.76	70.1	1258.	8.27
25132.75	-5.12	75.4	1432.	9.64	5145.	. :181	13.42	67.3	1146.	7.61
25133.75	-4.77	72.3	1368.	8.87	4828.	.170	14.04	64.3	1039.	6.95
25134.75	<b>∸5.</b> 05	69.6	1168*	_8.53	5242.	185	14.63	61.7	938.	6.40
25135.75	-5.39	66.3	1074.	7.47	5758.	.200	15.28	58.5	840.	5.75
25136.75	-5.18	63.1	965.	5.77	5602.	.195	15.89	55.3	747.	5.15
25137.75	<b>-</b> 5.51	60.0	360.	6.15	6085.	.506	16.49	52.3	659.	4.61
25138.75	-5.48	56.7	762.	5.46	6134.	.214	17.09	49.1	576.	4.05
25139:75	-5.08	53.7	569.	4.90	5740.	.197	17.62	46.2	499.	3.59
25140.75	-5,43	50.6	581.	4.35	6SSe	.216	18.15	43.1	427.	3.13
25141.75	-5.80	47.2	494.	3.79	6744.	• 233	18.68	39.8	359.	2.67
25142.75	-5.94	43.7	455	3.24	5987.	.241	19.21	36.4	297.	2.23
25143.75	-6.45	40.0	350.	2.72	7674	-259	19.72	32.8	239.	1.81
25144.75	-6.31	36.4	286.	2.25	7570.	•257	20.20	29.2	189.	1.44
25145.75	-6.05	32.3	528.	1.78	7324.	.249	20.63	25.3	143.	1.08
25146.75	-5.95	29.1	176.	1.44			20.98	22.2	105.	.83
25147.75	-4.44	25.4	130.	1.09	5504	.165	21.28	18.5	72.	•58
25148.00	-3.39	24·3	150.	1.04	4249.	:146	21.58	18.0	65.	54

TEST NO. SSC	MARK III 4	NTISKĮD/SO	MMERS	TIRESZW	ET RUNWA	Υ		
	CT WGT	PRESS ALT	1 -	TEMP	WIND	VEL	WIND	DIREC :
STAND WGT TE 34000.LBS 344	AA 1 7 F	7 632 IN F	117 /	Z-7 (	1 + -	17 1 3	C J L 9 7	DEG MAG
34000.LBS 344		. 14.1012			4	p co.	1	r
·	1	FST DAY				STA	NDARD D	AY
TOD ACCEL GN	D-SPD DIST	KE	F3R	URR .	EBR	KTAS		KE
77182.70 -3.40 1	45.1 6080	32.06	0.	0.000	0.00		5178.	27.09
27183.50 -3.62 1				0.000	0.00	132.9		26.59
	40.8 5544	30.21	1500.		.51		4793.	
	37.9 5409		667.	.033	•46	127.1	4583.	
	35.6 5178	28.00	1667.	* U / 5		124.9	4380.	23.49
	32.2 4952		1615.	.074	1.10	121.6	4177.	22.24
	29.9 4732	25.69	1135.	- 051	1.30	119.4	3984	21.44
27189.50 -5.15 1	26.6 4515		21877		1.77		3790	20-30-
	24.3 4304	23.54	1117.	.050	2.01	113.9	3606.	19.54
27191.50 -4.81 1	21.1 4096	22:32	2150		2.46	110.8	3421.	18:46
	18.9 3594	21.53	1471.	.062	2.75	108.7	3245	17.77
	16.3 3596	20.59	1121.	.049			3071	16.95
27194.50 -4.89 1	14.0 3500	19.81	2634.	-111		103.9	2902	16.26
	11.1 3311	18.80	2455			101.1	2736	15.34
	108.4 3125	17.88	2925.		4.38	98.4	2574.	14.57
	05.5 2945		2984.	.123	4.91	95.6	2416.	13.77
27198:50 -4.95		17 05	3267.	• 135	5.46	92.9	2264.	12.98
27199.50 -4.67	00"4" 2500	15.11 "	3097.	•15e	6.05	89.9	2115	12.10
		17. 31	3/4/13	1/4/1	44 - 64 M	7/41	17160	110-71
27201.50 -5.49	96.9 2433	. 13.38	4210.	175	7.20	84.2	1832	
27202.50 -4.62	90.7. 2116	. 12.51	.3418.	• [43	/ = / ()	UIAC	10,00	/ * * *
27203.50 -5.44	87.7 1965	11.72	4419.	•193	8.40			··· -9-23-
27204-50 -3-45	85.3 1820	. 11.07	2386.	.097	8.83	75.9	1445	8.67
27205.50 -5.62	82.5 1578	10.35	4834		9.39			7.40
27204 50 -4 08	74.3 1542	• 9.58	4251.	.170	10.00		1208	
27207.50 -5.16	76.4 1411	8.69	4559	- 180	10.57		1097.	6.81
27208.50 -5.61	72.8 1284	8.08	5154.	<b>-</b> 207			990 • 889 •	6.13 5.63
27209.50 -5.00	7071 1163							5.05
27210.50 -5.62	66.8 1048		5362.	.210	12.35	57.9	793. 701.	4.52
27211.50 -5.35	63.6 938		5176.			54.8 51.7	615.	4.02
27212.50 -5.38	60.4 533	5.56	5296.	-	13.46		534.	
27213.50 -5.86		4.96	5883.	•535	14.01	48.5	457.	3.04
27214.50 -5.66	53.5 540	4.36	5776	.218		45.0	388.	2.65
27215.50 -5.67		. 3.87	5856	.227	15.04	42.0	323.	2.23
27216.50 -6.18	40.8 471	-	6475	•252	15.55	38.5	263.	1.82
27217.50 -6.34	43.0 ":395	2.82	6723.		16.05	31.3	209	1.47
27218.50 -5.71	39.4 326	2.37	011/	.238	16.48	27.7	161.	1.15
27219-506-85	35.7 262	1.94		287	16.91	23 0	119.	.86
27220.50 -6.27	31.8 205		6845	•262	17 45	23.9 20.1	83.	•61
	28.0 154	. 1.19		.274	17 05	16-4	53.	.40
27222.50 -7.03	24.1 110	89	7752	• 301	*1.0 JU	16.4 12.1	29	
27223.50 -6.92	19.7 73	• 59	7681.	-247	10.74	8.0	14.	
27224.50 -4.35	16.5 43	• 41	4971	-147	18.39	. 8.8	17	-12
27224.55 -4.28	16:342	. 41	4900	•1H3	10.922	, 0.0	10.	•

TEST NO.	56A	MARI	KILA	NTISKIDA	SOMMERS	TIRES/WI	EI KUNWA	A T	energy of the second	1 1
STAND WG	T	TEST WGT			ALT	TEMP	WIND			DIREC
43000 LBS		3250.LBS	2	7.551 IN	i HG]	7.5 C		KTS		DEG MAG
43000000				1		5 MY 3/1		1.5 1 1/25		33.1
				EST DAY-						DAY
TOD	ACCEL	GND-SPD	DIST	KE	FBR		EBR	KTAS	DIST	KE 73
23400.19	-4.41	159.5	9039.			0.000			8329	
23401.00	-4.21	157.6	8822.			0.000	0.00	151.4	8124.	43.63
23402.00	-4.58	154.8	8558.			0.000	0.00	148.7	7874.	42.07
23403.00	-4.33	152.2	B299.			0.000	0.00	146.1	7629	40.61
23404.00	-4.44	149.7	8044.		746.	.029	· •11	143.6	7389	39.25
23405.00	-3.38	147.2	7794.			0.000	.17	141.1	7153.	
23406.00	-4:04	145.2	7547.	40.35		.017	.19	139.1	6921	36.85
23407.00	-3.14	142.9	7304.	39.12	_	0.000	•53	137.0	6693.	35.70
23408.00	-4.11	141.1.	7064.	38.10	851.	.032	.30	135.1	6469.	34.74
23409.00	-3.65	138.4	6828.	36.68	373.	.014	•50	132.5	6247	33.41
23410.00	-3.46	136.6	6596.	35.72	296.	.011	•52	130.7	6030	
23411.00	-4.20	134.3	6368.	34.51	1404.	.051	.76	128.4	5815.	
23412.00	-3.66	131.8	6143.	33.25	901.	.031	1.05	125.9	5605	30.19
23413.00	-3.10	129.9	5923.	32.31	282.	.010	1.14	124.1	5399	29.31
23414.00	-3.29	128.0	5705.	31.36	637.	.022	1.25	122.2	5196.	
23415.00	-3.98	125.8	5490.	30.32	1724.	.058	1.54	120.1	4995.	27.45
23416.00	-2.75	123.8	5280.	29.36	377.	.012	1.73	118.1		26.56
23417.00	-4.00	121.8	5072.	28.42	2219.	.068	2.03	116.2	4606.	25.68
23418.00	-3.81	119.5	4869.		2131.	• 065	2.50	113.8	4416.	24.66
23419.00	-3.05	117.3	4670.	26.35	1203.	.037	2.78	111.7	4230.	23.75
23420.00	-4.23	115.2	4472.	25.43	2946.	.087	3.25	109.6	4046.	
23421.00	-3.82	113.2	4281.	24.55	2508.	.074	3.69	107.7	3869.	
23422.00	-4.21	110.1	4092	23.20	-3185.	•098	4.35.			
23423.00	-3.11	108.4	3907.		1770.	.054	4.70	102.9	3521.	
23424.00	-3.42	1-06.6	-3726.	- 21.74	2314.	•069			3353•	
23425.00	-4.25	104.1	3548.	20.77	3520.	.105	5.62	98.7	3188.	
23426.00	-3.52	101.8	-3374	19.85	- 2672.	.080	6.14	96.4		17.70
23427.00	-2.91	99.7	3204.	19.03	1948.	.058	6.46	94.3	2870	16.94
23427.04	-2-88	99.7.	3197.	1.9.02	.1914.	•.057:	.6.46	. 94.3	2863.	T.D=.33

TEST NO.	56C	MAĤ	K II A	NTISKID/	SOMMERS	TIRES	/WET RUNW	ΑY		
	GT	TEST WGT		PRESS A		TEMP	WIND	VEI	WIND	DIREC
36000.LB	5	35200.LBS	2	7.565 IN	HG	21.0-C	4.8	KTS	200-0	DEG MAG
			4.1						al a la	
TOD	ACCEL	CND CDD	T	EST DAY-				S	TANDARD	DAY
27442.23	-4.22	GND-SPD.		KE	FBR .	UBR	EBR	KTAS.	DIST	KE
27443.00	-4.50		7353.		0.	0.000		142.7	-: 7018·	32.45
27444.00	-5.14		7161.		179.		•01	140.8	6831.	31.58
27445.00	-4.11		6917.		1051.	.052	~ • 20	137.9	6590	30.29
27446.00	-4.37	140.4	6678		85.	•004	•32	135.1	6355.	29.10
27447.00	-4.32	138.0	6443.		537.	.026	∙ •38	132.8	6125.	28.09
27448.00	-3.87	135.6 132.9	6212.		651.	• 0.31	•51	130.3	5899.	27.06
27449.00	-4.09	130.6	5986.		321.	•015		127.6	5677.	25.95
27450.00	-4.07	128.1	5763.	26.60	703.	•032	•75	125.4	5460.	25.06
27451.00	-4.08	125.7	5545.	25.57	. 859.	•038		122.9	5246.	24.07
27452.00	-3.94	123.4	5331.	24.62	998.	• 044	1.15	120.5	5037.	23.14
27453.00	<del>-4.35</del>	121.0	5121.	23.72	963.	-044	1.35	118.2	4832.	22.26
27454.00	-3.99	118.3	4915.	22.80	1546.	• 069	1.62	115.8	4632.	21.37
27455.00	-3.07	116.3	4713. 4515.	21.81	1358.	059		113.1	4434.	20:40
27456.00	-3.07	114.6		21.07	468.	•020	2.10	111.1	4243.	19.68
27457.00	-3.46	112.5	4320. 4129.	20.45	592.	•024		109.4	4055.	19.08
27458.00	-3.60	110.4	3940.	19.72	1152.	• 0.47.	2.38	107.4	3870.	18:38
27459.00	-4.06	108.3	3755.	19.01					· 3688.	17.68
27460.00	-3.87	105.9	3575.	18.28	2028.	062		103.2	3510.	16.98
27461.00	-4.02	103.4	3398.	17.49	1952.	•077		100.9	3336	
27462.00	-2.82	101.7	3226.	16.68	2235.	•090		98.4		15.43
27463.00	-4.31	99.3	3056.	16.12 15.35	1006.	•040	3.94	96.7	3000.	14.89
27464.00	-3.78	97.2	2890.	14.72	2772.	.108	4.33	94.2	2836.	14.15
27465.00	-3.63	94.3	2729.	13.86			4.70	92.2	2677.	13.54
27466.00	-3.83	92.8	2570.	13.42	2299.	•085	5.13	89.3	2521.	12.71
27467.00	-3.62		2417.	12.72	2449.		5.45		2370	
27468.00	-4.65		2266	11.95	3674.		5.86	85.4	2224.	11.61
27469.00	-4.16		2120	11.25	3247.	.139	6.36	82.6		
27470.00	-2.82				1865	•123	6.87	80.0	1939.	10.21
27471.00	-5.01			10.24	4311.	166	7.21	16.9	- 1805	
27472.00	-4.45		1706.	9.39	3821.		7.63 8.21	76.1	1674.	9.24
27473.00	-4.17		1576.	8.77	3611.	.134		72.7	1545.	8.43
27474.00	-2.46		1452.	8.56	1785.		8.71 8.91	70.1	1422.	7.84
27475.00	-6.96		1329.	7.72	6814		9.57	69.3	1308.	
27476.00	-3.40		1213.	7.06	3020.	.111	10.08	65.5	1190.	6.84
27477.00	-4.84		1100.	6.67	4649	174	10.49	62.5	1080.	6.22
27478.00	-5.26	62.2	993.	6.02	5203.	195	11.04	60.6	976.	5.85
27479.00	-3.89	59.4	891.	5.49	3779.	140	11.47	57.4	875.	5.24
27480.00	-4.10	57.6	791.	5.17	4064	_		54.6 52.8	779.	4.75
27481.00	-6.70	54.1	597.	4.57	6987			52.8 49.4		4.45
27482.00	-3.86	50.7	509.	4.01	3972.			49.4	601.	3.89
27483.00	-4.07	49.1	525.	3.76	4226.	·160			- 520.	
27483.58	-3.92	47.1	478.	3.46	4110.				446.	3.14
		· i				****	1000	42.4	402.	2.87

TEST NO.	57A	MAR	K II AN	TISKID/	SOMMERS	TIRES/W	IET RUNW	ΑY		
STAND WE	i T	TEST WGT	م ،	RESS A	LT	TEMP	WIND	VEL	WIND	DIREC
43000 LBS		43200 LBS		.589 IN		18.3 C			195.0	DEG MAG
						;				
			TE						ANDARD D	
TOD	ACCEL	GND-SPD	DIST	ΚĒ	FBR	- UBR	EBR	KTAS	DIST	KE
23301.61	-4.18	157.8	8755.	47.65	71.	•005	•00	151.2	8033.	43.54
23302.50	-4.07	155.5	8520.	46.25		0.000	• 05	148.9	7811.	42.22
23303.50	-4.52	153.1	8259.	44.83	173.	.008	• 06	146.6	-7566•	40.90
23304.50	-4.02	150.5	8003.	43.29		0.000	.06	144.0	7325.	39.45
23305.50	-4.32	147.9	7751.	41.85		0.000	.07	141.5	7087	38.10
23306.50	-3.73	145.6	7504.	40.56		0.000	.07	139.2	6855.	36.89
23307.50	-4.27	143.2	7259.	39.20	766.	.032	.19	136.8	6625.	35.61
23308.50	-3.34	140.9	7020.	37.98		0.000	.23	134.6	6401.	34.47
23309.50	-4.07	138.9	6784.	36.90	783.	.031	•30	135.6	6180	33.46
23310.50	-3.86	136.3	6552.	35.51	755.	.029	•55	130.0	5962.	32.16
23311.50	-3.40	134.4	6323.	34.55	271.	-010		128.1	5749.	31.26
23312.50	-3.45	132.2	6099.	33.45	450.	.017	.72	126.0	5539.	30.23
23313.50	-3.41	130.3	5877.	32.45	575.	.021	- 82	124.1	5333.	29.30
23314.50	-4.27	127.9	5659.	31.28	1858.	•067	1.15	121.7	5129.	28.21
23315.50	-2.80	125.7	5445.	30.23	-63•	•002		119.6		27.23
23316.50	-3.78	123.8	5234.	29.33	1443.	.052	1.49	117.7	4734.	26.38
23317.50	-3.26	121.8	5027.	28.36-	960.	.034	1.74	115.7		
23318.50	-3.54	119.8	4823.	27.47	1467.	050	1.97	113.8	4353.	24.65
23319.50	-3.88	117.5	4523.	26.39-	2094.		2.37		4166.	
23320.50	-3.94	115.5	4426.	25.53	2336.	077	2.75	109.6	3984.	22.85
23321.50	-3,66	112.8	4234.	24.34	<b>2203</b> .	.071	3.26	106.9		21.74
23322.50	-3.68	110.9	4045.	23.52	2366.	.073	3.65	105.0	3630.	20.98
23323.50	-3.80	108.6	3860.	22.56	2662	<b>-</b> 082/	4.14			20.09 -
23324.50	-3.32	106.4	3679.	21.67	2129.	•066	4.56	100.6	3291.	19.26
23325.50	-4.15	104.3	3500.	20.80	3358.	.102	5.06		3126	
23326.50	-4.05	101.9	3326.	19.84	3346.	.100	5.64	96.1	2965	17.57
23327.50	-3.92	99.5	3156.	18.92	3281.	-100		93.7		-16.72
23328.50	-3.89	97.3	2990.	18.10	3343.	•101	6.72	91.6	2655.	15.96
23329.50	-4.05	- 94.9	2828	17-21 -			7.30			
23330.50	-2.72	92.7	2670.	16.44	1972.	.059	7.67	87.1	2361.	14.43
23330.56	-2.68	92.6	2561.	16.41	1917.	•058	7.67	87.0	2353.	14.41

TEST NO. 578	MARI	K II AN	TISKIDZ	SOMMERS	TIRES	WET RUNWA	AY		
STAND WGT	TEST WGT	ום	PESS A	i T	TEMP	WIND	VEL.	WIND	DIREC
38000.L9S	35300 LBS		590 IN		18.3 C	- 4.9		215.0	DEG MAG
30000€⊏33	303001203	Ī				110 - 110		1 = =	
		TF	ST DAY-				S1	ANDARD [	DAY
TOD ACCE	L GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
25465.50 -4.1		7674.		. 85.	-004	.01	140.7	6925	33.32-
25466.50 -4.3		7427.	35.83	483.	.021	.11	138.2	6695.	32.13
25467.50 -4.0		7184.	34.53	370.	015	-23	135.6	6468	-30.93
25468 50 -4.3		6944.	33.34	799.	.034	•38	133.2	6245	29.83
25469,50 -4.0		6710.	32.20	617.	.025	•55	130.8	6027.	28.77
25470.50 -3.4		6480.	31:09	126.	.005	.65	128.4	5814.	27.74
25471.50 -3.7		6253.	30.17	523.	.021	.70	126.4	5604	26.89
25472.50 -3.8		6029.	80.65	839.	.032	.91	124.1	5397.	25.89
25473.50 -3.1		5810.	28.21	127.	.005	98	122.1	-5195•	25.08-
25474.50 -3.5	. 1	5594.	27.40	643.	.025	1.07	120.3	4996.	24.33
25475.50 -3.3		5381.		618.	023	1.21	118.2	4801	23.50
25476.50 -3.5		5172.	25.64	905.	.035	1.38	116.2	4608.	22.71
25477.50 -3.8		4966.	24.75	1446.	.054	1.64	114.1	4418	21.89
25478.50 -3.5		4764.	23.82	1205.	.045	1.93	111.8	4233.	21.03
25479.50 3.1		4566	23.09	875 ·	0-32-	- 2.09 -		-4052-	
25480.50 -3.9		4370.	22.20	1917.	.070	2.41	107.8	3872.	19.54
25481-50 -3:6		41.79.	21.44	1647.	062	2.71	1-05.8	3697	18 • 84 -
25482.50 -3.5		3991.	20.51	1.717.	.062	3.07	103.4	3524	17.99
25483.50 -3.1		3807.	19.83-	1358.		-3.32	-101-+6-	3357	1737
25484.50 -3.5		3626.	19.09	1842.	.067	3.61	99.6	3192.	16.69
25485.50 -3.9		3449.	18.32	2457.	090	4- 01-		3030•	15.98
25486.50 -3.3		3276.	17.54	1856.	.068	4.37	95.3	2873.	15.27
25487.50 -4.1	9 99.5	-3106.		- 2987.	.105	4.80 -			14.59
25488.50 -3.8	3 97.0	2939.	15.94	2667.	• 095	5.29	90.6	2566	13.80
25489.50 -4.7	2 94.9	2778.		3830•	136			-2419	
25490.50 -4.2	91.7	2520.	14.27	3396.	.120	6.39	85.5	2275.	12.29
25491.50 -4.0	2 89.6	2467.	13.61	3226.	112		83.4		-11-69
25492.50 -4.0		2318.	12.87	3314.	121	7.35	80.9	2001.	11.02
25493.50 -4.4	5 84.8	2173	12.18		- 1.39	7.87	78.6		.10.39
25494.50 -4.6		2032.	11.34	4277.	•151	8.47	75.7	1742.	9.63 9.02
25495.50 -4.1		1896.	10.66	3808.	.135	9.00	73.2	1619.	-
25496.50 -4.5		1765.	10.00	4296.	.153	9.54	70.8	1501.	8.42
25497.50 -3.7		1638.	9.32	3480.	.125	10.03	68.1	1387.	7.81
25498.50 -4.1		1514.	8.77	4005.	.140	10.48	66.0	1277•	7.32
25499.50 -4.8		1394.	8.14	4925.	•172	11.03	63.4	1170.	6.76 6.15
25500.50 -4.6		1280.	7.46	4796	.168	11.60	60.5	1067	5.70
25501.50 -2.3	-	1170.	6.95	2109.	•074	11.93	58.2	971.	5.69
25501.60 -2.1	.0 64.0	1160.	6.94	1894.	•065	11.93	58.1	962•	5.09

* *			-	~	DISOMMER			4"		Marie Land
STAND WG		TEST WGT		PRESS	ALT	TEMP	WIND	VEL	WIND	DIREC
34000°LBS		34550.LBS	•	27.593	IN HG	21.1 C	6.8	KTS	237.0	DEG MA
				TEST 04	Y			51	FANDARD.	DAY
TOD	ACCEL	GND-SPD	DIST		FBR	- UBR	EBR	KTAS	DIST	KE
27582.10	-4.37	147.2	7699	. 33.1	4 0	0.000	0.00	137.1	6617.	28.28
27583.00	-4.16		7478	. 32.1	1 0.	0.000	0.00	134.8	6417.	27.37
27584.00	-4.18		7235	31.0	4 70	. 004-	00	132.5		26.41
27585.00	-4.56	139.9	6997	. 29.9	2 643	032	.11	129.9	5986.	25.41
27586.00	-3.77	137.3	6763	. 28.8	1 - 0.	0.000	•19	127.4	5776.	24.43
27587.00	-4.21	135.1	6533	. 27.9	1 600	. 029	• 25	125.3	5571.	23.62
27588.00	-4.21	132.4	6307	. 26.8	1 778.			122.6	5368	
7589.00	-3.95	130.1	6086	. 25.8	8 645		•58	120.4	5170.	21.81
27590.00	-3:25	127.9	5868	. 25.0	3 - 0,	0.000	•65	118.3	4978	-21.06
7591.00	-4.05	125.8	5654	. 24.2			.77	116.3	4788.	20.34
7592.00	-3.59	123.3	5444	. 23.2	4 - 644			113.7		19.47
7593.00	-3.70	121.1	5237	. 22.4	4 896		1.15	111.7	4417.	18.77
7594.00	-3.42	119.0	5034	. 21.6	7 730.	.032	1.31	109.6		18.09
7595.00	-3.96	117.0	4835	. 20.9	5 1432		1.52	107.7	4063.	17.45
7596.00	-2.97	114.8	4540	20-1			1.71			-16.75
7597.00	-3.33	113.3	4447	. 19.6	4 968.	.041	1.79	104.1		16.30
7598-00-	-4.13	-110-7-	4258	18.7	31939.	E80		101.5	3555	
7599.00	-3.09	108.8	4073				2.36	99.6	3394	14.95
7600.00-	-3.69	-106.7	3891	. 17.4	21674	0.71	2-62	97.6	3235	-14.35
7601.00	-3.48	104.5	3713	. 16.7		.066	2.90	95.5	3079.	13.72
7602.00	-3.66	102.5	3538	16.0				93.5		-13-17-
7603.00	-3.76	100.4	3367	. 15.4			3.54	91.5	2778.	12.59
7604.00	-3.30	98.2	3200	. 14.7			3.85	89.3	2632.	12.01
7605.00	-3.37	96.1	3036	. 14.17			4.15	87.3	2490.	11.46
7606.00	-3.91	94.1	2875	. 13.5			4.50	85.4		-10.97
7607.00	-4.16	91.7	2718	. 12.8	2865.	.120	4.94	83.0	2215.	10.36
7608.00	-3.87	89.1	2566	12.1	2664.	•115	5.37		2082.	9.75
7609.00	-4.23	86.9	2417	11.5		.127	5.80	78.3	1954.	9.22
7610.00	-4.12	84.2	2273			.128	6.27	75.7		8.62
7611.00	-3.76	82.0	2132.	. 10.28	2841.	.113	6.68	73.5	1708.	8.14
7612.00	-3.22	80.0	1996	9.80	.2344	.092-	7.01	71.6	1592.	
7613.00	-4.56	77.8	1862			.153	7.44	69.4	1479.	7.25
7614.00	-3.67		1734.		2996.	.120	7.89	66.7.	1368.	6.69
7615.00	-3.85	73.0	1509	8.16		.129	8.26	64.8	1263.	6.32
7616.00	-3.82	70.6	1488			.129	8.67	62.4		5.87
7617.00	-4.61	68.3	1370.			.169	9.10	60.1	1062.	5.45
7618.00	-4.16	65.5	1257			.152	9.57	57.4	967.	4.96
7619.00	-4.72	63.0	1149.	6.07		.173	10.01	55.0	876.	4.55
7620.00	-3,97	60.3	1045			.143	10.44	52.3	789.	4.12
7620.90	-2.63	58.4	955			.091	10.65	50.5	716.	3.84

STAND WGT		TEQTUGT	<u>.</u>	RESS-A	L-T	TEMP	WIND	VEL	WIND	DIREC
43000 . L. BS	Ī	43500.LBS	27	.543 IN	HG :	17.8 C	3.7	KTS	220.0	DE G MA
معد بالسيامة كران دين	ا اللهٔ تستیلی داری	43500.LBS						ST	INDARD (	) AY
T00			15	SIDATE				KTAS	DIST	····KE
	ACCEL	"GNO-SPU	0121	1.7.4.7	162.	000	.01	150.0	9374.	42.85
23889.00	-4.61	156.5	10282 .	47.17	105 •	-0-07-0 -0-07-0		-147-0-	91-28	41-14
23889.00 23890.00	-4.25	153.4	10022	45.33	0	0.000	•11	144.7	8887	39.88
23891.00	-4.09	454 *	9764	A C. UM	11.4	16 46 11 11 11		T-141	900,0	
23891.50		149.9	9637	43.25		2.000	.11	140.1	8418	37.34
23893.00	-2.58	146.4	9262.	41.25	0.	0.000				
23894.00	-2.05	145.8	9017	40.92		0.000			7963.	
	-5.15		8772.	39.28	2334.	.082	49	136.6		34.31
23896.00	-3.74	140.4	8533%	-37.98	2334 • 539 •	.019	. 73	134.3	7520	33.22
	-3.45		8298 •	36.81	13' 25'	.009	. 83	132.1		
23898.00	-3.97	136.0	8066.	35.63	1118.	. 039	1.01			32.13
23899.00	-3.08	×133.9		34.54		.002	1.12	127.9	7.092	
23900-00	-3.80	132.1	7614 .	33.62	1163.		1.25	125.1	6884	30.26
23901.00	-2.84	129.9	7394 .	32.52	. 7.	.000	1.40		6679.	
23902.00	-2.88	128-4	7176	31.76	112		- 1.41		6478	28.55
	-3.16		6907.	30.57	5/8.		1.55	120.1	6229.	
23904.25			6696	- 29 <del>.5</del> 6	1316.	042	-1-79			26.51
23905.25	-2.92	121.8	6489.	28:57	571.	.019	2.00	116.0	5840.	
	-2.29		6284	28:01	0.	-0.000	2.01	114.8		25.08
23907.25	-3.75		6082.	27.23		.061	2.22	113.1	5466	
23908-25	-2:87		5 884 T	26-23	919.	.028	2.50	111.0	5282.	
23909.25	-3.20	114.9	5688	25.42	1494.		2.75	109.2	5101.	
23918:25				24.72	598	.018	2.92	107.6	4925	22.04
	-3.34			23.99	590. 1893.	.057	3.18	106.0	4750.	
23911.25			5118.		2071.	.361	3.56	104.0	4577	20.60
23912.25	34 31	107.7	LO35 .	22.32	2296	.967	3.94	102.1	4408.	19.84
23913.25 <del>23914.25</del>	-3 . 4:	10747	4755	- 21 . 55-	7.2.3-	-021-	4.21	1-9-02	-4242.	19.12
			1.577	24.23	1584.	-047	4.32	99.4	4082	15.0
23915.25	2.00	105.0	45100-	2020	1886.	05 b	4.72	97.1	3920*	1-79
23916.25			1.270	10 77	1284	. በፕሬ	4.95	95.7	3763	1 ( • 4:
23917.25 <del>23918</del> .25	-2.39	9 101.2	4230 6	4.04.5.	2294			94.3	3-608	16.9
			7000	18.25	2349	.068	5.71	92.0	3454.	16.13
23919.25 <del>23928.25</del>	-3.12	97.4	3894 •	10.20	40.72	0.20	5.Q1		3306	15-6
23920-25	-2.0	90.1	37311	47 74	3242	.091	5.29	89.2	3159.	15.1
23921.25	-3.6	7 94.5	3569.	17.21	3242	044	G • C 9	87.3	-3016×	
23921 • 25 <del>239</del> 22 • 25		992-6	3412	-10002	7075	007	7 07	85.6	2874	13.9
23923.25	-3.59	9 90.9	3257.	15.91	3275	.093				13.3
23924-25	-2.7	788-9-	3105	15.22	2245	0.70	7.78	82.2		
23925.25	-2.9:	1 87.4	2957	14.72	2486	072	7.78	06.2	2469	
23926.25	3 2	785-4	2811 a	14584	3051	······································	0.21	70 7	2339	11.79
	-7 2	7 97 3	2668_	13.54	3118		8 • 60	(0.1	2337	T T T T T
-2-3928 - 25	3-1	781-4	2528	-12.77	3076	0.88	9.11	75.0	2000	10.8
23929.25	Q	7 80.7	2392.	12.55	0 .	0.000	9.18	75.6	2090	10.0

TAND WGT		TEST-MET		RESS-	AL		TEMP	NIND	VET-	MIND	DIKEL
TAND WGT 8000.LBS	- 3	18550.LRS	210	, 540	TM	ם טרו	. u . u				
TOD				21 UA		- F D D		FBR-	KT-AS-	0101	
TOD	ACCEL	GNO-SPU	0121	76	<b>7</b> B	977.	.042				
5976.91	-4.94	145.8	8922 •	36.3	3 U	O 1 O 0	0.00		138.1	7950	-32.0
5976.91 5977.75	-3.58	143.8	8717	35.4	27	8 .	3.000		476 7	フフウア	31 . 2
5978.75 5979.75	-3.70	141.8	84//*		A			4 4	-4-3-37	7506	30.0
5979.75 5980.75 5981.75	-3.99	139.3	8239	33.	1 U	2200	0.000	-14	131.9	7290 •	29.2
5980.75	-3.49	137.5	8005 •	32 •	24 30	<u> </u>	0 0 0 0 0		129.8	7077	28.3
5981.75	-3.64	135.2	7776	31.4	4.0	701	.033	.28	127.4	6867.	27.3
5982.75 <del>598</del> 3.75	-4.11	132.8	7549 •	3U • 1	12	( ) L =		30 -	125-3-	6661	-26.3
5983.75	-3.54	130.6	7327	290	11	2030	• 011	- 40	123.3	6459.	25.5
5984.75	-3.12	128.6	7109.	28.	24	E40		.46			
5985.75	-3.54			27.	36	2170	017	• 54			24.0
	-3.28	124.7	6681.	26.	54	356.		- 70	117.4	5871	23.1
5987 . 75	-3.60	122.5		25.		350.	047	.80	115.5		22.4
		120.6	6267.	24.	82	344.	.013	. 8 .00	-443-6-	5495	-21.7
5989.75	3.05	-118.7	6065	24%	05' -	.4277	01.7	1.02	111.9	5311	21.0
5990.75	-3.55	117.0	5866.	23.	35	1117.	.043	1.02	400.7	54-31 L	20.2
5991-75-	-2.92	-114.7	5671 •	22.	46	475	019	4 25	100.4	4954	19.7
5992.75	-2.99	113.4	5478.	21.	93	675.	.025	1.29	4.063		19.0
5993.75	3.47	-111.2	5289	21%	09 -	1345	.051	1.50	404 6	4608.	18.4
			5103.	20.	45	558.	.021	1.65	104.6		17.6
5495.75	-2.50	109.5 107.8	4919	19.	83	382	014	1.74	404 (	4274.	17.3
5996.75	-3.61	106.2									
5997.75	-2.96		4561	-18~	46	-1146.		2.23	33.2	7054	16.1
5998.75	-2.65	102.6	4387.	17.	95	827.	.030	2.36	97.9	3951.	
5999.75	-2-93	-100.9	4215	17.	38~	1253	046	-2.55	96.3	27.74	14.9
6000.75			10.5	4 4	70	4 4 1. /.	1/4/2	2.79	94.3	3039.	T 4.
6001.75		-97.7	3881	-16.	29	-1516	055	2.95	-95.1	3400	47
6002.75	-3.08	95.3	7710	4 5	1. O	4608.	-1161	5.29	9001	3337	
6003.75	2: 49	94.2	3558	15.	13	-1031.	0-3-8	- 3.43	89.6	3192	13.
6004.75	-4.40	91.9		4 1		71.1.0	122	3.87	8/.5	34414	120
6004.75	32	90.3		13.	92 -		0.000-	4-02	85.9	-2919	12.
				4.7	C A	2060	4 0 6	4 - 211	744	C / / U D	1 6 0
CACT 35	<del>-3-4</del> 0	89.3 86.9	-2947-	12.	88	2114.		4.63	82.5-	2633.	11.
C000-75	-2-35	85.4	2658	11	94	2540	-0-0-8	5.20	79.4	2371	-10.
6010.75	-3, 00 -3, 20	81.4									
60144.75	-2.65	79.7		. 10.	84	15744		-5.87	75.5	2120.	9.
6012.75	-7 60	77.8	2250 .		33	3082.	.106	6.23	13.1	1 220 .	7.
6012-75	-3.10	75.7		9.				6.59	71.7	- 1880·	8.
	-3.45	74.0	1994 .	9.	34	3058.	.104	6.94	69.9		8.
6014.75	-2.76		1871.		84	2302.		7.26	68.0	1654.	
6015.75			1751		43	3440 .		7.60	56.3		
6016.75	-3.68		1634.		91	2982.		7.99		1440.	
6017.75	-3.66	66.3	1521 .	7	-50	3281	.112	8.33	62.4	1337.	
6018.75	-3.42		4.414	7.	-0-1	3173	-106	8.70		1236.	6.
6019-75-			1304.	ĸ.	60	3932	. 133	9.07	20.4	1141.	
6020.75	-3.85			. 6	4 3-	3260		9.44	56.2	1049.	5.
26021.75	-3.22		1201	-	72	3544	121	9.79	54.2	959	4 .
26022.75	-3.49	57.9	1101.	5	. 79	2717	.092	10.08	- 52.6	-873	-4.
26023.75	-2.69	56.2	962.	2	.24		.091	10.13	51.8	834	4.

TEST NO. 58C	MARK	II.	ANTISKID/SOMMERS	1	TIRES (WORN) / WET	RUNWAY
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		TEST WGT		PRESS	ALT	TEMP	MIND	VEL		DIREC
34000.L		34550.LBS		27.549	IN HG	22.8 C	2.9	KIS	240.0	DEG MAG
		GND-SPD		TEST DA	Y			STA		
	11.000	0110, 0.0		7 7 144		A 151.7	- WIT	111111111111111111111111111111111111111	OIST.	KE,
27749.G		138.2	7681			0.000	0.00	131.6	6'870.	26.05
27750.0				. 28.2		004		129.3	6663.	
27750.7				. 27.5			. 0 ₹	127.5	6507.	
27751.7				26.6	40			125.5	6303.	
27752.7			6838	25.7	5 7	001		123.3	6101.	
27753.7			6620	. 24.9	1048	048		121.4	5903.	22.17
27754.7			6408				• 35	118.5	5708.	
	5 -2.76		6198			0.000	-, 35	117.0	5519.	
27756.7			5991			057	.50 .61	114.9	5330.	19.89
27757.7							61	112.8	5147.	
27758.7			5590			055	•67	111.0	4966.	
27759.7	5 - 3, 76	115.1	53.95	20.2	5 1088	348	. 82	109,1	4,788.	17.91
27760.7			5203				1.01	106.8	4614.	
27761.7	5 -3.12	111.1	5013	18.8	9 650	027	1.08	1.05.3		16.68
27762.7			4827	. 18.2	7 923		1.24	103.5	4275.	
	5 -2.14			. 17.6	Q Q	0.000	1.32	101.5	4110.	
27764.7		105.5	4463	. 17.0	2 2881		1.59	99.8	3945.	
	5 - 2, 37				9 305	0,12	1.81		3787.	14.32
27766.7			4115			. 054	1.96	96.8	3631.	
	0 -3,36		3903	15.1	0 1545	06.2	2,+23	93.8	3440.	13.25
27769.0			37 38		0 1397		2.48	91.9	3290.	12.71
27770.0	0 - 3.06	95. 4	3574	1,3,9	1 1443	. 056	2.73	89.9		12.18
27771.0		93.6	3414	. 13.4	6 1626		2.95	88.4	2999.	11.77
27772.0			3258		1262	. 648	. 3.15	86.8	2859.	11.35
27773.0			3164	. 12.3	8 2418	093	3.48	84.7	2720.	10.79
	0 -3.38		2954	11.8	4 2121		3,81	82.8	2585.	10.31
27775.0		85.8	2807				4.12	80.6	2453.	9.78
2,7776 • 0			2663				4.42	79.0	2325.	9.40
27777.0		81.9	2523				4.73	76.9	2199.	8:89
27778.0			2385				4.97	75.3	2076.	8.53
27779.0	_		2251				5.15	74.3	1957.	8.31
27780 · C			21 26				5.55	71.9	1839.	7.78
27781.0			1992				5.92	69.9	1725.	7.36
27782.0			1868				6.22	67.9	1614.	6.94
27783.0			1746				6.56	66.2	1506.	6.60
27784.0			1629				6.95	63.8	1401.	6.13
27785.0	-		1515			_	7.36	61.6	1299.	5.71
27786.0			1405				7.62	59.7	1203.	. 5 • 36
27787.0	-		1297			. 146	7.93	58.1	1107.	5.09
27788.0			1194			130	8.33	55.7	1016.	4.67
27789.0		58.2	1095			098	8.61	53.8	929.	4.36
27790.0			998	4 . 8	0 4800	. 176	9.09	51.7	843.	4.03
27791.2		52.4	884	4.2			9.47	48.2	742.	3.50
27792.5	0 -4.28	49.8	776	3.8	0 433+	. 161	9.85	45.7	648.	.3.14
27793.5	0 -4.21	47.3	694	. 3.4			10.23	43.3	576.	2.82
27794.5			616		5 4681	172	10.58	40.7	508.	2.49
27795.5		42.1	5 43	. 2.7			10.99	38.2	444.	2.19
27796.7	5 -3.99	39.2	457	. 2.3			11.25	35.4	371.	1.88
27797.7			392	2.0		. 219	11.63	32.4	314.	1.58
27798.7	5 -4.19	33.7	334	1.7	4 4533	. 181		30.0	265,	1.36
27799.7			280	1.4				27.2	218.	1.11
27800.7	5 -3.61	27.4	231				12.42	23.9	176.	. 86
27801.0	7 -2.15	26.9	216				12.43	23.4	164.	.83

TEST NO. 5	59A	MARK I	IT ANTIS	KIDZSOM	MERS TIR	RES (WORN	₽)/WET KU		-	
STAND NO	т	TEST WG	т р	RESS, AL	T	TEMP	WIND	VEL	WIND	DIREC
STAND MG		3350.LB		509 IN	HG 3	85.0 C	3.5	KTS	215.0	DEG MAG
43000.LBS	-									- 22 72
	-7-	<u> </u>	TE	ST DAY-				STA	NDARD. [	)AY
TOD	**************************************	CMD=CBD	DIST	KE				KTAS	DIST	KE
	-4.68	160.0	10413.	49.13	0.	0.000	0.00	149.5	9052.	42.55
45589.84	1	157.4	10175		2 am 20 a	0.000	0.00	147.0	8834	41.14
45590.75	-3.97 -4.16	155.3	9911.	46.27		0 - 0 0 0	0.00	145.0	8600.	40.02
45591.75	-3.99	152.6	9550.	44.68		0.000	0.00	142.4	8368	
45592.75	-4.05	150.6	9395	43.53		0.000	0.00	140.5	8142.	37.59
45593.75	-3.70	147.9	9143.	42.00		0.000	0.00	138.0		36.24
45594.75 45595.75	-3.26	146.0	8595.	40.93	=0.	0.000	0.00.	136.2	7698	35.30
45596.75	-3.59	144.2	8550.	39.90	255.		.02	134.4		-34-39-
45597.75	-3.51	141.9	8409.	38.62	261.	.010	.14	132.2	7268	33.26
45598.75	-4.14	139.8	8171.	37.52	1277	.045	31	130.2		32.28
45599.75		137.3	7936.	36.20		0.000		127.9	6850	31.12
45600.75	=3.29	135.8	7707	35.37	404.	014	-7.52	126.4	6647	30-39
45601.75	-3.81	133.6	7479.	34.23	1186.	.042	.75	124.2	6446	29.39
	-3.51	131.3	7256	33.08	971.	033		122.1		28-37
45603.75	-3.10	129.3	7036.	32.09	557.		1.17	120.2	6054	
45604.75	-3.01	127.8	6819.	31.32	522		1:25	14,041		26.82
	-3.46	125.6	6506.	30.26	1283.	.042	1.52	116.6	5675	25.89
	-2.60	123.7	.6395	29.38	251.	008	1.67	114.9	5490	25.11
45607.75	-3.53	121.5	6188.	28.32	1707.	.054	2.01	112.7	5306.	24.18
45608.75	-1.24	120.5	5984.	27.85	Ů.	0.000	2.06	111.7	5130.	23.77
45609.75	-4.60	118.3	5781.	26.87	3345.	.102	2.46	109.7	4951	
45610.75	-2.83	116.4	5584.	26.01	1075.	.033	2.81	107.9		22.15
45611.75	-2.90	114.8	5388.	25,29	1294.	.039	3.03	106.3	4606.	
45612.75	-4.05	112.9	5196.	24.44	2945.	.•0₽₽	3.45			19.82
45613.75	-2.84	110.3	5008.	23.35	1443.	.043	3.92	102.0	4271 • 4111 •	
45614.75	-3.04	109.4	4623.	22: 98	1792.		4.07	101.2		
45615.75	-3.20	106.6	4540.	51.65	5553.		4.59	98.5	3949	18.13
45616.75	-2.99	165.6	4461.	21.42	1499.		4.83	97.6	3640	
45617.75	-3.29	103.5	4285.	20.55	2403.		5.26	95.5		16.60
45618.75	-3.05	101.2	4113.	19.67	2162.		5.70	93.4 91.7	3340	
45619.75	-3.44	94.5	3942.	19.00	2777.		6.11	89.8	3195	
45620.75	-3.14	97,5	3776.	18.23	2470.		6.50	88.2	3054	
45621.75	-2.89	95.8	3613.	17.61	2195.		6.92	86.4		14.21
45622.75	-3.14	93.9	3453.	16.93	2605.		7.32 7.69	84.7	2778	
45623.75	-2.84		3296.	16.31	2272		· -8-09 ··	B-3 · 0 · ·		
45624.75	-3.23		3142.	15.69	2874		8.52	81.2	2513	12.55
45625.75	-3.10		2991.	15.03	2781.			- 79-6-		12.05
45626.75	-2.69		2843.	14.45	2356		8.99	78.7	2318	
45627.29	-2.12	85.9	2764.	14.16	1615.	•045	0 0 7 7	1041		

TEST NO. 61A	MĀR	II A	NTISKID/	SOMMERS	TIRES/	WET RUNW	AY ,		* 2
STAND WGT	TEST WGT	;	PRESS A	LT	TEMP	WIND	VFI	WIND	DIREC
43000 LBS	42900.LBS		7.590 IN		22.2 C		KTS		DEG MAG
							.,,,,	44,44	02- 111-
	,	TE	EST DAY-				ST	AND ARD	DAY
	GND-SPD	DIŞT	KE	FBR	UBR	EBR	KTAS	DIST	KE
25014.14 -4.16	147.3	8826.	41.22	0 .	0.000	0.00	144.8	8545.	39.92
25015.00 -4.36		8613.	39.97	0.	0.000	0.83	142.6	8340.	38.71
25016.00 -3.89		9370.	38.51	Э.	0.000	0.00	140.2	8105.	37.39
25017.00 -3.46	pit a dancer	<b>8132.</b>	37.51	. 0 .	0.000	0.00	138.1	7874.	36.32
25018.00 -3.73		7896.	36.35	321.		.02	136.0	7646.	35.20
25019.00 -3.99		7664.	35.10	762	.030	.13	133.5	7422.	33.99
25020.00 -3.50		7437.	34.04	282.		.27	131.6	7.202.	32.96
25021.00 -3.16		7213.	33.05		0.000	.29	129.7	6985.	32.01
25022.80 -3.73		6992.	32.03	901 .		• 39	127.7	6771.	31.02
25023.00 -3.31		6774.	entrement conjuments in the bill	478	.017	-54	125.6	6.561.	30.01
25024.00 -3.18	_	6560.	30.06	457.		.6!	123.7	6353.	29.12
25025.00 -3.19		6349.	29.19		.021	•74	121.9	6149.	28.27
25026.00 -3.60		6142.	28.36	1267.	· 043	.91	120.1	5949.	27 . 47
25027.00 -3.17		5938	27.22	841	.028	1.18	117.7	5751.	26.37
25028.00 -3.14	115.3	5736.	26.56	904.		1.23	116.3	5556.	25.73
25029.00 -2.74		5539.	25.72	569	.018	1.45	114.4	5365.	24.92
25030.00 -2.25		5344.	25.01	110 .	. • 003	1.51	112.8	5176.	24.22
25031.00 -2.95		5152.	24.05	1159.	. 035	1.78	110.6	4991.	23.30
25032.00 -3.55		4963.	23.34	2175.		2.06	109.0	4807.	22.62
25033.00 -2.98		4777.	22.52	1400 .		2.48	107.3	4628.	21.92
25034.00 -3.17		45 95.	21.81	1743 •	• 053	2.79	105.4	4452.	21.13
25035.00 -2.7.8		4416.	21.15	1314	.039	3.03	103.8	4278.	20.49
25036.00 -3.30		4239.	20.37	2104.	.063	3.38	101.8	4107.	19.73
25037.00 -3.12		4066.	19.69	1929.	.059	3.69	100.1	3939.	19.08
25038.00 -2.80		3895.	18.91	1616.	.048	4.04	98.1	3774.	18.32
25039.00 -3.02	98.4	3728.	18.39	1969	.059	4.29	96.8	3612.	17.83
25040.00 -3.59		3564.	17.57	2954 .	.089	4.75	94.6	3453.	17.02
25041.00 -2.57		3403.	16.93	1554.	.046	5.06	92.9	3298.	16.41
25042.00 -3.54	92.7	3245.	16.33	2930 •	.086	5.42	91.2	3144.	15.83
25043.00 -3.09	90.6	3090.	15.60	2409 .	.071	5.84	89.1	2995.	15.12
25044.00 -2.81	83.9	2938.	15.01	2113.	.063	6.17	87.4	2848.	14.55
25044.29 -2.58	88.4	2897.	14.85	1819.	. 054	6.18	87.0	2808.	14.40

TEST NO.						TEHP	WET RUNN	VEL	WIND	DIREC
STAND NGT		TEST WGT		PRESS	ALT		47.00.00	KTS	145.0	DEG MA
3800C.LES		38150.L9S	27	.592 I	N AG	23.9 C	2	V12	140.3	MT SWE
			T	ST DAY				ST	ANDARD	
T00	A CCE I	GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
27228.80	-3.69		8493.	35.37	and the second second	0.000	0.00	140.5	7987.	33.23
27229.75	-3.79		8263.			. 001	.01	138.4	7769.	32.20
27230.75	-3.17		8024.	33.37	0.	0.000	.01	136.5	7543.	31.35
27231.75	-3.57		77.09.			.000	.01	134.6	7321.	30.48
27232.75	-4.01		7557.	31.40			.11	132.4	7102.	29.48
27233.75	-3.40		7329.		0.	0.000	.21	130.0	6886.	28.42
27234.75	-3.74		7104.	29.46	The second section of the second section of		.21	128.2	6674.	27.65
27235.75	-3.63		6883.	28.35		.011	.35	125.7	6465.	26.56
27236.75	-3.46		6666.	27.50			.3€	124.1	6261.	25.90
27237.75	-3.72		6453.	26.60		. 027	.50	121.8	6059.	THE RESIDENCE OF COLUMN
27238.75	-3.89		6243.	25.63			.68	119.6	5860.	
27239.75	-3.49		6036.	24.75			. 85	117.5	5666.	
27240.75	-3.06		£834.	23.99			.93	115.6	5475.	22.49
27241.75		117.3	5635.	23.2		. 024	1.0!	113.8	5287.	
27242.75	-4.01		5438.	22.41		The second secon	1.31	111.7	5101.	
27243.75	-2.99		5246.	21.5	7 739		1.53	109.6	4920.	
27244.75	-2.8		5056.	20.9		026	1.65	.108.0	4741.	
27245.75	-3.19		4870.	20.3			1.82	106.3	4565.	
27246.75	-3.49		4686.	THE RESERVE AND ADDRESS OF THE PARTY.			2.11	104.3	4392.	
27247.75	-3.05		45 07.				2.37	102.3	4223.	
27248.75	-3.42		4330.			062	2.62	100.7	4056.	
27249.75	-3.1		4157.				2.93	98.6	3893.	16.34
27250.75	-3.4		3986.			071	3.24	96.8	3732.	
27251.75	-2.5		3820.			035	3.40	94.9	3576.	
27252.75	-3.9		3655.				3.82	93.1	3421.	
27253.75	-3.1		3495.				4.18	90.9	3270.	13.91
27254.75	-3.0		3338.	E 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		064	4.45	89.3	3122.	
27255.75	-2.7		3184.			053	4.71	87.7	2977.	
27256.75	-2.9		3032.	and the same of the late of the		062	4.96	86.0	2835.	
27257.75	-2.9		2884.	The second second second			5.25	84.3	2695.	
27258.75	-3.2		2738.		The second second second	the second secon	5.57	82.6	2558.	
27259.75	-2.7		2596.				5.86	80.8	2424.	
27260.75	-3.4		2456.	the second of the second			6.21	79.0	2293.	
27261.75	-2.8		2320.				6.54	77.1	2165.	
27262.75	-2.2		2187		A CONTRACTOR OF THE PARTY OF TH		6.74	75.6	2040.	
27262.85	-2.2		24 74	10.3			6.74	75.5	2027.	9.59

STAND HET		TEST WGT	p	RESS	ALT	TEMP	HIND	VEL		DIREC
34000.LBS		34300. LBS	27	.593 I	N HG	23. 9 C	1.7	KTS	180.0	DEG MAG
= ( =  V =   =	44	Called	ТЕ	ST DAY		and the same		ST	NDARD	DAY
TOD	ACCEL	GNO-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
	-4.45	143.8	7654.	31.41		0.000	0.00	138.9	7035.	29.02
	-4.38	142.0		30.62		0.000	0.01	137.1	6855.	28.28
29292.25	-4.90	138.9	7174.	29.28		.040	.17	134.0	6633.	27.04
29293.25	-3.75		6942.	28.28		0.000	.19	131.7	6417.	26.10
29294.25	-4.46	134.0	6713.	27.26		.030	.25	129.3	6203.	25.15
	-4.34	131.4	6489.	26.21			.45	126.7	5994.	24.18
29296.25	-3.73	129.1	6270.	25.29			.45	124.5	5790.	23.32
29297.25	-4.19		£053.	24.38		. 037	.55	122.2	5588.	22.47
29298.25	-4.22		5842.	23.44			.75	119.8	5391.	21.60
29299.25	-3.42		5634.	22.64		. 011	.82	117.7	5197.	20.85
29300.25	-4.16		5430.	21.75		. 055	1.01	115.3	5007.	50.05
29301.25	-3.18		5230.	21.09	222.	.010	1.07	113.6	4821.	19.41
29302.25	-4.23		5032.	20.21	1543.	. 069	1.31	111.2	4637.	
29303.25	-3.52		4840.	19.48		. 038	1.49	109.1	4458.	17.91
29304.25	-3.33		4651.	18.71			1.67	106.9	4282.	17.19
29305.25	-3.34		4465.	18.21			1.77	105.4	4110.	
29306.25	-3.50		4282.	17.39		. 053	2.03	102.9	3940.	15.94
29307.25	-3.28		4103.	16.85			2.17	101.4	3774.	
29308.25	-3.02		3927.	16.16			2.39	99.3	361.0 .	14.83
29309.25	-3.37		3755.	15.69		.059	2.55	97.7	3450.	14.35
29310.25	-2.95		35 85.	15.00	The second second second	The second second	2.75	95.6	3293.	13.76
29311.25	-3.41		3419.	14.46			3.01	93.8	3139.	13.25
29312.25	-3.53		3256.	13.8		.077	3.31	91.7	2987.	12.66
29313.25	-3.20		30 97	13.25		100 A 20 Call 9	3.50	89.8	2840.	12.13
29314.25	-3.47		2940.	12.7			3.85	87.9	2695.	11.62
29315.25	-3.52	83.4	27 88.	12.1	3 2068	. 088	4.15	85.8	2554.	
29316.25	-3.44	100 000	2639.	11.5			4.43	83.7	2416.	10.55
29317.25	-3.83	and the second second	2493.	11.0			4.75	81.9	2281.	
29318.25	-3.95		2351.	10.37			5.22	79.3	2149.	
29319.25	-2.94		2213.	9.9		. 076	5.48	77.7	2022.	9.08
29320.25	-3.52		2078.	9.4			5.81	75.5	1897.	8.57
29321.25	-3.73		1947.	8.9		100000000000000000000000000000000000000	6.13	73.7	1776.	8.18
29322.25	-3.31		1819.	8.4			6.49	71.4	1658.	7.66
29323.25	-3.13		1695.	8.0			6.73	69.8	1543.	7.33
29324.25	-3.83		1574.	7.5		A COUNTY OF THE PARTY OF THE PARTY.	7.13	67.6	1431.	6.88
29325.25	-3.87		1456.	7.1			7.48	65.4	1323.	6.44
29326.25	-3.86		1343.	6.6			7.85	63.1	1219.	
TINE REPORT	-4.21		1233.	6.1			8.24	60.8	1118.	
29327.25	-3.28	THE RESERVE AND ADDRESS.	1127.	5.7		- A-198 1 ST	8.57	58.6	1021.	e i e me de la la
29328.25	-2.88	3.7.4	1107.	5.6	2 2 2 2 2 2 2		8.57	58.2	1002.	

TEST NO.	62A	MA	ARK II A	NTISKID	OUNLOP	TIRES/W	ET RUNW	AY		
STAND WG	T -	TEST WG1	ГР	RESS AL	_T	TEMP	WIND		WIND	DIREC
43000 LBS		2900 LBS		.489 IN	HG 1	6.1 C	4.5	KTS	209.0	DEG MAG
		A RECORD OF THE RESIDENCE OF						STA	NDARD D	AY
			TE	ST DAY-		1100	EBR · ·		DIST	KE
TOD	ACCEL		DIST		- FBR	UBR	0.00	146.8	9771.	41.04
23984.50	-3.81	152.6	10484.	44.23	0.	*000	0.00	144.4	9524	39.71
23985.50	-3.73	150.2	10228.	42.83	0.	*000	0.00	142.6	9283	38.71
23986.50	-3.59	148.3	9976.	41.78	0.	*000	.04	140.3	9044.	37.46
23987.50	-3.79	146.0	9728.	40.47	116.	.005	.05	138.2	8810.	36.37
23988.50	-3.62	143.9	9484.	39.33	67.	.003		135.8	8577	35.09
23989.50	-3.87	141.4	9242.	37.99	533.	.021	•19	133.8	8350	34.10
23990.50	-3.33	139.5	9005.	36.95	0.	#000	.21	131.8	8126.	33.05
23991.50	~-4.02	137.4	8771.	35.85		.038	•33	129.4	7905.	31.87
23992.50	-3.14	135.0	8542.	34.61	0.	*000	•46	127.8	7689	31.08
23993.50	-3.46	133.4	8315.	33.78	522.	.019	•49	125.5	7475	30.00
23994.50	-3.55	131.1	8092.	32.65	803.	.028	•68	123.5	7264.	29.03
23995.50	-3.56	129.0	- 7 <del>9</del> 72.		935.	034	.85	121.5	7058	28.12
23996.50	-3.23	127.1	7656.	30.66		.022	1.01 1.14	119.7	6855	27.28
23997.50	-3.20	125.2	7443.	29.78	709.	.025	1.28	117.8	6655.	26.43
23998.50	-3.05	123.3	7233.	28.88	630.	.022		116.2	6458	25.70
23999.50	-3.02	121.7	7026.	28.11	758.	.025	1.40	114.3	6264	24.88
24000.50	-3.29	119.8	68231	27.25	1290.	.043	1.62	112.4	6073	24.03
24001.50	-3.12	117.8	6622.	26.35	1210.	.039	1.88	110.8	5886	23.36
24002.50	-2.65	116.2	6425	25.64	687•	.022	2.04	109.3	5703.	22.75
24003.50	-2.73	114.7	6230		874		2.17	107.4	5520.	21.97
24004.50	-2.98	112.8	6038.	24.18	1307.	.042	-2.62	105.0	- 5341.	
24005.50	-2.68	111.3	5B49•	23.51	1010.	.032	2.85	104.2	5165	20.67
24006.50	-2.78	109.6	5663.	22.79	1235.	.038		102.5	4992.	19.99
24007.50	-2.89	107.8	5479.	22.08	1486.	•046	3.11	100.9	4822.	19.38
24008.50	-2.44	106.2	5299.	21.43	954	.030	3.32	99.4	4654	
24009.50	-2.79	104.7		- 20.83	1492.	0.36	3.78	97.8-	4489.	18.22
24010.50	-2.46	103.1	4945.	20.20	1155.	.035	3.96		4327.	
24011.50	-2.46	101.8	4772.		1189.	.037		94.9	4167.	17.14
24012.50	-2.54	100.2	4502.	19.05	1388	•042	4.21 4.43	93.5	4010.	
24013.50	-2.42	98.7	4434.	18.52		.039	4.72	91.9	3855.	16.06
24014.50	-2.81	97.1	4268.	17.91	1885.	.058	4-97	90.4	- 3703.	
24015.50	-2.44	95.6	4106.	17.37	1459		-	88.8	3553.	
24016,50	-2.73	94.0	3945.	16.78	1917.	.059	5.26 5.50	87.4	3407	
24017.50	-2.31	92.6	3788.	16.29	1435.	•042	5.73	86.0	3263.	
24018.50	-2.43	91.2	3633.	15.81	1648	.050	5.73	84.5		
24019.50	-2.61		3480.		1942		6.02	83.1	2981.	
24020.50	-2.86	88.3	3330.	14.79	2353.	.070			- 2843	
24021-50	3.04	86.3	3182.	14.14	2656	•080·	7.05	79.6	2709.	
24022.50	-2.68	84.7	3038.	13.62	2243.	.067	7.38	78.0	2578	
24023.50	-2.88		2896.	13.13	2559.	.078	7.73	76.3	2449	
24024.50			2758.	12.58	2438	.073	7.97	74.7	2323	
24025.50		79.8	2621.	12.09	2092•	•063	1 6 7 1	1701		

TEST NO. 628	MAR	RK II A	VIISKID/	DUNLOP	TIRES/W	ET RUNWA	A.A.		
STAND WGT 38000.LBS		-		•	TEMP	MIND	VEL	WIND	DIREC
STAND WGT	TEST WGT	-P1	RESS AL	1 1	1 E M C	3.2	KTS	218.9	DEG MAG
38000.LBS	38350.LBS	27	. 485 IN	MG 1	· • 1 0	012	1,10		
TOD ACCEL 26296.16 -4.63	GNU-SPU	01.03	76.55	0.	0.000	0.00	141.1	8729.	33.50
26296.16 -4.63 26297.00 -3.89	140.7	3433 .	30002		4 306	0 00	479 0	-8534- "	-32-46
26297.00 -3.89	144.5 142.2 140.0	9207	30.44	0.	0.000	0.00	136.6	8306.	31.40
26298.00 -3.81	14202	90474	37.07	-0.	0.000	-0.00	134.5	8082.	30.43
26299.00 -3.99	137.7	2573.	32-18	0.	0.000	0.00	132.2	7862.	29,40
26300.00 -3.70	135.4	8342	32.18 31.14 30.14 29.11 28.23	252.	.013	.02	130.0	7644.	28,43
26301.00 -4.04	133.2	8115.	30-14	0.	0.000	.04	127.9	7432.	27.50
26302.00 <b>-</b> 3.68 26303.00 <b>-</b> 3.52	131.0	7893	29.11	0	0.000	.05	125.6	7222.	26.54
	129.0	7673	28.23	٥.	0.300	.05	123.6	7016.	25.72
26304.00 -3.42 26305.00 -3.61	126.8	7457	27.28	344.	.016	12	121.5 "	6813.	24.83
	124.8	7245	25.44	343.	.016	.17	119.5	6614.	24.05
26306.00 -3.51 26307.00 -3.17	127.6	7036	26.44 25.53	- 68.	003	.24	117.4	-6418	23.20
26307.00 -3.14	121.0	6830	24.85	174.	.008	. 25	115.8	6226	22.56
26307.00 -3.17 26308.00 -3.14 26309.00 -3.54 26310.00 -2.41 26311.00 -3.61	118-9	6628	24.00	778.	035	.39-	113.8	-6036.	21.77
26340.00 =2.41	117.1	6429.	23.27	0.	0.000	• 43	112.0	5851.	21.09
26344-0003-61	-115-4	6232	22.60	1071 ·	048	-53	110-3-	5667	20.46
26312.00 -3.05	113.3	6040 .	21.78	521.	.023	•69	108.2	5486	19.70
									19-12
26313.00 -3.15 26314.00 -3.07 26315.00 -2.76	109.8	5663.	2û.45	764.	.033	• 93	104.8	5135.	18.40
26345-00 2-76	10.8-1	-5479	19-84	48 <del>6 •</del>	-021	1.02	-193-1-	4965	17.09
26316.00 -2.93	106.6								
26-317-002-71	4 10 44 - 8		40 07	C.4.C	N.2£	1.24	999	4031.	16.77
26318.00 =3.13	103.2	4944 .	18.09 -17.39	1197.	• 050	1.38	98.4	4400	15.62
26349-002-71	-101.2	4773.	17.39	814.	0.33	1.58	95-4	43000	15.15
26320.00 -2.92	99.7	4603.							
26320.00 -2.92 26321.00 -2.40	98.0	4436	16.88 16.31	602.	024-	1.087	91.8	2877 - 3220 *	14.17
			15.82	1132.	.045	2.06	91.0	2605	1-3-69-
		4110 .	15.31	7.51		2 07	90.2	751.0	13.34
26324.00 -2.43	93.8	3951.	14.92	830 •	•033	2.27	97.4	347¢	- 12-76
26323.00 -2.40 26324.00 -2.40 26325.00 -3.20	91.8	3794.	-14.30	1870		2 (0	07 • T	3263.	12.38
26325.00 -3.20 26326.00 -2.10 <del>26327.00 -3</del> .20	90.4	3641.	13.89	735.	.029	2.09	07. A	3422	1184
26327.00-3.24	+	3489	·····1·3· 3·1···	2000	0 / 4	7 47	82.3	2986.	11.41
26328.00 -2.33	86.9	3341.	.12.83	10/1•	.041	3 34	84.2-	- 2953	11-09-
26329.00 -2.3	2 85.8	31 <del>-96</del>	12.50	1-347	0.53	7 57	79.5	2721.	10.64
26330.00 -2.6	7 84.1	3052.	12.00	1595.	# U D C	7. 76-	7.8. A	2592	- 18-24
26331.00 2.6	4 82.5	2911	11.57	1620		3 05	76.7	2466	9.89
26332.00 -2.4	3 81.2	2773.	11.19	1440	079		75.8	- 2342.	9.45
26330.00 -2.6 26331.00 -2.6 26332.00 -2.4 26333.00 -2.9	79.4	~ 2638 •	10.72	4746	.064	4.45	73.5	2220	9.09
26334.00 -2.5	4 1010	2000				4.69	71.9	2101.	
26335.00 -2.5	8 76.3	2374 •	9.89	1822. 2046.		4.92	70.5	1985.	_
26336.00 -2.7		2247	9.53			5.21	68 . 8	1871.	
26337.00 -2.9		2122.	9.09	2372		5.49	67.1	1760.	
26338.00 -2.7	_	2000.	B • 67	2202		5.72	65.7	1652.	
26339.00 -2.4		1881 •	8.32	1941.		5.99	64.1	1546.	
26340.00 +2.8		1764	7.94	2404. 1911.		6.08	63.1		
26340.61 -2.3	6 67.4	1694.	7.70	T 2TT #	1300				

TEST NO	O. 63A	MARK	II-ANTISK	10/00	NLOP TIRES/	WET	RUNWA	Y
STAND	WGT	TEST WGT	PRESS	ALT	TEMP		WIND	VEL

								1
	TEST WGT	PRESS	ALT		MIND		WIND	DIREC
40000.LBS	40300.LBS	27.440	IN HG	15.0 C	7.4		200.0	DEG MAG
· ·		TEST D/	.v	. = 1 - 1			TANDARD !	
TOD ACC			FBR				DIST	
24234.87 -4.5		231. 41.4		0.000	0.00			36.55
24235.75 -3.4		006. 40.2		0.000			8874	
24236.75 -3.4		755 39.0		0.000	6.00	139.3		34.36
4237.75 -3.		507. 37.6					8407.	
4238.75 -4.		263. 36.6				134.7		32.11
4239.753		123. 35.6						
4240.75 -4.		786. 34.4			.24	130.4		30.10
4241 75 -2		554 - 33-4			29			
4242.75 -3.0		324. 32.5			• 32	126.5		28.32
4243.75 -3.1			8 - 587				7098.	
4244.75 -3.		875. 30.5			.51	122.4		26.51
4245.75 3.4		656 - 29 6	8 605				6691.	
4246.75 -3.		440 . 28.7		.016	.71	118.5		24.86
4247.75 -3.		227 27.	368	014-				-24.15
4248.75 -2.		118. 27.0			. 87	114.8		23.35
4249.75 -3.	39 121.6 6	811 - 26 -						22.70
4250.75 -2.0		508 25 5			1.14	111.2		21.91
4251.75 -2.0		407 . 24 . 9	278	010-	116	109.9	5547-	21.37
24252.75 -3.0		209. 24.2			1.28	108.3		20.76
24253.75 3.1								20.03
4254.75 -2.7		822 - 22 - 7			1.64	104.7		19.42
4255.75 -2.1	15 111.3 50	632. 22.1	- 60		-1.71	103.1	4842.	18.82
4256.75 -3.		445. 21.6	2 1377	.051	1.83	101.9	4675.	18.38
4257.75 -2.		262. 20.8				100.1	4508.	- 17.73
4258.75 -2.5		080 - 20 - 2	21 1300	-047	2.27	98.3	4343.	17.11
4259.75 2.3	37 105.0 4°	902. 19.6	5 - 853	.028	2-43	96.8	41.83	- 16.60
4260.75 -2.4	48 103.5 4	726. 19.1	LO 893	.032	2.58	95.4	4026.	16.11
4261.75 -2.5	51 102.2 4	552. 18.6	2 992	035	2.7.	94.1	3871	15.67
4262.75 -3.	1 100.3 4	381. 17.9	1690	.051	2.93	92.2	3716.	15.06
4263.75 -1.4	99.0 48	21317.5	50 450		-3-12	91.0	- 3568.	14.66
24264.75 -2.6		17.0	3 - 1411	.050	3.28	89.7		14.23
24265.75 -2-	75 95.9 31	884. 16.4	1- 1565		3.55	- 87-9	3274	13.69
4266.75 -2.4	94.5 37	723. 15.9			3.76	86.5	3132.	13.25
4267.75 -2.2		565 . 15.4	1051	0-37	- 3-96	- 85.0	2992.	12.79
24268.75 -2.1	2 91.8 3	489. 15.0			4.07	83.8		12.44
24268.77 -2.0	11 91.8 34	486. 15.0	2 831	030	4.07	-83.8	-2853	12.44

TEST	10. 633	МА	RK II	ANTISK	ID/DUNLOP	TIRES/	WET RUNI	HAY	
STAND	WG T	TEST WGT		PRESS	A1 T	TEMP-	WTM	}4/E/	WIND DIPE-C
36000.	LBS	36350.LBS	ä	27.440	IN HG	17.9 C	9.4	KTS	WIND DIRECT 195.0 DEG MAG
_				TEST DA	Y			ST	ANDARD DAY
	ACCE	E GND=250	DIST	KE	FBR	U3R	EBR	KTAS	DIST KE-
26615.	10 -4.1	6 149.5	9368	35.9	an.	0 - 00 0	0 00	478.5	8027 70 57
26616	00 -3.8	5147:4	-9142	34-9	5 0 •	0.000	0.00	136.4	<del>7821 29.65</del>
26617.	00 -4.0	4 145.2	8895	33.9	5 0.	0.300	0.00	134.3	7598 28.74 -7375 27.66
26618	00 -3.8	3~ 142.6	8653.	32.7	4 ·	-0-000-	-02	-131-7-	7375 27-66
26519.	00 -3.9	3 140.4	8413.	31.7	150.	•007	.03	129.5	7158. 26.73 -6945. 25.81
26620.	00 -4.0	1 138.1	8178	30.6	390	019	-10	127.3-	6945. 25.81
26621	00 -3.79	5 135.7	7948.	29.65	5 247.	-112	.17	125.0	6735. 24.89
		1 - 133.6	7720	28.71	241.	011		122.8	6529. 24.04
26623.			7496	27.91	145.	.007	•23	121.0	6329. 23.33 -6130. 22.48
	00 3.7		7276	26.95	689.	•032	36	118-8-	6130 22.48
26625.	00 -3.39	127.2	7059.	26.00	3 400-	. 018	- 49	116.6	5934. 24.66
26526	003-17	7 125.4	6847	25.30	244.	-011	. 52	114-8-	5744 21 01
26627.		123.1	6637.	24.39	550.	.023	• 67	112.6	5554. 20.20
26628	00 -2.99	121.7	~643U •	23-82	2226.	-010	- 69		-5373. 19.70
26629.						.047	• 87	109.1	5198. 18.97
	003-00		6027	- 22-26	538.	-023	1.01	10772	5012 18 31
26631.			5829.	21.57	1081.	.047	1.18	105.4	4838. 17.70
26632	00 2.67	114.0	5636 e	-20.90	3-34.	015	130		4667. 17.11
26633.			5445.		1423.	•059	1.50	101.8	4497. 16.50
26534	00 -2-30	110.2	5258 ·	19.55	146.	006			4332. 15.92
26635.			5073.	19.12	966.	.040	1.71	98.8	4172. 15.54
26636		106.7			1469.	061			4009 - 14.84
26637.			4712.				2.15	95.1	3855. 14.42
26638.				-17.25		.042	2.31	93.4	37011390-
26639		– .	4362.		1224.	.351	2.54	91.6	3549. 13.38 -3402. 12.96
	0.02.07		4192.		369.	•015 ···	~2~66~~	90-2-	3402 • 12 • 96
26641.			4024.			.051	2.82	88.7	3257. 12.55
26642.			3858.		1690.	•067·	3.06	87.2-	3257. 12.55 -3115. 12.11
26643.			3696.	14.65	923.	.038	3.29	85.4	2974. 11.62 -2839. 11.31
26644	00 -2.44	94.2	3536.	14.28	1072.	043	-3.42 -	- 84 · 2	<del>-2839• -11-31</del>
26645	00 -3.13	92.1	3378.	13.66	1943.	•077	3.73	82.2	2702 10 77 2571 10 40
26646.	00-2.30	90.7	3224	13.24	1065		<del>3-, 9</del> 3	80 . 8	
26647.0		89.2	3072.	12.80	1755.	.070	4.16	79.3	2442. 10.03
26648.	002.54	87.4	2923	12-29	1-4-71		4-42-	77.5	2314. 9.58
26649.			27.77 .			.064	4.62	76.3	2192. 9.27
26650 • (	UU -2.56				1625.	- 063-			-2070 8.85-
26651.0			2492.	11.09		.062	5.08	73.3	1953. 8.56
	10 -2.86	81.4	2353	10.66	2053.	- 083-	- 5 <del>- 35</del>	71.7-	1836 - 8-19
26653.0		79.7	2217.	10.22	1795.	.069	5.61	70.0	1722. 7.81
26654.0		78.3	2084.	9.86	1795. 1772. 846.	• 867	- 5 • 8-3	68.6-	1613. 7.51
26654.8	80 -1.63	77.1	1979.	9.56	846.	.032	5.94	67.5	1526. 7.25

TEST NO. 644	AM	HK III A	TISKID	/USAF	TIRES	NET RUNWA	Y		
STAND WGT	TEST WGT	PRE	SS AL	*	TEMP	CNIW	VEL	WIND	DIREC
43000 LHS	43250.LBS		515 IN	HG :	11.6 C	0.0	KTS	0.0	DEG MAG
		TEAT	5 DV				c.T.	ANDARD C	) A V
	L GNU-SPD	DIST	KE DAY	FBR	-UBR	EBR	KTAS	ANDARD ( DIST	KE.
24859.96 -4.1			38.57	42.		00	141.2	7076.	37.95
24860.75 -3.2			37.64		0.000	.00	139.5	6891.	37.03
24861.75 -3.8			36.65		014		137.6	6660	
24862.75 -3.6			35.36	294.	.011	.15	135.2	6432.	34.79
24863.75 -3.6			34.31	478.	.018	.21	133.2	6208.	33.76
24864.75 -3.8			33.19	940.	.034	•38	131.0	5987.	32.65
24835.75 -4.0		5965.	32.05	1255.	• 046	61	128.7	-5771 •	
24866.75 -4.1	3 126.8	5649.	30.78	1581.	• 056	•95	126.1	5558.	30.29
24867.75 -3.6	2 124.7			1043.	.036	1.17	124.1	5349.	29.30
24868.75 -4.1	2 122.5		28.75	1859.	.064	1.48	121.9	5144.	28.29
24869.75 -3.9			27.55	1708.	• (tb0	1.87	119.4	1942.	27.12
24870.75 -3.8			26.59	1806.	• 060	2.18	117.2	4745	26.16
24871.75 -4.2			5.48	2640.	•0#3	2.66	114.7	4551.	25.06
24872.75 -3.8			24.39	2295	.072	3.14	112.3	4362	24.00
24873.75 -4.0			23.45	2659.	-082	3.59	110:1	4176. 3995.	23.07 22.02
24874.75 -4.2			2.38	3000.	.09K	4.1J 4.67	107.6 105.1	3817.	21.04
24875.75 -3.9 24876.75 -4.1			21.39	2802. 3242.	.086 .099	5.18	102.9	3643	20.16
24876.75 -4.3 24877.75 -3.9			9.48	3026.	.093	5.74	100.3	3474.	19.16
24878.75 -3.8			8.60	2972.	098	6.24	98.1	3308	18.30
24879.75 -4.0			7.74	3419	106	6.75		3146.	17.50
24880.75 -3.5			6.92	2849	.086	7.26	93.5	2989	16.64
24881.75 -3.7			6.12	3191.	.096	7.75	91.3	2834.	15.86
24882.75 -3.6			5.40	3369.	.103	8.23	89.2	2684.	15.15
24883.75 -3.8			4.53	3479.	.106	-8.78	86.7	2537.	14.30
24884.75 -3.9	4 85.2		3.89	3746.	-112	9.27	84.7	2393•	13.66
24885.75 -3.9	9 82.6		3.06	3915.	•11A	9.84	82.1		12.85
24886.75 -3.5			2.42	3429.	.104	10.30	80.1	2119.	12.22
24887.75 -4.1			1.70	4270.		10.84		198.7 • .	
24888.75 -3.9			0.99	4111.	.126	11.39	75.4	1859.	10.81
24889.75 -3.6			0.36	3812.		-11.87	73.2		10.19
24890.75 -4.4			9.64	4962	•151	12.44	70.6	1615.	9.49
24891.75 -3.4		1524.	9.06	3687	111	12.92	68.4	1500.	8.91 8.29
24892.75 -4.4		1410. 1300.	8.43	5079. 4349.	•153 •132	13.44 13.95	66.0 63.6	1387. 1279.	
24893.75 -3.8 24894.75 -4.2		1194.	7.81 7.21	4975.	148	14.46	61.1	1175.	7.10
24894.75 -4.2 24895.75 -3.6		1092.	6.72	4295	.129	14.90		1075.	6.62
24896.75 -4.6		994	6.15	5714.	.176	15.41	56.4	978	6.05
24897.75 -4.4		901.	5.58	5466.	-164	15.93	53.7	887.	5.49
24898.75 -4.4		812.	5.03	5580.	.167	16.42	51.0	799.	4.94
24899.75 -3.7		- 728 ·	4.58	4667.	.140	16.83	48.7	716.	4.51
24900.75 -4.8			4.12	6156.	.185	17.27	46.2	636.	4.06
24901.75 -3.5	9 43.8	571.	3.68	4594.	.137	17.67	43.6	562.	3.62
24902:75 -4.4	4 41.6	499.	3.32	5782.	.173	18.04	41.4	491.	3.26
24903.75 -4.2		431.	2.90	5549.	.164		38.7		2.85
24904.75 -3.9		368.	2.56	5186.	• 155	18.76	36.4	362.	2.52
24905.75 -4.1		308.	2.21	5537.	.164	19.08	33.8	303.	
24906.75 -4.5		252.	1.92	6135	·185	19.39	31.5	248	1.89
24907.75 -4.7		201.	1.57	6485	.194	19.72	28.4	198•	1.54
24908.75 -4.4		155.	1.31	6065.	•182	19.99	26.0	152.	1.29
24907.75 -4.8		113.	1.03	6603.	.199	20.26 20.41	23•1 20•7	111. 75.	1.02 .81
24910.75 -2.3	1 20.8	77.	.83	3296.	• 095	C V = 4 I	CV4/	131	B C 1

TEST NO. 6	<b>4</b> B	мДЕ	K III	ANTIS	KID/USAF	TIRES/W	ET RUNWA	Y		
1631 140 0	40								WIND	DIREC
STAND WGT		TEST WGT		RESS	ALT	TEMP	WIND 0.0			DEG MAG
38000.LBS	31	8150.L9S	27	•515	IN HG	16.7 C	0.0	IC13	0.0	020
								ST	ANDARD D	ΑΥ
-			TE	ST DA	Y FBR	UHR	EBR	KTAS	DIST '	KE
		GND-SPD	DIST	KE				130.9		-28.85
	-3.99	132.7	6008.	29.7			.12	129.1	5658	28.05
	-3.92	130.8	5532.	28.9			.51	126.9	5446	- 27 . 08
C . C . C	<b>-3.7</b> 1	128.6	5613.	27.9	-	-	.35	124.6	5237.	
	-3.85	126.3	5398.	26.9	-			122.5	5032	25.26
	-3.60			26.0			-68	120.2		
	-4.11	121.8	4979	25.0			1.00	117.8	- 4633 e-	23.36
	-4.37	119.4	4775.				1.33	115.3	4440.	
	-4.04	116.8	4576.	23.0		-		112.9	4250.	21.45
27274.75		114.4	4381.	22.1			2.05	110.5	4064.	20.53
	-4.55	111.9	4189.	20.2		-	2.45	107.9	3884.	-19.59
27276.75		109.4	4003.				2.84	105.6	3706.	
	-4.25	107.0	3820.	19.3			3.26	103.1	3533.	17.89
27278.75		104.5	3642	18.4			3.77	100.5	3364.	
	-4.57	101.8	3468	17.5		_	4.19	98.1-	3200-	16.18-
	-3.87	99.4	3298.	16.6 15.8			4.63	95.6	3039.	15.38
27281.75	-4.21	96.9	3132.		0. 2564		5.05	93.3	2882	14.65
27282:75		946	2971.	14.3		-	5.55	90.A	2729.	13.88
27283.75	-4.60	92.0	2813.	13.5		_		88.4	2581.	13.14
		89.6	2560	12.1			6.56	85.6	2436.	
27285.75	-4.59	86.8	2511.						2296.	11.66
_,	-4.03	84.4	2367.	12.0			7.47	81.0	2160.	11.03
27287.75	-3.86	82.0	2226	10.		137	7.95		- 2027 •	10.39
	-4.35	79.6	2090.	10.			8.43	76.1	1900.	
27289.75	-3.99	77.1	1958	9.4			8.87	73.7	- 1775 •	
	-3.90	74.7	1530. 1706.	B. €			9.26	71.5	1655.	8.60
27291.75	-3.44	72.4		8.			9.66	69.4	1537•	B:11
27292.75	-3.97	70.4	1585. 1468.	7.0			10.09	67.2	1424.	
27293.75	-4.02	68.1		7.		-	10.56	64.6	1315.	
27294.75	-4.22	65.4	1355• 1247•	6.			10.97	62.4	1209.	6.55
27295.75	-4.09	63.2	1142.	6.			11.46	59.6	1108.	
	4.63	60.4	1042	5.		-	11.86	57.3	1011.	
27297.75	<b>-3.65</b>	58.0	946.		-	-	12.21	55.1	918.	
27298.75	-3.54	55.8 53.7	953.	_		-	12.62	53.0	828.	
27299.75	-4.87	-50.4	766		-	176	13.09	49.7	743.	
27300.75		48.0	582				13.48	47.3	662•	
27301.75	-4.48	· 45.3	-504.			-	- 13.86	44.7	586•	3.37
		42.9	529.				14.22	42.3	513.	
27303.75	-4.69			2.			14.59	39.5	446.	2.62
27304.75		27 4	394	_			14.91	37.1	382•	
27305.75	-4.67	37.6 34.6	333.				15.25	34.2	323•	
27306.75	-4.71 -5.10	31.8	277.				15.57	31.4	269.	
27307.75	-5.10	28.6	226				15.87	28.2	219.	
	-5.14		180.				16.15	25.4		
27309.75	-5.05 -4.68	22.7	139.		87 5693		16.38	22.4		
27310.75	-4.68 -2.97	20.2	103.		69 370		16.53	.50 • 0	100.	
27311.75 27311.91			98		68 -320		16.53	19.7	95•	•66
2/317.91	-6.36	2000		·						

TEST NO. 6	54C	ААМ	RK III A	ANTISKI	DIUSAF	TIRES/WE	T RUNWA	Y		y ny orana Menericana di
1231 1101			*				MIND		WİND	DIREC
STAND WG	r	TEST WGT	. Pr		LT	TEMP	- 00	KTS	0.0	DEG MAG
34000.LRS		34350.LBS	27	.515 IN	нь	19.4 C	0.0			
			TEIS	-T 04V-				ST/	ANDARD [	AY
•				KE	FBR	UBR	EBR :	KTAS .	DIST	, KE, ==
TOD		GND-SPD	DIST	24.55	331.	-019	-01	124.4	5367.	23.30
29362.90	-4.11	127.1	5554	23.73	375.	.021	.10	122.3	5195.	22.52
29363.75	-4.01	124.9	5474.	22.79	603.	.033		119.9	4997.	21.63
29364.75	-4.09	122.4	5264. 5059.	21.98	512.	.027	31	117.7	4802.	20.86
29365.75	-3.86	120.2	4959	21.17	190.	-010	.38		4612	20.10
29366.75	-3.43		4561.	20.44	724.	037	.47	113.5	4424	19.40
29367.75	-3.82	115.9	4468.		- 727.	036	- 62	111.2	-4241	18:62
29368.75	-3.69	113.6 111.4	4278.	18.88	811.	.040	.77	109.1	4060	17.92
29369.75	-3.65 -4.29	109.1	4091.	18.12	1630.	- /• 081	1.01	106.9		17.19
29370.75	-4.28	106.6	3909.	17.27	1780.		1.32	104.4	3710.	16.39
29371.75	-4.04	-104.1	3731.	16.47	1661.	080	4.63	101.9	3542 •	15.63
29372.75	-4.19	101.8	3557.	15.77	1941.	.093	1.92	99.7.	3377	14.97
29 <b>373.7</b> 5 29 <b>374.7</b> 5	-4.31	99.2	3388.	14.97	2206.	.104	. S*S8	97.2	3216.	13.46
29375.75	-4.11	96.6	3273.	14.18	21,34.		2.66	94.6	3059	12.89
29376.75	-3.15	_	3061.	13.58	1200.	5.0	2.89	92.6	2906	12.38
29377.75	-3.65	-	2903.	13.04	1845.		3.13	90.7	2609	
29378.75	-4.24		2749.	12.42	~2576.		- 3.47	88.5	2467	
29379.75	-4.06		2599.	11.66	2510.		3.89	- 85.8	2328	10.59
29380.75	-3.41		2453.	11.46		086	4.10	83.9	2192.	
29381.75	-4.54		2310.	10.50	3229.	. 144	4.57	81.4	2062	9.41-
29382.75	-3.92		21-72.	9.91		119	4.96	79.1 76.5	1934	
29383.75	-4.26		2038.	9.29	3136	• 141	5.36	74.2	1911	8.29
29384.75	-4.00		1908.		5965		5.75	72.1	1691	
29385.75	-3.87	73.6	1782.	8.23	2909		6.11 6.53	-69.5	1575	. : -,7.27
29386.75	-4.47	71.0	1660.	7.66	3658		6.89	67.2	1464.	
29387.75	-3.68	68.6	1542.	7.16	2904		7.29	64.6	1356	
29388.75	-4.24	66.0	1428.	6.62	3595		7.59	62.8	1251	
29389.75	-3.38		1318.	6.25	2740		7.94	60.6	-1151	
29390.75	-4.19		1212.	5.82	- 3667		8.37	57.9	1053	_ ,
29391.75	-4.86	59.1	1110.	5.32	4419. 3251			55.3	961	4.60
29392.75	-3.63		1013.	-4.85 4.50	3796		9.05	53.3	872	
29393.75	-4.08		919.	4.07	3872		9.41	. 50.7	787	-3.86
29394.75	-4.07		529. 744.	3.74	3722		9.72	48.5	706	
29395.75	-3.89		_	-3.36		166-		46.1		
29396.75	4.17		585.	3.04	3750	. 151	10.35	43.8	555	2.89
29397.75	-3.78		512.	2-75	3924	-150	10.62	- 41.7-		2.61
29398.75	-3.90		442.	2.40			10.94	38.9	419	2.28
29399.75	-4.65		377.				-11-24	36.4	-357	1-99
29400.75	-4.32		316.	1.84	4199		11.49	34.1	300	
29401.75	-3.99		259.	1.57			11.76	-31.4		149.
29402.75	-4.9		208.	1.29		-	12.02	28.5	197	
29403.75	-4.3°		161.	1.09	_		12.23	26.2	152	
29404.75	-4.2		118.	87		. 505	12.44	23.4	112	
29405.75	-4.77		80.	.70			12.58	21.1	7.6	
29406.75	-2.5t		73.	-69			12.58	20.9	69	
29406.95	-1.8	0 6100		-	**					and the second s

TEST NO. 654 MARK III ANTISKID/STANDARD TIRES/HET RUNWAY (WATER ONLY)

STAND W	GT	TEST WGT	r	PRESS	,	TEMP	MINO	VEL	UTHE	DTD #0
43000 LB	S	42500.LBS	27	.534 T	и нь	10.6 0	4.0	V CL	MIND	DIREC DEG MAG
	1	4		- di		1010 0	4.0	K12	U . U	UEG MAG
				ST DAY				ST	AND ARD	1AV
1.00	. A COLL	GNU-5PD	DIST	KE	FBR	UBR	EBR.	KTAS.	TOTO	KE
24125.95	- 4. 33	417 5	7756	1.0 05	-			148.4	7526	
24126.75	-4.19	145.6 143.1 143.8 138.3	7158.	39.86	9.	0.000	0.06	146.4	7.324.	40.79
24127.75	- 3.79	143.1	6915.	38.52	3 -	0.000	. 0.06	143.9	7075	39.41
24128.75	-4,53	140.8	6674.	37.29	383	.019	.02	141.6	6.829.	
24129.75	-3.46	138.3	6440.	35.97	0.	0.000	. 6 9	139.0	6589	36.80
C 4T 20 E 1 2	-4043	130.2	6207.	34.88	1289.	046	ુ• 2 ટ	136.9		35.69
24131.75	-4.07	133.5	5980.	33.53	955.	.034		134.3	6119.	34.31
24132.75	1-4.31	131.2	5757.	32.37	1440 .	051	.74	131.9	5893.	33.12
24133.75			5538.	31.97	1105.	.039		129.2	5666	31.79
24134.75		126.4	5322.		1945	068	1.33	127.1	5446	30.74
24135.75	-4.54	123.2	5112.	28.57	2252	677	1.87	123.9	5230.	29.23
24136.75	-3.92		4905.	27.55	4683	-056	2.21	121.7	5019.	28.19
24137.75	-4.01	118.5	4703.	26.43	2063	065	2.60	119.2	4812.	27.05
24138.75	4.34	115.3	4505.	25.43	2645	.081	3.04	116.9	4609.	26. 02
24139.75	-3.94	113.8	4311.	24.37	2645 · 2274 ·	.068	3.51	114.5	4411.	24.94
24140.75	-3.75	111.5	4121.	23.37	2152 .	1066			4217	23.91
24141.75	-4.74		3935.	22.49	3575 .	.111	4.45	109.7	4026	22.92
24142.75	-3.84	456.7	77 57	24 26	0007			106.0	3840.	
24143.75 24144.75 24145.75	-3.88	104.4	3575.	20.49	2710.	.081	5.44	105.0	3658.	20.97
24144,75	-4.28	101.7	3401.	19.44	3350.	103	6.02			40 90
24145.75	-4.15	99.0	3232.	18.46	3320 -	.100	6.60	99.6	3480.	18.89
24146.75	-4.33	96.6	3066.	17.56	3682.	. 110	7.17	07 1		17.96
24147.75	-4.11	94.1	2905.	16.65	3491 •	106	7.75	~94.6	2973.	
24148.75	-4,34	91.6	2748.	15.79		. 118	8.33	92.1	2812.	17.03
24149.75	-3.53	89:4	2596.	15.05	2949	.087	8-81	35.1	2014	16.16
24150.75	-4.28	87.0	2446.		4 0 39 .	-128	8.81 9.36 9.93	97 5	2507	15.40
24151.75	-4.48	84.6		13.47	4394	.131	9.95	95 4	22036	14.50
24152.75	-3.64	82.1	2162.	12.60	3389	. 181	10.49	82.6	2212.	
24153.75 24154.75	- 3.84	79.7	2025.	11.94	3750.	112	11.00	80.1	2072	12.99 12.22
24154.75	-3.58	77.8	1592.	11.39	3608.	.108	11.44	78.2		
24155.75	-4.41	12.2	1762.	10.65	4676 .	,137	12.01	75.7	1935.	11.65
24156.75		72.9	1638.	9.99	3756.		12.51	73.3	1803. 1676.	10.90
24157.75	-4.73	70.6	1516.	9.37	5254	.158	13.05	71.0	1551.	10.22
24158.75	-4.83	67.8		8.64	5485	.163	13.67	68.2	1432.	9.58
24159.75	-4:45	64.8	1288.		5075.	.153	14.27	65.2	1313.	8.85
	-3.78		1181.	7.33	4272 .	.127	14.73	62.8	1208.	8.08
24161.75	-4.26	60.1	1977.	6.80	4970	. 150	15.22	60.4		7.50
	-4.85	57.4	978-	5.20	5822.	.177	15.7€	57.7	1102. 1001.	6.96
24163.75	-4.39	54.5	883.		5306	. 158		54.8		
	-3.21	52.5	793.	5.18	3804.	.113	16.29 16.68	52.8	904.	
24165.75	-4.95	58.2		4.74		. 184	17.15	50.5	812.	5.30 4.85
24166.75	-4.98	46.9	625.	4.14	6286.	.185	17.62	47.2	723.	
24167.75	-5.51	44.1	547.	3.66	7048	. 210	18.11	44.3	639.	4 . 24 .
24168.75	-4.97	43.7	476.	3.12	6410	191	18.59		560.	3.74
	-4.52	38.1	469.	2.73	5998	. 180	18.98	40.9 38.3	487.	3.19
24176.75	-4.95	35.2	347.	2.34	6498.	192	19.37	35,4	419.	2.80
	-4.43	32.4	290.	1.97	5860	.174	19.71	32.6	355.	2.39
	-4.03	30.0	237.	1.70	5368.	. 161	19.95	36.2	297.	2.02
24173.75	-5.35	27.3.	189.	1.40	7149.	.218	20.30	27.4	243.	1.74
24174,75	-5.13	24.1	145		6916	207	20.65	24.2	193.	1.43
24175.75	-4.7:4	21.1	107.	-83	6459	186	20.85	21.2	148.	1.11
24176.55	-1.88	19.3	80.	.70	2708	. C78	20.93	19.4	169.	• 85 73
		•					50 0 0,5	1204	82.	•72

TEST NO. 658 MARK III ANTISKID/STANDARD TIRES/WET RUNWAY (WATER ONLY)

STAND WGT TEST WGT PRESS ALT TEMP WIND VEL	WIND DIREC
38000.LBS 38500.LBS 27.535 IN HG 12.4 C 4.0 KTS	0.0 DEG MAG
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DARD DAY
	DIST KE
	33.28
	32.29
	5812. 31.09
	5590. 30.09
	371. 29.20
	28.06
	+945. 27.04
	4738. 25.96
	4535. 24.96
	336. 23.98
	4141. 23.02
	3951. 21.80
	3765. 20.86
	3584. 19.70
	3407. 18.86
	3234. 18.06
	3066. 16.93
25968.50 -4.20 99.1 2999. 16.75 2861099 5.23 98.2	2902. 16.21
25969.50 -4.33 96.3 2834. 15.79 3146108 5.75 95.3	2743. 15.28
25970.50 -4.33 94.0 2673. 15.07 3251114 6.23 93.1 3	2587. 14.58
	2436. 13.83
25972.50 -4.11 89.5 2365. 13.66 3217106 7.07 88.6	2288. 13.22
25973.50 -4.84 86.6 2216. 12.79 4197144 7.67 85.8	2144. 12.38
	2005. 11.63
	1870. 10.92
25976.50 -4.42 79.0 1796. 10.63 3995136 9.23 78.2	1738. 10.2 <del>8</del>
25977.50 -4.46 76.4 1666. 9.95 4150138 9.75 75.7	1612. 9.63
	1489. 8.90
	1371. 8.44
25980.50 -4.48 65.3 1298. 7.95 4451151 11:29 67.6 1	1256. 7.69
25981.50 -4.36 66.3 1185. 7.48 4385145 11.75 65.6	1146. 7.24
	1041. 6.62
25983.50 -5.15 61.0 970. 6.34 5490185 12.71 60.4	939. 6.13
25984.50 -4.38 57.9 87G. 5.71 467G153 13.22 57.3	842. 5.53
25985.50 -4.92 55.6 774. 5.28 5370180 13.68 55.1	749. 5.10
25986.50 -4.93 52.4 684. 4.67 5481180 14.18 51.9	662. 4.52
25987.50 -4.95 49.4 597. 4.15 5575186 14.66 48.9	578. 4.02
25988.50 -5.09 46.7 516. 3.71 5618. 190 15.10 46.2	500. 3.59
25989.50 -5.93 43.2 441. 3.17 6885235 15.60 42.7	427. 3.67
25990.50 -4.95 39.9 371. 2.71 5799191 16.03 39.5	359. 2.62
25991.50 -5.45 36.9 306. 2.32 6459. 212 16.42 36.6	295. 2.25
25992.50 -5.87 33.5 246. 1.92 7012238 16.81 33.2	238. 1.85
25993.50 -5.80 30.1 193. 1.54 6983240 17.18 29.8	187. 1.49
25994.50 -5.27 26.5 145. 1.20 6404220 17.51 26.3	140. 1.16
25995.16 -2.82 24.8 117. 1.05 3499120 17.59 24.5	113. 1.01

TEST NO. 650 MARK III ANTISKIO/STANDARD TIRES/HET RUNHAY (HATER ONLY)

TOD	STAND WGT	TEST_WGT	P	RESS AL	LT	TEMP	WIND	VEL	HIND	DIREC
TOD	3/AND FOI			535 IN			0.0	KTS	0.0	DEG MAG
TOO ACCEL GND-SPD DIST KE	340001113	342001633							a Library	
TOO ACCEL GND-SPD DIST KE F9R UBR EAR KTAS DIST KE 2770F.06 -4.27 132.6 5748, 26.83 249, 012 01 130.7 550.8 25.72 2770F.00 -3.84 128.0 5321. 25.01 78. 004 04 126.2 5100. 23.97 27710.00 -4.08 128.8 5107. 24.19 480. 023 01 128.5 5308. 24.85 27711.00 -3.76 123.3 4897. 23.22 290. 014 15 124.6 4693. 22.25 27712.00 -4.01 121.0 4691. 22.37 727. 034 .25 119.4 4494. 23.18 27711.00 -3.76 123.3 4897. 23.22 290. 014 15 124.6 4693. 22.25 27712.00 -4.01 121.0 4691. 22.37 727. 034 .25 119.4 4495. 21.44 27713.00 -3.87 118.6 488. 21.50 709. 033 .44 117.0 4301. 20.60 27714.06 -4.89 116.2 4290. 20.63 1971. 091 .71 114.6 4111. 19.77 27715.00 -3.93 111.0 35 77. 18.83 1455. 059 1.00 114.8 3926. 18.80 27715.00 -3.93 111.0 35 77. 18.83 1455. 059 1.00 114.8 3926. 18.80 27715.00 -4.63 103.6 372. 18.02 2262. 092 1.65 107.1 3566. 17.27 27718.00 -4.53 103.2 3564. 16.27 2497. 099 2.52 101. 3393. 16.30 27719.00 -4.53 103.2 3564. 16.27 2497. 099 2.52 101. 3393. 16.50 27722.00 -4.53 103.2 3564. 16.27 2497. 099 2.52 101. 3393. 16.50 27722.00 -4.53 103.2 3564. 16.27 2497. 099 2.52 101. 3393. 16.50 27722.00 -4.53 103.2 3564. 16.27 2497. 099 2.52 101. 3393. 16.50 27722.00 -4.53 103.2 3564. 16.27 2497. 099 3.41 96.3 2899 13.97 27722.00 -4.53 103.2 3564. 16.27 2497. 099 3.41 96.3 2899 13.97 27722.00 -4.53 103.2 2393. 15.34 2545. 104 2.99 98.8 3060. 14.70 27728.00 -3.95 87.7 2399. 11.75 2599. 101. 5.94 86.5 2299. 13.97 27722.00 -4.57 85.6 2251. 11.18 2565. 097 3.81 94.1 2743. 13.32 27723.00 -3.95 87.7 2399. 11.75 2599. 101. 5.94 86.5 2299. 13.27 27720.00 -4.57 85.6 2251. 11.18 3456. 116 5.97 813 2024. 995 327720.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 2024. 995 327720.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 2024. 995 327720.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 2024. 995 327720.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 3024. 995 327720.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 5024. 995 32730.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 5024. 995 32730.00 -4.57 85.6 2551. 11.18 3456. 116 5.97 813 502. 995 32730.00 -4.57 85.6 5.			TE	ST DAY-				ST	AND ARO D	AY
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27718.0		*# ** ** * * * * * * * * * * * * * * *	3722.		2262 .	.092	1.65	107.1	3566.	
27719.00				17.01	2529 .	.102	2.13	1.04.1	3393.	
27720.00 -4.53 100.2 3193. 15.34 2545. 104 2.99 98.8 3060. 14.70 27721.00 -4.18 97.7 3025. 14.57 2539. 0.99 3.41 96.3 2899. 13.97 27722.00 -4.18 95.4 2863. 13.90 2508. 0.97 3.81 94.1 2743. 13.32 27723.00 -3.94 92.9 2704. 13.18 2366. 0.90 4.18 91.6 2592. 12.63 27724.00 -4.50 90.4 2550. 12.47 3067. 120 4.61 89.1 2443. 11.95 27725.00 -3.95 87.7 23.99 11.75 2593. 101 5.04 86.5 2299. 11.26 27726.00 -4.57 85.5 2253. 11.18 3468. 130 5.45 84.4 2159. 10.72 27727.00 -4.14 82.4 2112. 10.38 3015. 116 5.97 81.3 2024. 9.95 27728.00 -4.39 80.2 1974. 9.82 3383. 12.9 6.38 79.1 1892. 9.41 27729.00 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.76 27730.00 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.76 27731.00 -4.17 72.4 1588. 8.01 3414. 1357 7.74 71.4 1522. 7.67 27733.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27733.00 -4.17 65.0 1241. 6.45 3693. 135 8.93 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 152 8.15 66.7 1407. 7.11 27737.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27737.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27737.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27737.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27737.00 -4.50 69.7 1469. 7.2 3865. 152 8.15 66.7 1407. 7.11 27738.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27737.00 -4.50 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.00 -4.52 55.2 836. 4.65 4358. 161 10.49 54.4 601. 4.65 27739.00 -4.43 66.6 579. 332 4467. 172 11.70 46.0 555. 3.18 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27740.00 -5.30 37.8 3660. 2.90 5612. 216 12.09 43.0 481. 2.78 27740.00 -5.30 37.8 3660. 2.90 5612. 216 12.09 43.0 481. 2.78 27740.00 -5.30 37.8 3660. 2.90 5612. 216 12.09 43.0 481. 2.78 27740.00 -5.30 37.8 3660. 2.90 5612. 216 12.09 43.0 481. 2.78 27740.00 -5.57 34.1 304. 1.78 5964. 225 13.12 33.7 292. 1.70 27740.00 -5.57 34.1 304. 1.78 5964. 225 13.15 33.7 292. 1.70 27740.00 -5.57 34.1 304. 1.78 5964. 225 13.15 33.7 292.			3364.	16.27	2497 .	.099	2.52	101.8	3224.	
27721.00 - 4.31 97.7 3025. 14.57 2539. 099 3.41 96.3 2699. 13.97 27722.00 - 4.18 95.4 2863. 13.99 2508. 097 3.81 94.1 2743. 13.32 27723.00 - 3.94 92.9 2704. 13.18 2366. 099 4.18 91.6 2592. 12.63 27724.00 - 4.50 90.4 2550. 12.47 3067. 120 4.61 89.1 2443. 11.95 27725.00 - 3.95 87.7 2399. 11.75 2593. 101 5.04 86.5 2299. 11.26 27726.00 - 4.57 85.6 2253. 11.18 3469. 130 5.45 84.4 2159. 10.72 27727.00 - 4.14 82.4 2112. 10.38 3016. 116 5.97 81.3 2024. 9.95 27728.00 - 4.39 80.2 1974. 9.82 3383. 12.9 6.32 79.1 1892. 9.41 27729.00 - 4.47 77.4 1841. 91.4 5562. 138 6.85 76.3 1764. 8.76 27730.00 - 4.47 77.4 1841. 91.4 5562. 138 6.85 76.3 1764. 8.76 27731.00 - 4.47 77.4 1841. 91.4 5562. 138 6.85 76.3 1764. 8.76 27731.00 - 4.47 77.8 1712. 8.53 3556. 143 7.32 73.7 1641. 8.18 27733.00 - 4.50 69.7 1469. 7.2 3865. 155 8.15 68.7 1407. 7.11 27733.00 - 4.50 69.7 1469. 7.2 3865. 155 8.15 68.7 1407. 7.11 27733.00 - 4.50 69.7 1469. 7.2 3865. 155 8.15 68.7 1407. 7.11 27733.00 - 4.23 59.9 1030. 5.48 3908. 105 8.55 66.4 1297. 6.64 27736.00 - 4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 967. 5.26 27737.00 - 3.35 57.5 931. 5.06 3563. 141 10.47 54.4 801. 4.46 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27735.00 - 4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 967. 5.26 27737.00 - 3.95 57.5 931. 5.06 3563. 141 10.47 54.4 801. 4.46 27739.00 - 4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 967. 5.26 27737.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 632. 3.56 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 6.0 555. 3.18 27742.00 - 5.30 37.8 366. 2.18 5598. 214 12.41 31.37 3.3 500. 2.09 27740.00 - 4.88 49.3 660. 3.71 4.992. 184 11.31 48.6 6.32 3.56 2.70 2.70 4.70 0. 5.77 4.70 0. 5		•	31 93.	15.34	2545 .	.104	2.99	98.8	3060.	
27722.00 -4.18 95.4 2863 13.90 2508 097 3.81 94.1 2743 13.32 27723.00 -3.94 92.9 2714 13.18 2365 090 4.18 91.6 2592 12.63 27724.00 -3.95 87.7 23.99 11.75 2593 101 5.04 86.5 2299 11.26 27726.00 -4.57 85.5 2253 11.18 3469 130 5.45 84.4 2159 10.72 27727.00 -4.14 82.4 2112 10.38 3016 116 5.97 81.3 2024 9.95 27728.00 -4.33 80.2 1974 9.82 3383 129 6.32 79.1 1892 9.41 27729.00 -4.47 77.4 1841 9.14 3562 138 6.85 76.3 1764 8.76 27730.00 -4.47 77.4 1841 9.14 3562 138 6.85 76.3 1764 8.76 27730.00 -4.47 74.8 1712 8.53 3556 143 7.32 73.7 1641 8.18 17733.00 -4.17 72.4 1588 8.01 3414 135 7.74 71.4 1522 7.67 27733.00 -4.50 69.7 1469 7.42 3865 152 8.15 68.7 1407 7.11 27733.00 -3.42 67.3 1354 6.93 2808 105 8.55 66.4 1297 6.64 27734.00 -4.17 65.0 1241 6.45 3693 135 8.92 64.1 1190 6.18 27735.00 -4.50 69.7 1354 6.93 2808 105 8.55 66.4 1297 6.64 27736.00 -4.23 59.9 10.30 5.48 3908 147 9.75 9.1 987 5.26 27736.00 -4.52 55.2 836 4.65 3593 135 8.92 64.1 1190 6.18 27739.00 -4.50 69.7 1241 6.45 3693 135 8.92 64.1 1190 6.18 27739.00 -4.50 69.7 38.50 5.48 3908 147 9.75 9.1 987 5.26 27730.00 -4.52 55.2 836 4.65 3583 141 10.11 56.7 892 4.85 27730.00 -4.52 55.2 836 4.65 3583 141 10.11 56.7 892 4.85 27730.00 -4.54 62.5 133 5.00 5.48 3908 147 9.75 9.1 987 5.26 27730.00 -4.52 55.2 836 4.65 358 141 10.11 56.7 892 4.85 27730.00 -4.54 36.6 579 33.3 5.06 3563 141 10.11 56.7 892 4.85 27740.00 -4.88 49.3 660 3.71 4892 184 11.32 48.6 632 3.56 27740.00 -4.88 49.3 660 3.71 4892 184 11.31 48.6 632 3.56 27740.00 -4.88 49.3 660 3.71 4892 184 11.31 48.6 632 3.56 27740.00 -5.30 37.8 366 2.10 5598 214 12.81 37.3 350 2.09 27745.00 -5.57 34.1 30.4 178 5964 225 13.15 33.7 292 1.70 27746.00 -4.53 37.8 366 2.10 5598 214 12.81 37.3 350 2.09 27745.00 -5.57 34.1 30.4 178 5964 225 13.15 33.7 292 1.70 27746.00 -4.51 37.5 28.4 199 12.23 5635 212 13.71 28.0 190 1.18 27745.00 -5.57 34.1 30.4 178 5964 225 13.15 33.7 292 1.70 27746.00 -4.51 37.1 28.4 199 12.23 5635 212 13.71 28.0 190 1.18 27745.00 -5.57 34.1 130.4 178 5964 225 13.15 3.71 28.0 190 1.18 27745.00 -5.57 3.1 12.8	4		30 25.	14.57	2539 .	.099	3.41	96.3	2899.	
27723.0 0 -3.94 92.9 27.4. 13.18 2366. 090 4.18 91.6 2592. 12.63 27725.0 0 -3.95 87.7 2399. 11.75 2593. 101 5.04 86.5 2299. 11.26 27726.0 0 -4.57 85.6 2253. 11.18 3463. 130 5.45 84.4 2159. 10.72 27727.0 0 -4.14 82.4 2112. 10.38 3016. 116 5.97 81.3 2024. 9.95 27728.0 0 -4.39 80.2 1974. 9.82 3383. 129 6.32 79.1 1892. 9.41 27729.0 0 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.76 27730.0 0 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.76 27730.0 0 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.18 27731.0 0 -4.17 72.4 1588. 8.01 3414. 135 7.74 77.4 1522. 7.67 27732.0 0 -4.50 69.7 1469. 7.42 3865. 152 8.15 68.7 1407. 7.11 27733.0 0 -3.42 67.3 1354. 6.93 2808. 105 8.56 66.4 1297. 6.54 27734.0 0 -4.17 65.0 1241. 6.45 3693. 135 8.91 64.1 1190. 6.18 27735.0 0 -4.24 62.5 1133. 5.97 4045. 154 9.34 61.6 1085. 5.72 27735.0 0 -4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.0 0 -3.95 57.5 931. 5.06 3563. 141 10.11 50.7 892. 4.85 27739.0 0 -4.83 49.3 660. 3.71 4892. 184 10.11 50.7 892. 4.85 27739.0 0 -4.83 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27741.0 0 -4.83 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27741.0 0 -4.83 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27745.0 0 -4.43 46.6 5779. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.0 0 -5.43 43.6 502. 2.90 5612. 216 12.02 43.0 481. 2.78 27745.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27745.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.0 0 -5.57 34.1 304. 1.78 5964. 225 13.1E 37.7 292. 1.70 27746.0 0 -5.57 34.1 1.8 144. 2.5 5635. 2			28 63.	13.90	2508 .	.097	3.81	94.1	2743.	Water of Charles St. Lat.
27724.00 -4.50 90.4 2550. 12.47 3067. 120 4.61 89.1 2443. 11.95 27726.00 -3.95 87.7 2399. 11.75 2593. 101 5.04 86.5 2299. 11.26 27726.00 -4.57 85.5 2253. 11.18 3463. 130 5.45 84.4 2159. 10.72 27727.00 -4.14 52.4 2112. 10.38 3016. 115 5.97 81.3 2024. 9.95 27728.00 -4.39 80.2 1974. 9.82 3383. 129 6.32 79.1 1892. 9.41 27729.00 -4.47 77.4 1841. 9.14 3562. 138 6.86 76.3 1764. 8.76 27730.00 -4.47 77.4 1871. 8.53 3655. 143 7.32 73.7 1641. 8.18 27731.00 -4.17 72.4 1588. 8.01 3414. 135 7.74 71.4 1522. 7.67 27732.00 -4.50 69.7 1469. 7.42 3865. 152 8.17 68.7 1407. 7.11 27733.00 -3.42 67.3 1354. 6.93 2808. 105 8.56 66.4 1297. 6.54 27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.93 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27737.00 -3.35 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.85 27737.00 -4.88 49.3 660. 3.71 4892. 184 11.33 48.6 632. 3.56 27741.00 -4.88 49.3 660. 3.71 4892. 184 11.33 48.6 632. 3.56 27741.00 -4.84 46.6 579. 3.32 4467. 172 11.71 46.0 5555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.09 43.0 481. 2.78 27744.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27745.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27746.00 -5.57 34.1 304. 1.78 5964. 225 13.12 33.7 292. 1.70 27746.00 -4.51 20.41 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -4.51 20.41 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -4.51 20.41 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27748.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27748.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46			27 24.		2366 .	.090		91.6	2592.	
27725,00 -3.95 87.7 23.99 11.75 25.98 .101 5.04 86.5 22.99 11.26 27726,00 -4.5.7 85.6 22.53 11.18 34.69 .130 5.45 84.4 21.59 10.72 27727.00 -4.14 82.4 2112 10.38 3016 .116 5.97 81.3 20.24 9.95 27728.00 -4.39 80.2 1974 9.82 33.83 12.9 6.31 79.1 18.92 9.41 27729.00 -4.47 77.4 18.41 9.14 25.62 .138 6.86 76.3 17.64 8.76 27730.00 -4.47 74.8 1712 8.53 35.56 .143 7.37 73.7 16.41 8.18 27731.00 -4.17 72.4 15.88 8.01 3414 13.5 7.74 71.4 15.22 7.67 27732.00 -4.50 69.7 14.69 7.42 38.65 .152 8.15 68.7 14.07 7.11 27733.00 -3.42 67.3 13.54 6.93 28.08 10.5 8.56 66.4 12.97 6.54 27735.00 -4.17 65.0 12.41 6.45 36.93 13.5 8.91 64.1 11.90 6.18 27735.00 -4.23 59.9 10.30 5.48 3.908 14.7 9.75 59.1 98.7 5.26 27737.00 -4.52 65.2 83.6 4.65 43.58 14.1 10.11 56.7 892 4.85 27736.00 -4.52 65.2 83.6 4.65 43.58 1.61 10.41 56.7 892 4.85 27739.00 -4.52 65.2 83.6 4.65 43.58 1.61 10.41 56.7 892 4.85 27739.00 -4.52 65.2 745. 41.6 4.55 4.58 1.13 4.86 6.32 3.56 27741.00 -4.88 49.3 66.0 3.71 4.892 1.84 11.31 48.6 6.32 3.56 27742.00 -4.88 49.3 66.0 3.71 4.892 1.84 11.31 48.6 6.32 3.56 27742.00 -5.48 43.6 602 2.90 5612 21.6 12.01 43.0 46.1 2.71 2.71 2.71 2.71 2.71 2.71 2.71 2.	_ , , _ , , .		2550.	12.47	3067 .	. 120	4.61	89.1	2443.	
27726.00			2399.		2598 .	. 101	5.04	86.5	2299.	
27727.0 C -4.14		7 85.5	2253.	11.18	3468 .	.130	5.45	84.4	2159.	
27728.0 C -4.39	10 1 10 10 10 10 10 10			10.38	3015 .	.115	5.97	81.3	2024.	C & C C
27729.00 - 4.47 77.4 1841 9.14 3562 138 6.8E 76.3 1764 8.76 27730.00 -4.47 74.8 1712 8.53 3656. 143 7.32 73.7 1641 8.18 27731.00 -4.17 72.4 1588 8.01 3414 135 7.74 71.4 1522 7.67 27732.00 -4.50 69.7 1469 7.42 3865 152 8.15 68.7 1407 7.11 27733.00 -3.42 67.3 1354 6.93 2808 105 8.5E 66.4 1297 6.64 27734.00 -4.17 65.0 1241 6.45 3693 135 8.92 64.1 1190 6.18 27735.00 -4.44 62.5 1133 5.97 4045 154 9.34 61.6 1086 5.72 27736.00 -4.23 59.9 1030 5.48 3908 147 9.75 59.1 987 5.26 27737.00 -3.95 57.5 931 5.06 3663 141 10.11 56.7 892 4.65 27738.00 -4.52 55.2 836 4.65 4358 161 10.42 54.4 801 4.46 27739.00 -5.00 52.2 745 4.16 4951 185 10.92 51.5 714 3.99 27740.00 -4.88 49.3 660 3.71 4892 184 11.31 48.6 632 3.56 27741.00 -4.43 46.6 579 3.32 4467 172 11.71 46.0 555 3.18 27743.00 -5.43 43.6 502 2.90 5612 216 12.02 43.0 481 2.78 27743.00 -5.57 34.1 304 1.78 5964 225 13.1E 33.7 292 170 27745.00 -5.57 34.1 304 1.78 5964 225 13.1E 33.7 292 1.70 27748.00 -4.51 31.5 250 1.52 4895 118 14.2 1 2.8 1 37.3 350 2.09 27747.00 -5.17 28.4 199 123 5655 212 13.71 28.0 190 1.18 27748.00 -6.20 25.0 153 96 6790 256 13.95 24.7 146. 92 27748.00 -4.41 21.8 114 72 4928 180 14.21 21.5 109 59	_		1974.		3383 .	.129		79.1	1892.	Marie Company
27730.00 -4.47 74.8 1712. 8.53 3656. 143 7.32 73.7 1641. 8.18 27731.00 -4.17 72.4 1588. 8.01 3414. 135 7.74 71.4 1522. 7.67 27732.00 -4.50 69.7 1469. 7.42 3865. 152 8.15 68.7 1407. 7.11 27733.00 -3.42 67.3 1354. 6.93 2808. 105 8.56 66.4 1297. 6.54 27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.91 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 2736.00 -4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.00 -3.35 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.65 27738.00 -4.52 55.2 836. 4.65 4358. 161 10.49 54.4 801. 4.46 27739.00 -5.00 52.2 745. 4.16 4951. 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4992. 184 11.31 48.6 632. 3.56 27741.00 -4.43 46.6 579. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.09 43.0 481. 2.78 27745.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27746.00 -4.53 31.5 250. 1.52 4961. 185 12.45 40.0 414. 2.41 27746.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.16 33.7 292. 1.70 27748.00 -6.25 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27748.00 -6.25 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27748.00 -6.25 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27748.00 -6.25 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27748.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5	1 mg 11 1 mm 12 M		1841.	9.14	3562 .	.138	6.86	76.3	1764.	
27731.00 -4.17 72.4 1588. 8.01 3414. 135 7.74 71.4 1522. 7.67 27732.00 -4.50 69.7 1469. 7.42 3865. 152 8.13 68.7 1407. 7.11 27733.00 -3.42 67.3 1354. 6.93 2808. 105 8.56 66.4 1297. 6.64 27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.91 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27736.00 -4.23 59.9 1030. 5.48 3908. 147 9.73 59.1 987. 5.26 27737.00 -3.95 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.85 27738.00 -4.52 55.2 836. 4.65 4358. 161 10.41 54.4 801. 4.46 27739.00 -5.00 52.2 745. 4.16 4951. 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27741.00 -4.43 46.6 579. 3.32 467. 172 11.70 46.0 5555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.01 43.0 481. 2.78 27743.00 -4.75 40.6 432. 2.52 4961. 185 12.41 40.0 27744.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27746.00 -5.57 34.1 304. 1.78 5964. 225 13.11 33.7 292. 1.70 27746.00 -4.557 34.1 304. 1.78 5964. 225 13.11 33.7 292. 1.70 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.95 24.7 146. 92 27749.00 -4.441 21.8 114. 72 4928. 180 14.21 21.5 109. 63			1712.	8.53	3656,	.143	7.32	73.7	1641.	
27732.00 -4.50 69.7 1469. 7.42 3865. 152 8.13 68.7 1407. 7.11 27733.00 -3.42 67.3 1354. 6.93 2808. 105 8.56 66.4 1297. 6.64 27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.92 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27736.00 -4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.00 -3.95 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.85 27738.00 -4.52 55.2 836. 4.65 4358. 161 10.42 54.4 801. 4.46 27739.00 -5.00 52.2 745. 4.16 4951. 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.32 48.6 632. 3.56 27741.00 -4.43 46.6 579. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.02 43.0 481. 2.78 27743.00 -4.75 40.6 432. 2.52 4961. 185 12.45 40.0 414. 2.41 27744.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.15 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 59	9 8 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	applicação de minima de mi			3414 .	,135	7.74	71.4		
27733.00 -3.42 67.3 1354. 6.93 2808. 105 8.5E 66.4 1297. 6.64 27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.93 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27736.00 -4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.00 -3.35 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.85 27738.00 -4.52 55.2 836. 4.65 4358. 161 10.49 54.4 801. 4.66 27739.00 -5.00 52.2 745. 4.16 4951. 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27741.00 -4.43 46.6 579. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.02 43.0 461. 2.78 27744.00 -5.43 43.6 502. 2.90 5612. 216 12.02 43.0 461. 2.78 27744.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.1E 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69			1469.	7.42	3865.	.152	8.13	68.7	and the second second second	COLUMN TO SERVICE AND ADDRESS.
27734.00 -4.17 65.0 1241. 6.45 3693. 135 8.93 64.1 1190. 6.18 27735.00 -4.44 62.5 1133. 5.97 4045. 154 9.34 61.6 1086. 5.72 27736.00 -4.23 59.9 1030. 5.48 3908. 147 9.75 59.1 987. 5.26 27737.00 -3.35 57.5 931. 5.06 3663. 141 10.11 56.7 892. 4.85 27738.00 -4.52 55.2 836. 4.65 4358. 161 10.45 54.4 801. 4.46 27739.00 -5.00 52.2 745. 4.16 4951. 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4892. 184 11.31 48.6 632. 3.56 27741.00 -4.43 46.6 579. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.05 43.0 481. 2.78 27744.00 -5.30 37.8 366. 2.16 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.16 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27748.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER. THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.			6.93	2808.	. 195			E 7512 10 5	
27735.00 -4.44 62.5 1133, 5.97 4045 154 9.34 61.6 1086, 5.72 27736.00 -4.23 59.9 1030, 5.48 3908 147 9.75 59.1 987, 5.26 27737.00 -3.35 57.5 931, 5.06 3663 141 10.11 56.7 892, 4.85 27738.00 -4.52 55.2 836, 4.65 4358 161 10.45 54.4 801, 4.6 27739.00 -5.00 52.2 745, 4.16 4951 185 10.92 51.5 714, 3.99 27740.00 -4.88 49.3 660, 3.71 4892, 184 11.33 48.6 632, 3.56 27741.00 -4.43 46.6 579, 3.32 4467, 172 11.70 46.0 555, 3.18 27742.00 -5.43 43.6 502, 2.90 5612, 216 12.02 43.0 461, 2.78 27744.00 -5.30 37.8 366, 2.16 5598, 214 12.81 37, 3.50, 2.09 27745.00 -5.57 34.1 304, 1.78 5964, 225 13.16 33.7 292, 1.70 27746.00 -4.53 31.5 250, 1.52 4895, 184 13.44 31.1 239, 1.46 27748.00 -5.17 28.4 199, 1.23 5635, 212 13.71 28.0 190, 1.18 27748.00 -6.20 25.0 153, 96 6790, 256 13.95 24.7 146, 92 27749.00 -4.41 21.8 114, 72 4928, 180 14.21 21.5 109, 69			1241.	6.45	3693 .	.135	8.93	64.1	1190.	
27737.0		4 62.5	1133.	5.97	4045 .	. 154	9.34			
27737.00       -3.95       57.5       931.       5.06       3663.       141       10.11       56.7       892.       4.85         27738.00       -4.52       55.2       836.       4.65       4358.       161       10.42       54.4       801.       4.46         27739.00       -5.00       52.2       745.       4.16       4951.       185       10.92       51.5       714.       3.99         27740.00       -4.88       49.3       660.       3.71       4892.       184.       11.31       48.6       632.       3.56         27741.00       -4.43       46.6       579.       3.32       4467.       172.       11.70       46.0       555.       3.18         27742.00       -5.43       43.6       502.       2.90       5612.       216.       12.02       43.0       481.       2.78         27743.00       -4.75       40.6       432.       2.52       4961.       185.       12.45       40.0       414.       2.41         27744.00       -5.30       37.8       366.       2.16       5598.       214.       12.81       37.3       350.       2.09         27745.00       -5.57       34.1<	27736.00 -4.2	3 59.9	1030.	5.48	3908.	. 147	9.75			
27740.00 -5.00 52.2 745. 4.16 4951 185 10.92 51.5 714. 3.99 27740.00 -4.88 49.3 660. 3.71 4892 184 11.31 48.6 632. 3.56 27741.00 -4.83 46.6 579. 3.32 4467. 172 11.70 46.0 555. 3.18 27742.00 -5.43 43.6 502. 2.90 5612. 216 12.09 43.0 481. 2.78 27743.00 -4.75 40.6 432. 2.52 4961 185 12.45 40.0 414. 2.41 27744.00 -5.30 37.8 366. 2.18 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.15 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27737.00 -3.5	5 57.5	931.	5.06		. 141	10.11	5.555		
27739.0	27738.00 -4.5	2 55.2	836.		4358 .	.161		W. D. T. U.	The second second	
27740.00       -4.88       49.3       660.       3.71       4892.       184       11.31       48.6       632.       3.56         27741.00       -4.43       46.6       579.       3.32       4467.       172       11.71       46.0       555.       3.18         27742.00       -5.43       43.6       502.       2.90       5612.       216       12.02       43.0       481.       2.78         27743.00       -4.75       40.6       432.       2.52       4961.       185       12.45       40.0       414.       2.41         27744.00       -5.30       37.8       366.       2.18       5598.       214       12.81       37.3       350.       2.09         27745.00       -5.57       34.1       304.       1.78       5964.       225       13.16       33.7       292.       1.70         27746.00       -4.53       31.5       250.       1.52       4895.       184       13.44       31.1       239.       1.46         27747.00       -5.17       28.4       199.       1.23       5635.       212       13.71       28.0       190.       1.18         27749.00       -6.20       25.3			745.	4.16	4951 .	.185	10.92			
27742.00 -5.43	27740.00 -4.8	8 49.3	660.	3.71	4892 .			1 7 2 7 7 7	* I S S S S S S S S S S S S S S S S S S	The second second second
27743.00 -4.75	27741.00 -4.4	3 46.6	579.	3.32	4467 .	0.00				
27744.00 -5.30 37.8 366. 2.16 5598. 214 12.81 37.3 350. 2.09 27745.00 -5.57 34.1 304. 1.78 5964. 225 13.15 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.60 -6.20 25.0 153. 96 6790. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27742.00 -5.4	3 43.6	502.	2.90	5612 .	.216		10 2 T D		
27745.00 -5.57 34.1 304. 1.78 5964. 225 13.18 33.7 292. 1.70 27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.03 -6.20 25.3 153. 96 6793. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27743.00 -4.7	5 40.6	432.	2.52	4961 .					
27746.00 -4.53 31.5 250. 1.52 4895. 184 13.44 31.1 239. 1.46 27747.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.03 -6.20 25.3 153. 96 6793. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27744.00 -5.3	37.8	366.	2.18	5598 .	The second second second				
27748.00 -5.17 28.4 199. 1.23 5635. 212 13.71 28.0 190. 1.18 27748.00 -6.20 25.0 153. 96 6790. 256 13.95 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27745.00 -5.5	7 34.1	304.	1.78	5964 .					
27749.00 -6.20 25.0 153. 96 6790. 256 13.99 24.7 146. 92 27749.00 -4.41 21.8 114. 72 4928. 180 14.21 21.5 109. 69	27746.00 -4.5	31.5	250.	1.52						The late and the late of the l
27748.65 -6.26 25.3 15396 5793256 13.99 24.7 14692 27749.06 -4.41 21.8 11472 4928180 14.21 21.5 10969	27747.00 -5.1	7 28.4	199.							
27749.00 -4.41 21.8 11472 4928180 14.21 21.5 10959			153.	.96						
			114.	.72						e ce les la
27750.00 -2.21 19.8 7960 2585097 14.32 19.5 7657		1 19. 8			the second second	and the state of t	14.32	19.5	76.	.57
27750.21 -1.74 19.5 7258 2091077 14.32 19.2 6956	27750.21 -1.7	4 19.5	72.	.58	2091 .	.077	14.32	19.2	69.	.56

TEST NO. 674	MARK II A	HTISKIDZS	TANDARU T	IRES CHOP	KN)/WET	HUNWAY "		****** *
STAND @GT	TEST WGT	PRESS	ĀLT	TEMP	WIND	VEL	WIND	DIREC
43000 LBS	43260.L9S	27.590	T Tape T	14.4 0	6.7	KTS	190.0	DEG MAG
	*						AND ADD 1	\4¥
			Y				ANDARD L	. KE :
	GNDSPD1		FBR	UBR"		"KTAS	0157	43.19
24392.20 -3.9				0.000	0.00	150.6	9857 • 9656 •	42.11
24393.00 -3.69				0.000	0.00	148.7	9407.	40.85
24394.00 -4.2			•	0.000	0.00	146.5	9162.	39.50
24395.00 -3.6			-	~0 • 000 =	• 0 i	144.1		38.42
24396.00 +3.6				0.000	•01	142.1	8923.	37.16
24397.00 -4.0						139.7	8685	
24398.00 -3.8				.014	.17	137.3	8451.	35.89 -34.91
24399.00 -3.4					.17	135.4	8224	
24400.00 -3.8				•026	•31	133.1	7997	33.70 32.68
24401.00 -3.5				•016	.41	131.0	7775.	
24402.00 -3.2				_	.49	128.9	7557	31.62
24403.00 -3.3	5 133.7 813				-52	127.1	7343.	30.73
24404.00 -3.5	3 131.6 78				•69	124.9	7131.	29.72
24405.00 -3.2	5 129.6 75	70. 32.1	2 577.	.080	.82	123.0	6923.	28.78
24406.00 -3.0	7 127.9 74	59. 31.d	7 - 445.		.89	121.3	6720.	27.99
24407.00 -3.5		44. 30.2	7 1127.	<u>.</u> 040	1.09	119.2	6517.	27.05
24408.00 -3.3		34. 29.4	2 1027.		1.27	117.4	6320	26.25
24409.00 -2.7		26. 28.4	6 48A.	.017	1.44	115.4	6125	25.35
24410.00 -3.1		21. 27.6	7 1086.	•036	1.60	113.7	5933	24.62
24411.00 -3.0		20. 26.9	5 1099.	.036	1.78	115.5	5746	-23.94
24412.00 -3.1		25.9	7 1408.	.046	5.0R	110.0	5559.	23.04
24413.00 -3.0		25. 25.2	4 1330.	.042	S•35	108.4	5377	22.35
24414.00 -2.6		34. 24.4		.030	2.54	106.5	5197	21.61
24415.00 -3.3		44. 23.7	5 5056	053	5.83	104.9		20.93
24416.00 -2.7		58. 22.4	6 1225.	.037	3.12	103.1	4847.	20.23
24417.00 -3.0		74. 22.2	8 1815.	• 055		101.5		-19.60 -
24418.00 -2.5		94. 21.5		.035	3.67	99.7	4509.	18.91
24419.00 -3.1	-	16. 20:9	4 1993.	• 051		98.2	4345	
24420.00 -3.1		1.05	9 2100.		4.31	96.3	4183.	17.66
24421.00 -3.1		59. 19.3	3 2296.	* *070 -	4-73	94.1	4021	
24422.00 -2.5		00. 18.8	1442.	.043	4.97	92.9	3868.	16.43
24423.00 -3.1				.074	5.33		3714.	15.78
24424.00 -2.8		72. 17.5	0 2023.	.061	5.68	89.3	3564.	15.18
24425.00 -3.0		12. 16.9		.070	6.03	87.7	3417.	14.63
24426.00 -3.4	_	54. 16.2			6.47	85.7	3271.	13.98
24427.00 -2.3		01." 15:5		. 05]	-6.83-	- 83·8		13.36
24428.00 -1.7		50. 15.1	7 930.	.028	6.98	82.7	2994.	13.03
24429.00 -2.2		00- 14-7	9 1627	-040	7-13	-81.6-	2859	12.67

TEST NO. 6	. <b>7</b> ਜ	MARK I	I ANTIS	KID/STA	MDARD T	IRESCHO	AN) /WET	RUNWAY		
er No Not		TECT NOT	Ď	PESS 4	LΤ	TEMP	JIND	VEL		DIREC
STAND WGT		TEST NGT 8600.LBS		.591 IN		16.1 C	6.5		197.0	DEG MAG
38000,L95	3									
			TF	ST MAY-				ST	ANDARD D	YAC
TOD	ACCEL	GND-SPD	DIST	KE.	Fak	(IHD	EBR	KTAS	DIST	KE
	-3.99	142.6	4738.	34.75	117.	.005	.01	134.5	7700.	30.43
	-3.62	140.4	8511.	33.70		0.000	.01	132.4	7491.	29.47
	-3.96	138.1	8276	35.61	383.	.018	.07	130.1	7274.	28.48
	<b>-3.</b> 53	136.0	8045	31.60		.001	.10	128.0	7062.	27.55
	-3.71	133.9	7817.	30.52	391.	.017	.16	125.9	6853.	26.66
	<del>-3.69</del>	131.6	7593.	29.59	524	.055	•58	123.7		25.72
	-3.33	129.4	7373.	16.88	210.	•000	•37	121.5	6445	24.84
	-3.28	127.6	7156		279.	012	•40	119.7	6248	
	-3.76	125.5	6942.	26.90	1003.	. ()47	.57	117.7	6052.	23.28
		123.4	6733.	26.01	745.	<b>2030</b>	.75	115.6		22.47
	-2.82	121.5	6526.	25.21	108.	.004	. A3	113.7	5672.	21.75
26435.75	-3.50	119.8	6322.	24.50	1034.	.042	.93	112.0		21.11
	-3.06	117.6	6122.	23.64	565.	.026	1.13	109.9	5305.	20.32
	-3.59	115.6	5925.	22.85	1434.	055	1.36	108.0	5126.	
	-2.74	113.7	5732.	22.11	520.	.020	1.53	106.1	4951.	
26439.75	-3.74	111.8	5541.	21.35	1345.	.070	1.79	104.2		18.26
26440.75	-3.35	109.7	5355	20.55	1504.		2.11	102.1		17.53
	-2.60	107.9	5171.	19.90	683.		5.58-	100.4	4442.	16.95
26442.75	-3.13	106.3	4990	19.30	1421.		2.48	98.8	4279.	
26443.75		104.4	4513.	18.62	1775.		2:77	96.9	4119.	15.80
26444.75	-3.10	102.4	453d ·	17.90	1595.		3.07	94.9	3961.	15.15
	-2.84	100.6	4467.	17:29	1374.	. 049	3.32	93.2	3807.	
26446.75	-2.67	99.1	429H.	16.77	1233.	.045	3.52	91.7	3657•	
26447.75	-2.73	97.5	4133.	15,23	1376.		3.73	90.1		13.66
26448.75	-3.41	95.5	3969.	15.58	2296.	·021	4.15	88.2	3363.	
26450.00	-2.81	793.5		14.93	1658.	•040	4.41	86.2		
26451.00	-3.34	91.4	3514.	14.29	2367.	.086	4.76	84.2	3045	
	-2.796	89.7	3462.	13:75	2002.	•071	5.08		2910.	
26453.00	-2.46	80.1	3312.	13.27	1463.		5.31	90.9	2777•	
	-2.95	86.4		12.77	~2135.				2647	
26455.00	-3.05	84.8	3020.	15.30	2304.		5.90	77.7	2520.	
	-3.54	82.6	2373.	11.65	. 1862		6.32	75.5	2392•	
26457.00	-2.49	81.0	2741.	11.22	1789.		6.60	73.9	2272•	
	-2.90	79.3	2505.	10.74	2350.		6.29	72.2	2153•	
26459.00	-3.27	77.4	2473.	10.25	2865.		7.24	70.4	2036	
	-3.44	75.7	2343.	9:79	- 3122		7.61	··68.7		
26461.00	-3.24	73.5	2214.	9.55	2956		8.01	66.5	1811.	
	-2.71	71.9	2095.	8.84	7369		-R - 30	65.0	1705.	
	-3.00	70.1	1975.		2792		8.62	63.2	1601.	
26464.00	-3.35	68.4	1958.	8.00	3263		8.97	61.5	1500	6.37 5.93
26465.00	-3.25	66.2	1745.	7.49	3204		9.35	59.4	1400•	
26466.00	-3.11	64.5	1534.	7.11	3088		9.68	57.7	1305	
26467.00	-3.66	62.3	1527.	6:64	3813		10.07	55.6 52.7	1212.	
26468.00	-3.20	60.5	1424.	6.25	3314.		10.42	53.7	1123. 1037.	
26469.00	-3.35	58.4	1323.	5 • ೮4	3556		10.77	51.7	954	
	-3.06	56.5	1226	5.45	3254		11.10	49.8	954 • 875 •	
26471.00	-2.28		1135.	5.15	2367		11.35	48•2 47•9	856	
26471.25			IJ09.	5.08	2075	• 050	~11.35	41.9	<b>₫</b> ⊅0•	3.110

A STATE OF THE PROPERTY OF THE

		ANTECH ID	STANDARD T	THES (WO)	NIZWET 1	RUNWAY		
TEST NO. 670							25.0	0.0000
STAND #GT	TEST WGT	PRES	S ALT	SJEMP -	WIND	()	CAIW.	DEG MAG
34000.LBS	34500 .LBS	27.59	S IN HG	15.0 C	8.5		193.0	
	- '	TEAT				STAI	NDARD D	
		DIST K	트 누선님	1164	CDK	KTAS	DIST	· KE
	CEL GND-SPD	7872. 28	.55 - 110		5 00	127.4	6792.	24.43
1.00,000		7573. 27		0.000	.03	125.4	6610.	23.65
		7448. 26.	.81 473	. 10.024	70.	123.2	6404.	22.85
	.06 132.5 .90 130.0	7226. 25			.19	120.8		21.96
	.38 .12b.1	7009. (25	.05 31	500.	. 6. 20	118.9	6003	21.26
	05 125.7	5794. 24	.12 895	1 01.0 -	35	116.5	5,000	20.43
	26 123.7	6584 - 23	.38 186	0000	.42	114.6	561/+	19.70
28099.25 -3 28100.25 -3	50 121.5	6377 22	.56 558	. 027	T. 253 - 1	112.4	5428	19.02
	37 119.6	6174. 21	.86	025	.62 •62	1.10.5	5645.	10.437
28102.25 -3	.19 117.5		.10 488	055	74. "	108.5	5004	17:00
28103.25 -3	.83 115.6	5777. 20	.41 . 1255	• • 059		44	4880	17.09
	40 113.3	5584. 19			1.15		4/110	16.36 15.74
	.19 111.3	5394. 18	.90 841		1.31	102.3		15.26
	.02 109.7	5208. 716	.37 744		1.43	100.7	43/40	14.64
	.64 107.6	5024. 17	.67 1492	069	.1.67		4209	14.00
	.03 105.3	4544. 16	.95 976	043	1.91	96.4	2002	13.60
	.16 103.9	4568. 16	.50 . 1171	052	2.05		2775	12.96
26110.25 -3		4494. 15	.78 1554		2.34	92.8	3584	12.47
28111.253		4324. 15	.22 1347	. \$ .060	Po 3%		3/34	11.98
28112.25 -2	.70 (98.0		.67 963	- 20042	2.76	89.2	3292	11.60
	.96 96.6	3993. 14	.24 1316	059	2.93			11.08
	.30 . 94.5	3532. 13	65 1774		3.20	83.9	2 2 0	10.60
	.11 - 92.6	2474 13	1.11 1656		3.41	82.2		10.16
	.15 90.9		.61 1779	136	4.06	80.4	2740.	
	.91 89.1		.12 2663		4.31		2608.	
	.74 86.8		.50 433		4.40		2485.	9.03
28119.25 -2	1.08. [6.]		.32 1615		4.75	75.3	2358	8.53
28120.25 -3	1.50 83.9	**	1.74 2445		5.02	73.5	2237.	8.13
	0.58 EE.		1805	100	5.32	71.7		7.73
28122.253	.35 80.2				5.55	70.1	2003.	
CO B M T T T T	.27 78.6		•		5.80	. 68.6	1892.	
	3.45 77.1				6.17	66.3	1779.	6.62
	74.8		3.54 2526 3.13 2679		6.48	64.5	1672.	
	72.9		7.73 2054		6.75	62.7	1569.	5.93
CO	70 71.2		7.33 3091		7.07	60.9	1467.	- 5.58
	8.59 69.3		5.90 2934		7.41	58.9	1369.	5.22
	67.2		50 2464	198		56.9	-1273	4.87
C01001-3	.89 65.2		22 2656		7.90	55.5	1184.	4.64
	63.8		.78 3224		8.30	-53.2	1093.	
	3.50 61.5		325		8.62	51.4	1008.	3.98
	3.49 59.7		5.07 304		8.43	49.4		3.67
	3.24 57.6		3320		9.23	47.5	846	3.39
F0*004-2	3.44 55.7 3.56 53.6		4.39 3500		9.55		770.	- 3.11
			4.04 3698	4 4 4	9.87	43.3	697.	
	3.68 51.4	889	3.72 300		10.15	41.3		
	2.99 49.4 3.72 47.6		3.46 381	V 100 100	10.42	39.5		
			3.12 385	.152	10.73		499.	
			2.55 355	.130	11.00	35.2	440.	
E (1 M 1 M 2 M 2 M 1	3.38 43.2 3.56 40.9		2:56 ** 380	145		32.9	384.	
20145	1.72 39.5	533.	2.39 185		11.37	31.6	346	1.50
28143.00 -	4 4 7 61							

TEST NO. 68A	, MAR	K II A	MISKIDAS	SOMMERS	.TIRES/	WET RUNW	AY		
STAND WGT	TEST WGT	ŗ	PRESS AL	T	TEMP	DAIM	VEL	WIND	DIREC
43000.LBS	4250J.LBS		7.625 IN		10.0 C	2.2	KTS	242.0	DEG MAG
	- ::::	T6	ST DAY-				ST	ANDARD I	ΣΑΥ
TOD ACCE	. GND-SPD	DIST	KE	FBR	UBR	EBR	KTAS	DIST	KE
24442.70 -4.18		8174.	44.38		0.000	0.00	152.4	3161.	44.22
24443.50 -4.7	151.2	7959.	43.11	0.	0.000	0.06	150.2	7.953.	42.94
24444.50 -5.14	148.2	7715.	41.44	0.	0.000	0.00	147.2	7696.	41.25
24445.50 -4.4:		7468.	39.94	9.	0.000	0.00	144.5	7446.	39.73
24446.50 -4.17		7225.	38.51	C .	0.000	0.00	141.8	7200.	38.29
24447.50 -3.88	3 149.6	6985.	37.26	349.	.013	.0€	139.5	6'958.	37.03
24448.50 -3.90		6750.	36.00	484	.019	.19	137.1	6721.	35.76
24449.50 -3.80	135.9	6519.	34.83	-541 .	.021	. 30	134.8	6487.	34.58
24450.50 -4.37		6291.	33.53	1458.	.056	.5 2	132.2	6258.	33.27
24451.50 -3.94		6068.	32.37	1067.	.039	. 84	129.9	6032.	32.10
24452.50 -3.54	123.7	5850.		701.	.025	1.04	127.5	5812.	30:97
24453.50 3.96	126.5	5634.	30.20	1403.	.048	1.26	125.4	5594.	29.31
24454.50 -3.75	124.2	5422.	29.11	1280.	.046	1.56	123.0	5381.	28.82
24455.50 -3.64	122.1	5215.	28.13	1272.	.044	1.80	120.9	5173.	27 . 83
24456.50 -3.8		5010.	27.06	1760.	.061	2.14	118.5	4967.	26.75
24457.50 -3.55	117.5	4610.	26.06	1699.	.056	2.50	116.3	4765	25.75
24458.50 -3.61	115.4	4613.	25.12	1802.	. 057	2.83	114.1	4567.	24.80
24459.50 -3.85	113.3	4420.	24.21	2269.	.071	3.23	112.0	4373.	23.89
24460.50 -3.56	111.1	4231.	23.27	2145.	. 057	3.63	169.8	4183.	22.94
24461.50 -4.08	108.7	4045.	22.29	2840 .	.088	4.11	107.4	3997.	21.96
24462.50 -3.65	105.5	3864.	21.39	2370 .	.075	4.57	105.2	3815.	21.05
24463.50 -3.8:	1 194.4	3686.	20.56	2683.	.085	4.95	103.1	3637.	20.23
24464.50 -4.35	101.8	3512.	19.56	3538.	.110	5.58	188.5	3461.	19.22
24465.50 -3.45	99.6	3342.	18.72	2460 .	.076	6.04	98.3	3291.	19.38
24466.50 -4.29		3175.	17.86	3684 .	.112	6.57	95.9	3124.	17.52
24467.50 -3.46		3013.	15.99	2683.	.083	7.08	93.5	2962.	16.65
24468.50 -3.5	92.9	2855.	16.29	2936.	.090	7.51	91.5	2803.	15.94
24469.50 -3.56	90.8	2730.	15.53	3400 .	-105	7.87	89.3	2643.	15.19

t.

	•	THE F WAT	OL.	RESS AL	T	TEMP	MIND	VEL		DIREC
STAND WG		TEST WGT 7800.LBS		630 IN	•	5 S C	4.8		215.0	DEG MAG
38000.L3S	3	/ AUU • LDS	211	1030 10						
			TE	T DAY				STA	NUARD D	)AY
			DIST	-KE	FBR	UBR	EBR	KTAS	DIST	KE
TOD		GND-SPD	6977.	33.35		0.000	0.00	136.6	6601.	31.39
26722.70	-4.03	141.2			152.	.009	.02	134.5	6415.	30.41
26723.50	-4.28	139.0	6788	32.35	73.	.004	.03	132.2	6189.	29.38
26724.50	-4.00	136.7	6555	31.29			.20	129.5	5964	28.19
26725 • 5°	-4.59	134.0	6326.	30.07	919.	•048		127.2	5747.	27.21
26726.50	-3.66	131.6	610S.	29.06	18.	•001	.25	124.9	5532	26.26
26727.50	-4.05	129.5	5882•	28.08	626.	.031	•32		5321	
26728.50	-4.05	127.1	5665.	27.03	303.	.040	-48	122.5	5115.	
26729.50	-3.86	124.8	5453.	26.05	704.	.034	.63	120.2	-	
26730.50	-3.80	122.4	5244.	25.06	807.	.037	.81	117.8	4912.	
26731.50	-3.77	120.3	5039.	24.22	919.	.041	•96	.115.7		22.52
26732.50	-3.74	117.9	4538.	23.25	1029.	.045	1.19	113.3	4519	
26733.50	-3.87	115.6	4541.	22.38	1349.	.059	1.43	111.0	4328	
_	-3.67	113.5	4447.	21.56	1254.	• 055	1.66	108.9		19.95
26734.50	-4.12	111.3	4258.	20.71	1919.	.082	1.98	1066.		19.13
26735.50	-3.79	108.8	4672.	19.80	1664.	.072	2.32	104.2	3779.	
26736.50		106.6	3591.	19.03	1552.	.065	2.60	102.0	3604	17.51
26737.50	-3.58		3712.	18.25	2107.	.088	2.93	99.8	3433.	
26738.50	-3.96	104.4		17.46	1738.	.072	3.27	97.5	3265.	16.00
26739.50	-3.53	102.2	3538.		1963.	.079	3.57	95.5	3102.	15.35
26740.50	-3.63	100.2	3367.	16.78		.093	3.95	93.2		14.61
26741.50	-3.79	97.8	3200.	16.02	2265.		4.32	91.1	2786.	
26742.50	-3.93	95.7	3037.	15.33	2526.	-104		88.6.		
26743.50	-3.66	93.3	2878.	14.55	2341.	• 094	4.73 5.09	86.5	2485	
26744.50	-3.71	91.2	2722.	13.40	2489	.101				11.93
26745.50	-4.27	8b.9	2570.	13.22	3260.	.131	5.54	. 84.2		
26746.50	-3.52	86.2	2422.	12.43		0.000	5.91	81.5	2198	10.79
26747.50	-3.03	84.7	2278.	12.02		0.000	5.91	80.1		
26748.50	-4.02	82.2	2137.	11.31		.126	6.34	77.6	1929.	
26749.50	-4.11	60.2	2000.	10.76	3462.	•133	6.77	75.5		9.59
26750.50	-4.47	77.4	1867.	10.03	3977.	•157	7.29	72.8	1674.	
26751.50	-4.12	74.9	1738.	9.40	3686.	.141	7.77	70.3	1552	
26752.50	-4.21	72.4	1614.	8.78	3879.	.149	8.24	67.8	1435.	
26753.50	-4.34	70.0	14,+.	8.19	4128.	.157	8.72	65.3	1322.	
26754.50	-4.14	67.3	1378.	7.58	3987.	•150	9.20	62.7	1213.	
•	-3.63	65.1	1266.	7.09	3456.	.133	9, 60	60 • 4.	1109.	
26755.50	-4.24	62.7	1158.	6.59	4254.		10.03	58.1	1009.	
26756.50		60.3	1055.	6.08	3914.		10.45	55.6	913.	5.20
26757.50	-3.88	57.8	955	5.59	4740.		10.88	53.1	821.	
26758.50	-4.51	_	560.	5.09	5046.		11.35		733	4.28
26759.50	<b>-4.71</b>		769.	4.54	5434.		11.83	47.4	650	
26760.50	-4.97	52.1		4.07	5102	.184	12.27	44.6	571	3.35
26761.50	-4.61	49.3	584.			-186		41.8	497	
26762.50	-4.51	46.5	503.		5105.	1 100	13.05	39.4		2.61
26763.50	-4.51	44.1	526	.3.25				36.5	365	
26764.50	-4.65		454.	2.84	5356		13.84	33.4		
26765.50	-5.71	38.1	387.	2.42	6646				251	
26766.50	-3.96	35.1	326.	2.06	4659.		14.18	30.4		
26767.50	-4.93		268.	1.81.						1.33
26768.50	-5,19	29.5	216.	1.45	6204.	.219	14.79	24.7	157	
26769.50	-4.91		168.	1.19	5907.		15.06	22.0		• <u> 81</u>
26770.50	-4.35		125.	•93	5310.		15.30	18.8	83	
26771.25	48		97.	-82	785.	027	15.36	17.4	62	51

TEST NO. 68C	МДЯ	K II ANT	ISKIDA	SOMMERS	TIPES	WET RUNWA	AY		
					TEMP .	WIND		WIND	DIREC -
STAND WGT	TEST WGT		1632 II	ALT	15.0 C	2.7	KTS		DEG MAG
34000.LBS	34100.LBS		nac Li		1.540 0				
4* =		IFS	T DAY					TANDARD I	
	L GND-SPD		KE	FRR	UBR	EBH	KTAS	DIST	KE
28416.17 -4.1		0416.	27.76	80.	.004	•00	132.5	6118.	26.40
28417.00 -4.2		6227.	26.92	231.	013	• 04	130.4	<b>5936</b>	25.60
28418.00 -4.2		5004.	25.92	394.	.022	.11	127.9	5719.	24.63
28419.00 -4.4	2 -128.4	.5785 • ··	24.89	790•			125.3		.23 .64
28420.00 -4.2		5570.	23.98	705.		•41	123.0	5300	22.75 21.80
28421.00 -3.9		5360.	22.99	554.		• •57	120.4	5097 • 4897 •	21.02
28422.00 -3.8		5154.	22.18	612.		•67	118.2		_ 20.18.
28423.00 -4.2	0 418,8	4951.	21.31	1157.			115.8	4510	19.32
28424.00 -3.7		4752.	20.42	770.		1.08	111.3		18.66
28425.003.7	8 .114.3		19.73		• 0.44	1.21	108.9	4138	17.86
28426.00 -3.8			18.90			1.44	106.7	3958	
28427.00 / -4.3	5 104.7	4179.				2.00	104.3	3782	16.36
28428.00 -3.6		3997.	17.34	- 1269.	.055			3609.	15.63
28429.00 4.3	5 104.8			2136.	.057	2.60	99.7	3441.	14.95
28430.00 -3.4		3543.	15.87	1307.			97.4	3276	14.27
28431.003.8	5 100.2				• 069	3.17	95.3	3115.	13.68
28432.00 -3.5		3304.	14.56	1034+	0.70		93.2	2958.	
28433.00 -3.6			13.33		.087	3.78	91.1	2804.	12.50
28434.00 -3.7		2980 •	10.70	1711.			89.0	2655.	1192
28435.00 -3.3		-2824 • 2670 •	12.16	2167.		4.37	87.0	2508.	11.38
28436.00 -3.6		2570.	11.56	2477		4.72	84.7	2365.	10.80
28437.003.8		2375.	10.97			5.10	82.5	2225.	10.24
28438.00 -4.0 28439.00 -4.2		2233	10.31	3083	132.	5.54	79.9	2089.	9.60
		2096	9.76			5.89	77.7	1958.	9.08
		1962.	9.25			6.25	.75.6	1831.	8.59
28441.00 -3.8 28442.00 -3.6		1832.	8.71	2763.		6.61	73.3	1706.	8.08
28443.00 -4.0		1705.	8.23	3238.	133	, 6.98	71.2		7.62
28444.00 -4.3		1583.	7.65		.154	7.42	68.5	1469.	
28445.00 -4.0	_	1465.	- 1.		140	7.81		1357•	6.58
28446.00 -4.8	_	1351.	6.58	4323	•179	8.27	63.4		6.05
28447.00 -4.0		1242.	6.11			. 8.67	61.0		5.60. 5.10
28448.00 -4.1		1136.	5.57			9.08	58.2		
28449.00 -4.0	56.7	1035.	.5.21			9.42	56.2		
28450.00 -4.2	7 56.1	938.	4.76			9.81	53.6		
28451.004.1	8 53.7	846.	4.35			10.17	51.1		
28452.00 -4.6	51.1	757.	3.94			10.55	48.6 45.9		
28453.00 -4.4		673.	3.53			10.92	43.4		-
28454.00 -4.1	45.9	594 •	3.17			11.25 11.60	40.7		
28455.00 -4.8		518.	2.81			11.94	38.0		_
28456.00 -4.		448.	2:47			12.27	35.2		
28457.00 -5.0			2.13			12.59	32.1		
28458.00 -5.		321.	1.79			12.86	29.3		
28459.00 -4.5		265	1.25		_	13.13	26.4		
28460.00 -5.		214. - 168.	1.00			13.39.	23.4		82
	56 25.7	128.	.75			13.62	20.0		- 60
28462.00 -4.8	39 22.3 44 19.9	92.	50			13.75	17.7	74.	
		88.	.58		149	13.75	17.4		•46
28463.12 -3.2	1741	4 ·	• -		-				

C

STAND WGT	TEST WGT	PPESS	ALT	TEMP.	MIND		MIND	DIREC
3000 LB5	43300.LBS	27.570		-12.8 C	5.6		195.0	DEG MAG
				ri a			TANDARD	
			AY			KTAC	DICT	KE
TOD ACC		IST KE			EBR			41.68
4439.65 -5.		493. 45.			.01	148.0	8751	40.85
4440.50 -1.	84 152.5 " 9	275. 44.		0.000	.04	146.5		
4441.50 -5.	06 150.6 9				. 13	144.7	8301	
4442.50 -4.	76 147.5 8	766. 41.			•56	141.6	8060	
4443.50 -3.	56 145.0 8			0.000		139.0	7824	36.80
4444.50 -3.		276. 39.			-64	136.9	7593.	35.70
4445.50 -3.	71 140.6 8	036. 37.			74	134.7	7366.	34.53
		801. 36%		0.000	.74	132.9	7144	
24447.50 -3.		568. 36.				131.4	6925	32.88
4448.50 -2.		339. 35.	00	0.000			6708.	31.82
24449.50 -2.			08 4 15 (	0.000	88	127.5	.6495	
4450.50 -3.				7015		125.8	6284	
24451.50 -3.	,	567. 32.		3010		124.0	6077	29.25
24452.50 -3		450. 31.		025	1.20	121.7		-58.51
4453.50 -3.		236. 30.		016		120.5		27.50
4454.50 -3			47 1122	2. (141)	- 1.45	118.2		26.60
24455.50 -3		318. 28.		7. 4.058		115.9	: 5277 •	25.59
		515: 27.			2:09	113.9	5086 ·	
		415. 26.			2.45	111.8	4897	23.78
		218. 25.	56 1429	046		109.8	4713.	22.93
		025. 24.				107.7	4531.	22.0B
24459.50 -3.		836 - 23			3.62	105.5	- 4353°	21-19-
24460.50 -3		550 22				1.03 . 4	4179.	20.34
24461.50 -3.		467. 21.			4.46	101.4	4008.	19.59
24462.50 -3		289. 21.		0.000	4.71	99.5	3842.	18.84
24463.50 -1.		111. 20.				98.5	3679.	18.45
24464.50 -3.	J					96.1	3516.	17.58
24465.50 -3.						94.3	-3359	
24466.503.		8768. 19. 8501. 18.				92.0	3203.	
24467.50 -3.						90.1	3052.	
24468.50 ,-3.						88.2	2904.	
24469.50 -3.		3278. 16.				86.2	2759	
24470.50 -3.		1122. 16.				84.1	2617.	
24471.50 -3.	• • • • • • • • • • • • • • • • • • • •	2969. 15.				81.9		12.76
24472.50 -3		2819. 14.				80.0	2345.	
24473.50 -3.		2673. 14.				78.0	-2214	
24474.50 -3		2531. 13.				76.2	2086	
24475.50 -3	i	2392. 12.				74.2		- 10.48
24476.50 -3	00 79.7	2256. 12.						
24477.50 -2		2123. 11.				72.5		
24477.75 -2		2090. 11.	60 1.73	4051	10.67	72.3	1015	7 6 7 0

STAND WG 38000.LBS		TEST WGT 38500.LBS		PRESS #	ALT N HG	ТЕМР 13-6 С	WIND 5.6	VEL KIS		DIREC DEG MAG
gár.			TE	ST DAY-				ST	ANDARD I	DAY
TOD	ACCEL	GND-SPD	DIST	KE	FBH	ÜĤĐ	EBR	KTAS	DIST	KE
26701.75	-4.27	144.4	8047.	35.53	505.		•01	137.3	7222•	
26702.75	-3.50	142.2	7805.	34.47	0.	0.000	.01	135.1	6998.	30.72
26703.75	-3.72	140.0	7567.	33.39	0.	0.000	.01	132.9	6776.	29.72
26704.75	-3.47	137.8	7333.	32.39	0.	0.000	•01	130.8	6558.	28:79
26705.75	-3.53	135.9	7101.	31.48		0.000	.01	128.9	6344.	27.95
26706.75	-3.38	133.8	6374.	30.53		0.000	•01		6134	27.07
26707.75	-3.65	131.7	6550.	29.56		016	. • 05	124.7	5926	26.17
26708.75	-3.43	129.6	6429.	28.63	. 281		-12	122.7		25.31
26709:75	<b>-3.</b> 65		6213.	27.72	637.		.21	120.6	5522•	24.47.
26710.75	-3.64	125.2	5999.	26.73	. 768			118.4	5323.	23.56
26711.75	-3.94	123.3	5789.	25.90	1239.		•56	116.4	5130.	22.79
26712.75	-3.96	120.8	5583.	24.85	- 1447.		.87	113.9	4939.	
26713.75	-3.81	118.4	5381.	23.91	1365.	_	1.15	111.6	4752.	
26714.75	-3.21	116.3	5183.	23.07	801.		- 1.35		4570	4
26715.75	3.88	114.4	4988.	22.31	1728.		1.60	107.6	4391.	19.49
26716.75	-3.08	112.1	479H.	21:49	913.		1.86	105.3		18.66
26717.75	-3.26	110.5	4609.	50.81	1200.		5.05	103.8	4043.	18.11
26718.75	-3.19	108.6	4425.	50.10	1231.		2.24	101.9	3875.	17.46
26719.75	2.86	106.8	4243.	19.43	949.		2.43	100.1	3710.	16.85
26720.75	-3.63	104.9	4064.	18.74	1953.		2.70	98.2	3547.	16.52
26721.75	-3.15	102.8	3989.	18.02	1507.		-3.00	96.2	3387.	15.56
26722.75	-3.71	100.8	3717.	17.30	2272.		3.35	94.1	3230.	14.91
26723.75	-3.69	98 <b>.7</b>	3549.	16.59	2364.		3.72	92.1	3077.	14.26
26724.75	-4.14	96.1	3384.	15.74	3015.		4.21	89.5	2926.	13.49
26725.75	-3.16	94.0	3224.	15.07	1960.		4.57	87.5	2780.	12.87
26726.75	-4.01	92.1	3067.	14.46	3051.		4.96	85.6	2638	12.33
26727.75	-3.68	69.7	2913.	13.70	2858		5.43	83.2	2498	11.64
26728:75	-3,46	R7.7	2764.	13.10	2668		5.82	81.2	2363	11.09
26729.75	-2.80	85.8	2618.	12.55	1969.		6.14	79.4	2232	10.60
26730.75	-3.99	84.0	2474.	12.02	3449.		6.53	77.5	2104.	10.12
26731.75	-3.64	81.4	2335.	11.29	3144.		7.02	75.0	1977.	9.46
26732.75	-3.44	79.6	2199.	10.79			7.39	73.2	1856.	9.01
26733.75	-3.50	-77.3	2067.	10.18	3124.		7.82	70.9	1737.	8.46
26734.75	3.25	75.5	193A.	9.70	2901.	_	8.19	69.1	1623.	8.04
26735.75	-3.39	73.4	1912.	9.18	3125.		8.57	67.1	1512.	7.57
26736.75	-3.73	71.4	1590.	8.68	3607		8.98	65.1	1404.	7.13
2673775	-3.50	69.1	1572.	8.15	3401.		9.40	62.9	1299.	6.65
26738.75	-3.75	67.1	1456		3762	_	-9.80	60.8	1198.	6.23
26739.75	-3.99	64.7	1345.	7.12	4120.		10.26	58.4	1099.	5.75
26740.75	~4.II	62.4	1238.	6.63	4334.		10.70	56.2	1005.	5.31
26741.75	-3.82	59.9	1135.	6.12	4060.		11.13	53.8	915.	4.86
26742.75	-4.42	57.6	1035.	5.65	4839.		11.57	51.4	828	4.45
26743.75	-3,77	55.1	941.	5.17	4129.		11.49	49.0	746.	
26744.75	-3.98	52.9	850.	4.77	4450.	•150	12,37	46.8	668.	3.69
26745.75	-4.15	50.4	762.	4.32	4710.		12.78	44.3	593	3.30
26746.75	-3.87	48.0	679.	3.92	4430		13.15	41.9	522.	2.96
26747.75	-4.22	45.8	500.	3.57	4890.		13.51	39.8	456.	2.66
26748.75	-4.57	42.9	526.	.3.14	5372.		13.91	37.0	393.	2.30
26749.50	-1.71	41.2	472.	2.89	1984.	•068	14.05	35.2	349.	2.09

TEST NO. 69C MARK III ANTISKID/SOMMERS TIRES (WORN)/WET RUNWAY  STAND WGT TEST WGT PRESS ALT TEMP WIND VEL WIND DIRECT 34000.LBS 34350.LBS 27.578 IN HG 15.1 C 6.5 KTS 210.0 DEG N	MAG
STAND WGT TEST WGT PRESS ALT 34000.LBS 34350.LBS 27.578 IN HG 15.1 C 6.5 KTS 210.0 DEG N	MAG
STAND WGT TEST WGT THESS ALT 34000.LBS 34350.LBS 27.578 IN HG 15.1 C 6.5 KTS 210.0 DEG N	MAG
34000 LBS 34350 - LBS 27-576 IN 18	
CTANDAGO DAV	
TEST DAYSTANDARD DAY-	u
CONTROL OF STATE OF SERVICE STATE OF SERVICE S	F
100 ACCE OND-30 27 27 27 31 - 001 -00 126.4 6161. 24.6	
28476-55 -3-77 132 1 6764 26-54 99 005 02 124-2 5963 23-1	
28477.50 -3.77 130 8 6543. 25.p3 60003 .05 122.0 5759. 22.0	
28470 50 33.85 127.7 6325 24.80 484 .025 .11 119.9 5558 21.	
20479 50 =3 38 125 6 pll2. 23.97. 143007 -17 117.7 5362. 20.0	
20401 50 -3 50 123 5 5962 23 21 392 4018 422 115 8 5169 20	
20/22 50 -3:37 121.5 5595. 22.45 387018 .30 113.7 4980. 19.	
29492 50 -3.68 119.5 5491. 21.70 829038 .42 111.7 4793. 18.	
28/8/ 50 1-3 82 117.2 5292. 20.88 1125051 .63 109.5 4610. 18.	
28485 50 =3.33 115.1 5096. 20.14 706033 1.80 107.4 4430 17.	
28/84 50 =3.53 113-1 4903. 19.46 .1052047 .96 105.5, 4255. 10.	
20/07 50 13 06 110 9 4714, 18,72 1111, 048 1,18 103,3 4002, 10,	
20/00 50 -3 42 108 9 4528 18.04 1156	
28489-50 =3.26 107.0 4346. 17.40 1096. 049 1.59 99.4 3756 14	
28490.50 =3.55 105.0 4167. 16.77 1485	46
28491.50 -3.63 102.8 3992. 16.07 1703074 2.11 95.3 3271 13.	
28492-50 -3-25 100-9 3820 15-47 1384 001 2-35 93-4 3271 13-	
28493-50 -3-17 98-8 3652- 14-84 1403062 2-61 91-3 3179- 12-	
28494-50 -3.38 97.1 3486. 14.34 17020/3 2.83	
28405 50 -3.87 94.7 3324. 13.64 2348100 3.20 87.3 2824. 11.	
28496.50 -2.98 92.7 3166. 13.08 1495061 3.48	
28497.50 -3.26 91.0 3011. 12.59 1851079 3.72 83.6 2543. 10.	
28408 50 =3.58 89.0 2659. 12.03 2277096 4.05 81.6 2407. 10.	57
28499.50 -3.06 87.1 2710. 11.53 1817075 4.33 79.7 2176. 9	13
28500.50 -3.44 85.2 2565. 11.03 2308094 4.63 77.9 2130. 9	68
28501-50 -3.15 83.2 2423. 10.53 2043088 "4.93 75.9 2020. 0.	25
28502.50 -3.82 61.3 2284. 10.05 2850119 3.27 71.0 1770 7	.75
28503.50 -3.38 79.0 2149. 9.48 2464104 5.64 71.7	33
28504-50 -3-49 77-0 2017- 9-01 2059- 111 5-97 09-8 1002	89
28505.50 -3.52 74.8 1889. 8.51 2768. 113 5.33 57.6 1840. 6.	48
28506.50 -3.54 72.8 1765. 8.05 2856. 120 0.66. 03.6 1333. 6.	.06
28507.50 -3.63 70.6 1644. 7.58 3022. 127 7.04 33.5 1331. 5	66
28508.50 =3.72 68.4 1220. 1.12	.28
28509.50 -3.49 66.1 1413. 5.07 332. 135 6.06 57.2 1038. 4.	.92
28510.50 -3.52 64.2 1302. 6.20 3240 340 4 45 55.0 55.0 946. 4	•56
28511.50 -3.92 62.0 1190. 5.33 3466 140 8.81 52.8 858. 4.	.19
28512.50 -3.72 59.8 1093. 3.73 3.73 0.17 50.5 773. 3.	.84
28513.50 -3.92 57.5 994. 5.03 154 9.52 48.3 693. 3.	•52
28514.50 -4.10 55.3 577. (3) (375 180 9.9) 45.7 615. 3.	.15
28515.50 -4.40" 52.0 500. 751 3.63 4029 1166 10.27 43.3 543. 2.	.82
28516.50 -4.02 50.6 771 3063 154 10.60 40.9 474. 2.	•52
28517.50 -3.89 47.7 337. 3.70 170 10 03 38.6 409. 2.	.24
28518.50 -4.33 45.4 500 2.74 5535 210 11.30 35.8 348. 1.	.93
28519.50 -5.26 42.6 42.6 23. 2.24 2124 203 11.67 32.6 291. 1.	.60
28520.50 -4.82 39.4 417. 2.36 4663 179 11.97 30.1. 240. 1.	.36
28521.50 -4.33 30.8 352. 2.00 1.74 4771 190 12.26 27.3 193. 1	.12
28522.50 -4.40 34.0 272. 1.53 4625	.95
20523.50 =4.21 31./ 637. 1.03 4063. 417. 4663.	.75
28524.50 -5.16 25.9 103. 1.01 -5.02 -13.03 -19.1 -79.	.55
20020-00 700 700 700 700 700 700 700 700 700	.43
28526.25 -2.69 23.5 105	

一,是我们的工作。这一种是我们一个一个人就看到一个生活的一个人就是是一个人的人,

## list of abbreviations and symbols

Item	Definition	Units
a	aircraft acceleration from phototheodolite data	ft/sec ²
AFISC	Air Force Inspection and Safety Center	
AFWL	Air Force Weapons Laboratory	
AOA	angle of attack	units
ASD	Aeronautical Systems Division	
BPG	B.F. Goodrich	
CD	drag coefficient	dimensionless
$c_{L}$	lift coefficient	dimensionless
D	aircraft drag	1b .
DBV	diagonally braked vehicle	
$\Delta E_{BR}$	energy absorbed by both brakes during de- celeration from one data point to the next	ft-lb
Es	standard day kinetic energy	ft-1b
Et	test day kinetic energy	ft-1b
FBR	braking force	1b
$F_{n_I}$	net idle thrus:	1b
fps	feet per second	
g	acceleration of gravity	32.2 ft/sec ²
L	aircraft lift	1b
LE	leading edge	
MCAIR	McDonnell Aircraft Company	
MLG	main landing gear	
NASA	National Aeronautics and Space Administra- tion	
Nm	normal force on the main landing gear	1b
Nn	normal force on the nose gear	1b
Nx	longitudinal acceleration	g
Ny	lateral acceleration	g
Nz	normal acceleration	g
PBM	pressure bias modulation	
RAD	Requirements Action Directive	
ROC	Required Operational Capability	
ΔS	the distance travelled by the aircraft from one data point to the next	ft

<u>Item</u>	Definition	Units
Sgs	standard day stopping distance at 2,300 feet, corrected for wind	ft
sgt	test day stopping distance, corrected for wind	ft
$s_{g_{t_w}}$	test day stopping distance, not corrected for wind	ft
TAC	Tactical Air Command	
TE	trailing edge	
USAFE	United States Air Force, Europe	
$v_g$	test day brake application groundspeed	fps
Vts	standard day true airspeed at 2,300 feet (or standard day, no wind groundspeed)	fps
$v_w$	component of wind along the runway, head- wind (+), tailwind (-)	fps
Ws	aircraft standard gross weight	1b
Wt	aircraft test gross weight	1b
α	angle of attack	deg
$\mu_{BR}$	braking coefficient of friction	dimensionless
$\mu_{r_n}$	rolling coefficient of friction; assumed to be 0.015	dimensionless
σs	standard day density ratio at 2,300 feet	dimensionless
σt	test day density ratio	dimensionless

## Subscripts

BR	brake, braking
g	ground, groundspeed
m	main landing gear
n	nose gear
s .	standard day
t	test day
w	wind